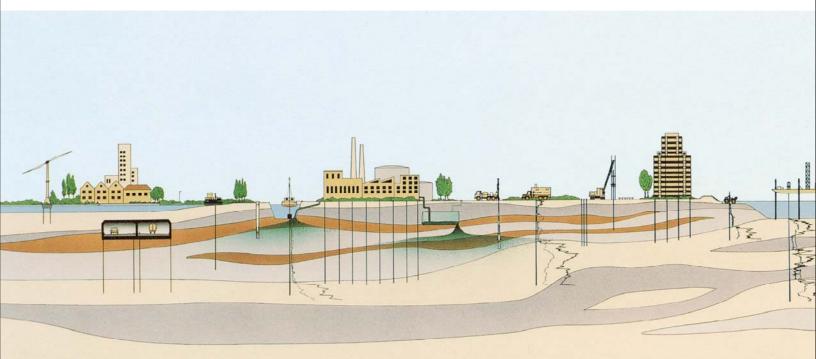
APPENDIX G: DESIGN GEOTECHNICAL DATA

FUGRO CONSULTANTS, INC.



DRAFT GEOTECHNICAL STUDY MISSISSIPPI RIVER LONG DISTANCE SEDIMENT PIPELINE (BA-43 EB) MISSISSIPPI RIVER TO BARATARIA WATERWAY LDNR RSIQ NO. 2503-08-22 JEFFERSON PARISH, LOUISIANA

MOFFATT & NICHOL BATON ROUGE, LOUISIANA



FUGRO CONSULTANTS, INC.



Report No. 04.55084005 - DRAFT November 29, 2011 4233 Rhoda Drive Baton Rouge, Louisiana 70816 Tel. (225) 292-5084 Fax: (225) 292-8084

MOFFATT & NICHOL

One American Place, Suite 800 301 Main Street Baton Rouge, LA 70825

Attention: Mr. Jonathan Hird, P.E.

Draft Geotechnical Study Mississippi River Long Distance Sediment Pipeline (BA-43B) Mississippi River to Barataria Waterway LDNR RSIQ No. 25503-08-22 Jefferson Parish, Louisiana

Fugro Consultants, Inc. (Fugro) is pleased to present this draft report of our geotechnical services for the above referenced project. Our services were performed in general accordance with our Proposal No. 5508-4005 dated July 13, 2011. We submitted a data report discussing our field and laboratory operations for the Phase I borings and CPTs on September 23, 2011 and preliminary recommendations based on the borings and CPTs for both Phase I and Phase II on October 28, 2011. Moffatt and Nichol provided comments subsequent to our preliminary recommendations that we have incorporated into this draft report.

This report includes a comprehensive discussion of our field and lab operations as well as a discussion of our engineering analyses and recommendations. We appreciate the opportunity to be of service to Moffatt and Nichol. Please call if you have any questions or comments concerning this draft report, or when we may be of further assistance.

Sincerely,

FUGRO CONSULTANTS, INC.

Jennifer E. Aguettant, P.E. Engineering Supervisor

Eric R. Marx, P.E. Branch Manager

Copies Submitted: (1) Addressee R:\08 GEOTECH\08-4005 MS River Long Distance Sediment Pipeline - Moffat & Nichol - LDNR\Engineering and Reporting\Final Report\04.55084005rpt MS River Long Distance Sediment Pipeline.doc)



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1.0 INTRODUCTION

1.1 Project Description

Over the last 100 years, the rate of land lost has increased rapidly in the Barataria Basin. One of the major factors has been the construction of levees on the Mississippi River and other natural channels, preventing the yearly deposition of soil as the river flooded and changed courses. Other contributing factors to land loss include manmade pipeline canals, subsidence, sea level rise, shoreline erosion, and saltwater intrusion.

The objective of this project is to obtain renewable sediment sources and provide an adequate corridor that supports equipment mobilization for long-distance conveyance of Mississippi River sediments to wetland creation projects in the Central Barataria Basin in Plaquemines, Jefferson, and Lafourche Parishes. A site vicinity map for the project is included on Plate 1. Our geotechnical study was concentrated on the proposed pipeline corridor alignment between the back levee and Barataria Waterway.

Two options were being considered for the pipeline alignment at the start of our study. The first option, designated the "Option A" alignment, follows a natural ridge immediately south of Chenier Traverse Bayou from the back levee to Bayou DuPont. The second option, designated the "Option B" alignment, follows an existing oil and gas channel that crosses the BA-39 Project area and then turns southwest towards Bayou Dupont. The alignments for Options A and B meet south of Bayou DuPont. After the completion of our field investigation, Option B was removed from consideration.

Moffatt and Nichol, the design engineer for the project, requested that we perform a geotechnical study within the project boundaries to assess subsurface conditions and provide geotechnical recommendations to the project team. Our findings are included herein.

1.2 Scope Of Services

The purposes of our geotechnical study were: 1) to explore and evaluate the subsurface soil conditions at the site, and 2) to provide geotechnical recommendations to assist the design team in developing plans and specifications for the sediment pipeline corridor. The scope of this study included the following:

- reviewing existing topographic and geotechnical information in the vicinity of the project to develop an exploration program
- drilling soil borings and performing Cone Penetration Test (CPT) soundings to evaluate subsurface conditions;



- performing field and laboratory tests on select soil samples to assess pertinent engineering soil properties;
- performing engineering analyses to estimate settlement, factors of safety against slope stability failures and ultimate bearing capacity due to the placement of marsh creation fill and containment dike material;
- preparing a report summarizing our findings and geotechnical recommendations.

Environmental assessments, compliance with state and federal regulatory requirements, and/or environmental analyses including those associated with mold, fungi, and other biologic agents were beyond the scope of this study. A geologic fault study was also beyond the scope of this study.

1.3 Applicability of Report

The explorations and analyses for this study were selected or developed based on our understanding of the project as described previously and in later sections of this report. If there are differences in project location or design features as we understand them, or if the locations or design features change, we should be authorized to review the changes and, if necessary, modify our conclusions and recommendations. The observations, conclusions, and recommendations presented in this report may not apply to locations not explored by our borings and CPTs or areas outside the project boundaries.

We have prepared this report exclusively for Moffatt and Nichol and the Louisiana Office of Coastal Protection and Restoration (OCPR) to guide the geotechnical aspects of the Long Distance Sediment Pipeline Project. We have conducted this study using the standard level of care and diligence normally practiced by recognized engineering firms now performing similar services under similar circumstances. We intend for this report, including all illustrations, to be used in its entirety. This report should be made available for information only and not as a warranty of subsurface conditions.



2.0 REVIEW OF EXISTING INFORMATION

Moffatt and Nichol provided reports of geotechnical studies performed by others in the vicinity of the Long Distance Sediment Pipeline project. In addition, survey data and construction observations from the recently constructed BA-39 marsh creation area was provided. The data was used to develop a field exploration program that would supplement the available subsurface information. In addition, the information was used as a guide to calibrate engineering analyses based on the performance of recently constructed marsh. We have provided a brief discussion of the contents of this available information in the following sections.

2.1 Eustis Engineering Company, Inc. Report (Project No. 19183, dated September 13, 2006)

Eustis Engineering Company, Inc. (Eustis) conducted a geotechnical investigation within the area of BA-39 and also in a potential borrow source area within the Mississippi River. BA-39 is located within the northeast portion of the alignment of the Long Distance Sediment Pipeline project. Eustis performed 3 soil borings along the Mississippi River bank in a potential borrow source area and 5 soil borings within the BA-39 area. The Eustis boring locations within BA-39 are shown on the Plan of Borings and CPTs on Plate 1. The boring logs from the Eustis report along with their plan of borings are presented in Appendix D.

Eustis performed settlement analyses of the containment dikes constructed to contain the marsh fill material as it is placed and the marsh fill material itself, in addition to the settlement of the underlying subsoils.

2.2 URS Corporation Report (Project No. 19228956, dated July 23, 2009)

URS Corporation (URS) conducted a geotechnical investigation within the BA-48 area adjacent to Bayou DuPont. The location of Bayou DuPont is shown on the Plan of Borings and CPTs on Plate 1. URS performed 9 soil borings within the BA-48 area. The URS soil boring locations within BA-48 are shown within the Plan of Borings and CPTS on Plate 1. The boring logs from the URS report are presented in Appendix D.

URS performed settlement analyses of the containment dikes and the marsh fill material. In addition, they also performed slope stability analyses of the containment dikes to evaluate stable side slopes.



2.3 BA-39 Data

The BA-39 marsh creation area was constructed between November 2009 and April 2010. The BA-39 marsh fill area is located in the northeast portion of the project location as shown on the Plan of Borings and CPTs on Plate 1. Sand was pumped from the Mississippi River to the BA-39 area to create the marsh.

Five settlement plates were placed on the natural mudline prior to the placement of the fill material. The locations of the settlement plates are shown on Plate 26. The elevations of the settlement plates were surveyed every one to two weeks during the construction process between November 1, 2009 and April 25, 2010. Moffatt and Nichol also provided information related to the end of construction of each cell within BA-39. Based on the settlement plate survey data and the dates of the end of construction of each cell, the underlying soils appear to have consolidated between 0.2-to 1-ft during the construction of BA-39.

Moffatt and Nichol also provided post-construction topographic survey information of the ground surface after completion of BA-39. The last date of the post-construction survey provided by Moffatt and Nichol was in April 2010. In April 2010, the ground surface within BA-39 appeared to be between EI. +2.0 and EI. +2.5. John Chance Land Surveys, Inc., a Fugro company, obtained recent topographic information within the BA-39 area on October 10, 2011, for LDNR Contract No. 2503-11-65, Task No. 9. Based on the recent topographic data, the current elevation within BA-39 is on the order of EI. +1.6-ft to EI. +1.8-ft. Using the topographic data provided by Moffatt and Nichol and John Chance Land Surveys, Inc., total settlement experienced by the sand fill material and the underlying soils is on the order of 0.2-ft to 0.9-ft between April 2010 and October 10, 2011. This information was used to calibrate our settlement analyses discussed later.



3.0 FIELD EXPLORATION

Based on a review of the existing survey and geotechnical information in Section 2.0, we developed a field exploration program to supplement the available data and obtain enough subsurface information suitable for design. Our field activities are discussed in this section. We have included discussions of drilling methods and boring/CPT locations, soil sampling methods, Cone Penetration Testing, water depth observations, and borehole and CPT completion.

3.1 Drilling Methods and Boring/CPT Locations

Our overall field exploration program consisted of a total of 10 soil borings to a depth of approximately 40 ft each below the mudline and 8 soil borings to a depth of approximately 60 ft each below the mudline. In addition, we also performed 10 Cone Penetration Tests (CPT) to a depth of approximately 40 ft each below the mudline, 5 CPTs to a depth of approximately 60 ft each below the mudline and 9 CPTs to a depth of approximately 10 ft each below the mudline.

The borings and CPTs were performed between August 17 and September 14, 2011. The borings and CPTs were performed in a marsh environment west of the Backwater Levee, east of the Barataria Waterway, and south of The Pen. The soil borings were drilled using our skid drilling equipment mounted to a marsh buggy using wet-rotary drilling techniques.

The approximate boring locations are presented in the Plan of Borings and CPTs on Plate 1. The soil boring locations were selected by Fugro and Moffatt and Nichol. Moffatt and Nichol provided proposed coordinates of the boring locations. T. Baker Smith staked the borings in the field prior to our drill crew's mobilization. It should be noted that location boring and CPT location 17 was moved approximately 1,000 ft to the east of its original location due to shallow pipelines in the vicinity that our drilling equipment would have to cross to access the original location. A list of the boring/CPT locations in each Phase and their depths is presented in the following table.

Location	Boring Depth	CPT Depth
1		40-ft
2		40-ft
3	60-ft	60-ft
4		40-ft
5	40-ft	
6		40-ft
7	60-ft	60-ft
8		40-ft
9	40-ft	
10		40-ft



Location	<u>Boring</u>	<u>CPT</u>
11	40-ft	
12	40-ft	
13	40-ft	
14		40-ft
15	40-ft	
16		40-ft
17	60-ft	60-ft
18	40-ft	
19	40-ft	
26	60-ft	60-ft
27		40-ft
28	60-ft	60-ft
29		40-ft
30		10-ft
32		10-ft
34		10-ft
35		10-ft
36		10-ft
37		10-ft
38	60-ft	
39		10-ft
40	40-ft	
41	60-ft	
42	40-ft	
43	60-ft	

We have presented the boring logs on Plates 2 through 19. A key to the terms and symbols used on our boring logs is presented on Plates 20a and 20b.

3.2 Soil Sampling Methods

Soil samples were generally taken at about 2-ft intervals to a depth of about 20-ft. Below the depth of continuous sampling, soil samples were taken at 5-ft intervals to the completion depth of the borings as indicated on the boring logs. Undisturbed samples of cohesive soils were obtained by hydraulically pushing a 3-inch-diameter, thin-walled tube a distance of about 24-inches. Our field procedure for cohesive soil sampling was conducted in general accordance with the *Standard Practice for Thin-Walled Tube Sampling of Soils* (ASTM D 1587). The thin-walled tubes were capped and sealed in the field and then transported back to our laboratory in the vertical position.



The samples were extruded in our laboratory and visually classified by one of our senior geotechnical personnel.

Our field procedure for sampling granular soils was conducted in general accordance with the *Standard Method for Penetration Test and Split-Barrel Sampling of Soils* (ASTM D 1586). Granular soil samples were obtained using the Standard Penetration Test (SPT) as described on Plate 20b. A manual hammer was used to obtain the hammer blows for each SPT. Our geotechnical personnel recorded the hammer blows for each sampling interval. The uncorrected SPT N-values are recorded on the boring logs. The soil samples obtained from the split-barrel sampler were visually classified and packaged for transportation to our laboratory.

3.3 Cone Penetration Testing

The CPT soundings were conducted using our skid-mounted CPT unit mounted on a marsh buggy that uses the weight of the marsh buggy to push a cylindrical steel probe into the ground. We obtained CPT data by pushing a series of cylindrical rods with an instrumented probe at the base into the soil at a constant rate¹. The probe consists of a cone tip element and a side friction sleeve element. Continuous measurements of penetration resistance at the cone tip and friction on the friction sleeve were recorded during the penetration. Continuous measurements of pore pressure were also made and recorded. CPT field data were saved on computer diskettes for further data reduction in the office.

The location of the CPTs can be found on the Plan of Borings and CPTs located on Plate 1. The CPT results will be correlated with the results of our borings.

The CPT logs are presented in Appendix C. A key identifying the terms and symbols used on the CPT logs and the generalized classification chart utilized for data reduction of the test results are also presented at the beginning of Appendix C.

3.4 Water Depth Observations

The soil borings and CPTs were performed in a marsh environment. Most of the boring/CPT locations were performed in the water; however, some were performed above the water level on the marsh. The approximate depth to the mudline for the exploration locations below the water surface at the time of our field operations varied between about 1.1- to 4.0-ft. The approximate depth of water at the boring/CPT locations is presented on the boring/CPT logs.

It should be noted that the water depth measurements are intended for the purpose of the geotechnical investigation only, and are not corrected for tidal or other variations. If utilized for



¹ Jean Louis Briaud and Jerome Miran, <u>The Cone Penetrometer Test</u>, Report to the Federal Highway Administration, Report No. FHWA-SA-91-043, February 1992.



other purposes, the water depth measurements should be adjusted to account for meteorological tide and datum corrections.

3.5 Borehole and CPT Completion

The borings and CPTs for this study were backfilled upon completion with cement-bentonite grout. We grouted the boreholes from the bottom up. When grout returned to the surface, we topped off each borehole by pouring grout from the surface.



4.0 LABORATORY TESTING

The laboratory-testing program for this study was directed toward evaluating the classification properties, undrained shear strength, and compressibility characteristics of the subsurface soils. Our laboratory tests were performed in general accordance with the appropriate ASTM standards as tabulated in this section.

4.1 Classification Tests

The classification tests included tests for natural moisture content, liquid and plastic limits (collectively termed Atterberg Limits), particle size distribution, percent passing a single sieve, and organic content. These tests aid in classifying the soils and are used to correlate the results of other tests performed on samples taken from different borings and/or different depths. The results of the classification tests are presented on the boring logs on Plates 2 through 19. The particle size analyses are presented on Plates 21a through 21f.

4.2 Undrained Shear Strength Tests

We measured the undrained shear strength of select undisturbed samples of cohesive soils by performing undisturbed and remolded miniature vane shear tests and undisturbed unconsolidatedundrained triaxial compression tests. Miniature vane shear tests were generally performed on each cohesive sample prior to extrusion. Natural moisture contents and dry unit weights were determined as routine portions of the compression tests. The results of the undisturbed shear strength tests are presented on the boring logs on Plates 2 through 19. The results of the undisturbed and remolded shear strength tests are presented in the Summary of Test Results in Appendix A.

4.3 One-Dimensional Consolidation Testing

We measured the compressibility characteristics of the soils along the proposed ridge alignment by performing 27 incremental one-dimensional consolidation tests. Undisturbed soil samples from various soil borings were selected at depths ranging from 3-ft to 54-ft below existing grade for consolidation testing. Natural moisture contents and dry unit weights were determined as routine portions of the consolidation tests. The consolidation test reports are presented in Appendix B. A summary of the consolidation test results is presented in the table on the following page.



	Summary of Consolidation Test Results							
Boring No.	Depth (ft)	e ₀	Cc	Cr	σ' _v (tsf)	σ' _p (tsf)	OCR	
B-3	15.0	1.11	0.30	0.07	0.33	0.44	1.3	
B-3	29.0	1.80	0.68	0.12	0.60	0.64	1.1	
B-5	7.0	1.77	0.53	0.11	0.18	0.23	1.3	
B-5	19.0	0.99	0.14	0.02	0.50	0.68	1.4	
B-7	3.0	3.13	1.87	0.23	0.03	0.03	1.0	
B-7	29.0	2.14	1.12	0.19	0.51	0.70	1.4	
B-9	3.0	6.07	1.95	0.32	0.03	0.03	1.0	
B-11	9.0	6.83	2.24	0.43	0.03	0.06	2.0	
B-12	7.0	7.07	2.68	0.43	0.03	0.03	1.0	
B-13	17.0	2.63	0.66	0.13	0.15	0.15	1.0	
B-15	5.0	0.90	0.18	0.02	0.11	0.45	4.1	
B-15	24.0	2.59	1.26	0.26	0.60	1.00	1.7	
B-17	17.0	1.00	0.22	0.03	0.45	0.95	2.1	
B-17	54.0	1.62	0.60	0.11	1.40	1.40	1.0	
B-18	7.0	1.73	0.58	0.15	0.05	0.40	8.0	
B-19	7.0	1.27	0.26	0.03	0.08	0.14	1.8	
B-26	7.0	3.01	0.93	0.29	0.08	0.18	2.3	
B-28	7.0	1.74	0.39	0.03	0.09	0.09	1.0	
B-28	13.0	2.19	0.70	0.16	0.21	0.17	0.8	
B-28	54.0	1.40	0.57	0.12	1.20	1.35	1.1	
B-38	3.0	3.23	1.21	0.25	0.03	0.03	1.0	
B-38	19.0	1.51	0.35	0.05	0.35	0.40	1.1	
B-40	13.0	2.49	0.76	0.12	0.14	0.14	1.0	
B-41	24.0	1.71	0.47	0.09	0.25	0.40	1.6	
B-42	11.0	5.50	2.60	0.34	0.07	0.07	1.0	
B-43	3.0	4.85	1.16	0.25	0.03	0.03	1.0	
B-43	19.0	4.15	1.15	0.28	0.20	0.20	1.0	
e_0 = initial void ratio σ'_v = effective overburden pressure C_c = compression index σ'_p = effective preconsolidation pressure								
C _r = recompression index OCR = overconsolidation ratio								

Summary of Consolidation Test Results



4.4 Summary of Laboratory Testing

The laboratory tests were conducted in accordance with the procedures described in the table below. The results of our laboratory tests are presented on the boring logs on Plates 2 through 19 and also in the Summary of Test Results in Appendix A.

Type of Test	Test Designation
Moisture Content	ASTM D 2216
Atterberg Limits	ASTM D 4318
Particle Size Distribution	ASTM D 6913
Material Finer than a No. 200 Sieve	ASTM D 1140
Organic Content	ASTM D 2974
Miniature Vane Shear (undisturbed and remolded)	ASTM D 4648
Unconsolidated-Undrained Triaxial Compression	ASTM D 2850
One-Dimensional Consolidation	ASTM D 2435



5.0 GENERALIZED SUBSURFACE CONDITIONS

The generalized subsurface soil conditions based on the results of our soil borings and Cone Penetration Test soundings are discussed in the following sections. Soil borings and CPTs within each soils reach were grouped based on similarities in stratigraphy and undrained shear strength. In summary, three distinct profiles were delineated along the alignment. The three soil profiles were designated Soils Reach 1, 2 and 3. The borings and CPTs included in each soils reach are defined in the table below.

Soils Reach	Soils Reach Borings CPTs		
1	B-3, B-5, B-7, B-38, and B-40	CPT-1, CPT-2, CPT-3, CPT-4, CPT-6,	
		CPT-7, CPT-8, CPT-30, and CPT-39	
2	B-9, B-11, B-12, B-13, B-19, B- 26, B-28, B-41, and B-42	CPT-10, CPT-26, CPT-27, CPT-28, and CPT-29	
3	B-15, B-17, B-18, and B-43	CPT-14, CPT-16, and CPT-17	

5.1 Soils Reach 1

Soils Reach 1 includes the portion of the pipeline alignment extending west of the backwater levee and east of Bayou DuPont and south of the Chenier Traverse Bayou as depicted on the Plan of Borings and CPTs. A generalized cross-section of the borings and CPTs included in Soils Reach 1 is presented on Plate 22.

Based on our field observations and the results of our laboratory testing and CPT interpretation, we classified the subsurface soils as mostly cohesive. Sand was found in the upper 3- to 7-ft of Borings B-3 and B-5 and CPT-1, CPT-2, CPT-3, CPT-4, CPT-30, and CPT-39. At CPT-6 and CPT-32, little to no sand fill was detected. We have assumed the sand to be fill material that was placed during the construction of BA-39. Based on grain size distributions performed on samples of the sand material obtained from Borings B-3 and B-5, the fill material is composed of poorly graded sand (SP).

The native soils beneath the sand fill consist primarily of fat and lean clay materials with organic clays and peat within the upper 4- to 5-ft. A layer of silty sand was encountered between El. -30-ft- and -40-ft in Boring B-38.



5.2 Soils Reach 2

Soils Reach 2 was designated to be the portion of the pipeline alignment extending south of Bayou DuPont and a portion of the Option B pipeline alignment as shown on the Plan of Borings and CPTs. The boring and CPT locations included in Soils Reach 2 are B-9, CPT-10, B-11, B-12, B-13, B/CPT-26, CPT-27, B/CPT-28, CPT-29, B-41, B-42, and B-19. Boring B-19 is actually located closer to Soils Reach 3; however, the soil conditions and strength parameters encountered in Boring B-19 are more similar to the borings included in Soils Reach 2. Therefore Boring B-19 was included in our analyses for Soils Reach 2. A generalized cross-section of the borings and CPTs included in Soils Reach 2 is presented on Plates 23 and 24.

Based on our field observations and the results of our laboratory testing and CPT interpretation, we would classify the subsurface soils as mostly cohesive material. The soils consist mostly of fat and lean clays with organic clay and peat found within the upper 4- to 14-ft of our soil borings. Silty sand was encountered in Boring B-9 between EI. -26-ft and -41-ft and in Boring B-28 between EI. - 31-ft and -41-ft. Sand pockets were also observed in Boring B-26 between EI. -41-ft and -48-ft. CPT-26, CPT-27, and CPT-28 also indicated sand between EI. -29-ft and -50-ft.

5.3 Soils Reach 3

Soils Reach 3 was designated to be the portion of the pipeline alignment extending to the west of Boring B-13, as shown on the Plan of Borings and CPTs. The boring and CPT locations included in Soils Reach 3 are CPT-14, B-15, CPT-16, B/CPT-17, B-18, B-19, and B-43. A generalized cross-section of the borings and CPTs included in Soils Reach 3 is presented on Plate 25.

Based on our field observations and the results of our laboratory testing and CPT interpretation, we would classify the subsurface soils as mostly cohesive material. The soils consist mostly of fat and lean clays. Organic clay and peat were observed within the upper 4- to 7-ft of Borings B-18 and B-43, which were located to the north of the proposed pipeline alignment. The rest of the borings in Soils Reach 3 indicated more lean clay as compared to the borings in Soils Reaches 1 and 2.

5.4 Design Soil Strength Parameters

Design undrained shear strength and unit weight profiles were developed for each soils reach based upon the results of the laboratory tests performed on samples from the soil borings along with cone penetration tests (CPT).

For the CPT data, site correlations have indicated that dividing the CPT tip resistance by a Nc factor of 20 correlates well with unconsolidated undrained triaxial shear tests. Therefore, combined plots of undrained shear strength versus elevation based on a Nc factor of 20 are presented on the design shear strength plots. Results of laboratory shear strength tests and unit



weights from undisturbed borings performed for this study are plotted for the various soils reaches on Plates 28 through 30.

5.5 Design Soil Compressibility Parameters

Soil compressibility parameters for design were developed using the 27 consolidation tests performed for this study. The results of the consolidation tests are discussed in Section 4.3. After reviewing the consolidation data, we determined in our analyses that the soil strata are normally consolidated and will compress along a "virgin" compression line (OCR = 1). Site-specific correlations for the compressibility index, C_c , as it relates to moisture content and liquid limit were generated based on all of the consolidation tests performed. We then plotted moisture content and liquid limit profiles for each Soils Reach and developed compressibility profiles for each soils reach.

In an effort to evaluate the time rate of settlement, we estimated the coefficient of consolidation (c_v) values from the consolidation tests and adjusted these values to match the historical data for BA-39 as discussed in the Settlement Analyses section of this report. Some of our soil borings and CPTs, especially those in Soils Reach 2, encountered layers of silty sand and poorly graded sand below a depth of about 20-ft. These sand layers will not compress as much as clay layers. As such, we neglected the presence of these sand layers in our analyses to provide a conservative estimate of settlement. In addition, these sand layers would behave as a drainage layer beneath the upper cohesive soils. The presence of a sand layer beneath the cohesive material would decrease the drainage path within the cohesive layer above and increase the rate of consolidation within the cohesive material.

As part of our consolidation testing program, some of the tested soil specimens were selected from Borings B-3 and B-5, which were performed within the formerly constructed BA-39 area. As previously mentioned, fill material was placed within the BA-39 area between November 2009 and April 2010. To develop our compressibility design profile within Soils Reach 1, the consolidation data from Borings B-3 and B-5 were considered in addition to the other borings within Soils Reach 1; however, we neglected any effects of consolidation from the application of the fill material.

In addition, we understand that the containment dikes within Soils Reach 1 will be constructed by excavating in-situ material from the interior of the footprint of the pipeline access corridor. The borrow excavation will be backfilled with the same sand fill material used to construct the pipeline access corridor. We anticipate the borrow excavation may extend to a depth of approximately 8-ft assuming a cut-to-fill ratio for the containment dikes of approximately 2.5:1.0. We understand the borrow excavation may extend to within 25-ft of the containment dike toes in the footprint of the pipeline access corridor. Therefore, most of the highly organic materials encountered in the upper 10-ft of our soil borings and CPTs will be removed and replaced with less compressible poorly graded sand. We evaluated the settlement of the pipeline access corridor fill material and foundation soils assuming the sand fill extended to EI. -9-ft. We also evaluated the settlement of



the pipeline access corridor fill material and foundation soils outside of the borrow excavation and the containment dikes assuming the in-situ compressible organic material was present.

We encountered a thick layer of organic clay and peat within the upper 20-ft of Borings B-42 and B-43 in the Marsh Creation Area. The Marsh Creation Area lies to the west of Soils Reach 2. The thick layer of organic material within the upper 20-ft of the Marsh Creation Area will compress more than the soils encountered within Soils Reach 2. To evaluate the range in compression that will occur in the March Creation Area, we evaluated the compressibility using both the compressibility profile defined for Soils Reach 2 and the more conservative profile based on Borings B-42 and B-43.

Bottom of	Generalized					
Layer	Soil		C _v ,			
Elevation, ft	Classification	C _c	ft²/day	eo		
-3.0	Peat	1.50	0.06	3.20		
-38.0	0.20	1.50				
-58.0 Fat Clay 0.68 0.20 1.80						
C _c = Coefficient of Compression						
C _v = Coefficient of Consolidation						
e _o = in situ initial void ratio						

Soils Reach 1: Compressibility Parameters

Note: The settlement analyses of the section of the pipeline access corridor in the vicinity of the borrow excavation assumed poorly graded sand was present from the mudline to El. -9-ft. We assumed the poorly graded sand was incompressible in our settlement analyses.

Bottom of	Generalized					
Layer	Soil		C _v ,			
Elevation, ft	Classification	C _c	ft²/day	eo		
-7.0	Peat	2.00	0.06	5.50		
-30.0	Fat Clay	0.34	0.20	2.40		
-45.0	Fat Clay	0.47	0.20	1.72		
-60.0 Fat Clay 0.34 0.20 1.40						
C _c = Coefficient of Compression						
C _v = Coefficient of Consolidation						
e _o = in situ initi	al void ratio					

Soils Reach 2: Compressibility Parameters



Solls Rea	ch 3: Compres	Sibility	Paramete	ers							
Bottom of	Generalized										
Layer	Soil		C _v ,								
Elevation, ft	Classification	C _c	ft²/day	eo							
-7.5	Peat	0.47	0.003	1.35							
-25.0	Fat Clay	0.29	0.03	1.00							
-32.5	Fat Clay	0.56	0.03	1.62							
-36.0	Fat Clay	0.34	0.03	1.50							
-60.0	Fat Clay	0.51	0.03	1.60							
C_c = Coefficier	C _c = Coefficient of Compression										
C_v = Coefficier	nt of Consolidation	on									

Soils Reach 3: Compressibility Parameters

e_o = in situ initial void ratio

Marsh Creation Area: Compressibility Parameters (Based on B-42 and B-43)

Bottom of	Generalized										
Layer	Soil		C _v ,								
Elevation, ft	Classification	C _c	ft²/day	eo							
-15.0	Peat	2.00	0.003	5.5							
-22.5	Organic Clay	1.40	0.003	4.5							
-60.0 Fat Clay 0.62 0.030 2											
C_c = Coefficier	nt of Compressio	n									
C_v = Coefficien	C _v = Coefficient of Consolidation										
e _o = in situ initi	e _o = in situ initial void ratio										



6.0 PROJECT FEATURES

Preliminary cross-sections for the design of the sediment pipeline corridor have been provided by Moffatt and Nichol throughout the course of our study. The most recent versions of these drawings at the time of this report are included in Appendix E.

We understand temporary containment dikes will be constructed along the portion of the access corridor between BA-39 and Bayou DuPont to contain the fill material as it is placed (see Cross-section 2 in Appendix E). In addition, a containment dike is also planned along the eastern edge of the access corridor adjacent to the existing canal for the section of the alignment south of the fish camp (see Cross-section 5 in Appendix E). We assumed the crown of the containment dike would be constructed to an elevation 1-ft above the adjacent access corridor fill material at the time of construction. Current plans have the containment dikes constructed of in-situ material excavated from the near-surface materials.

Subsequent to forming the containment dikes, sediment from the Mississippi River will be pumped to create the marsh platform along the pipeline access corridor alignment. In addition, an area adjacent to the pipeline corridor has been targeted for additional marsh creation.

We understand that the containment dikes along the access access corridor between BA-39 and Bayou DuPont will be degraded to an inclination of 20 Horizontal to 1 Vertical after construction of the access corridor (see Cross-section 2 in Appendix E). In addition, the section of the access corridor between Bayou DuPont and the fish camp, the western edge of the corridor south of the fish camp, and the marsh creation fill material will be constructed with a slope of approximately 20 Horizontal to 1 Vertical (see Cross-sections 4, 5, and 6 in Appendix E).

A brief discussion of the scope of engineering for each area of the project is included below.

6.1 Containment Dikes

Containment dikes will be constructed to contain the pipeline corridor fill material as it is placed along segments of the pipeline corridor. The final design of the containment dikes should consider the desired final elevation, side slopes, and crest width, which is based on the properties of the proposed material used for the construction of the containment dikes. The design should account for expected consolidation during construction, and the time needed for settlement to occur. For our analyses, we generated the following for the containment dikes:

- Time-settlement curves during construction;
- Short-term slope stability of the proposed side-slope inclinations;
- Cut to fill ratio for construction; and



• Construction sequence and recommendations

6.2 Pipeline Access Corridor and Adjacent Marsh Apron Fill Area

Hydraulically pumped borrow fill material from the Mississippi River will be placed within the containment dikes to create the pipeline access corridor and adjacent marsh apron. We have assumed that the material will be similar to the sand placed to create the BA-39 area. The following analyses were performed relative to the pipeline access corridor and marsh apron fill area:

- Time-settlement curves over the 20 year project life to meet certain elevation criteria including self-weight compression of the sand fill along with settlement of the underlying soils;
- Slope stability of the side slopes of the pipeline access corridor; and
- Cut to fill ratio for construction.

6.3 Additional Marsh Creation Fill Area

Hydraulically pumped borrow fill material from the Mississippi River will be placed in areas adjacent to the pipeline access corridor to create additional marsh restoration area. At the time of this report, the area to the west of Soils Reach 2 near Boring locations B-42 and B-43 were evaluated for additional marsh creation. The following analyses were performed relative to marsh creation area.

- Time-settlement curves over the 20 year project life to meet the elevation criteria set by Moffatt and Nichol including self-weight compression of the sand fill along with settlement of the underlying soils; and
- Cut to fill ratio for construction.

The analyses associated with the project features are discussed in the following sections. The results of our settlement analyses are discussed in Section 7.0, the results of our slope stability analyses are discussed in Section 8.0 and Construction Considerations are included in Section 9.0.



7.0 SETTLEMENT ANALYSES

Settlement analyses for the site were performed using the computer program Settle^{3D} developed by RocScience. Settle^{3D} uses Boussinesq's theory to compute stresses within the in-situ material under applied loads. The program then uses soil compressibility parameters to evaluate the change in thickness of individual layers and computes the overall movement at select locations. Settle^{3D} was used to compute the settlement of the in-situ material due to the application of the fill material for the containment dikes and the pipeline corridor fill material. We have presented a discussion of our settlement models and results in the following sections.

7.1 Settlement Models

For design purposes, we assigned the elevation of the water in the marsh to be at El. +0.5-ft, which is the mean low water level provided by Moffatt and Nichol. By using the mean low water level in our analyses, loads applied to the native soils by the fill material are more conservative than those computed using the mean sea level and the mean high water level. The current plan is to construct the pipeline corridor and marsh creation areas with the same material used to construct BA-39. Therefore, we assumed the placed fill material for the pipeline corridor will consist of poorly graded sand with an approximate total unit weight of 105 pcf. We understand the perimeter containment dikes will be constructed by excavating material along the centerline of the alignment. Accordingly, the containment dikes will be constructed of the organic clays and peat found in the upper strata of our soil borings. We assumed the containment dike material will have a total unit weight after placement of about 85 pcf. The soil compressibility profiles for each Soils Reach are included in Section 5.5.

Based on our understanding that the access corridors will be constructed of poorly graded sand, the majority of the self-weight compression of the sand material will occur during the construction process. We have estimated the self-weight compression of the fill material to be on the order of 2 to 3% of the fill height at the end of construction.

Moffatt and Nichol provided typical preliminary cross-sections of the pipeline access corridor and containment dikes. We evaluated the various cross-sections using the compressibility profile for the soils reach in which the cross-section is planned to be constructed. Moffatt and Nichol provided a range of mudline elevations within each soils reach. We evaluated the settlement using an upper and lower bound mudline elevation within each soils reach. The assumed mudline elevations evaluated for each soils reach are presented in the following table.



	Assumed Upper-	Assumed Lower-
	bound Mudline	bound Mudline
Soils Reach	Elevation, ft	Elevation, ft
1	+1.0	-1.0
2	+1.0	-2.0
3	+1.0	-2.5

Based on the parameters above, we evaluated various fill thicknesses for the pipeline access corridor to determine the minimum elevation needed to meet the long-term elevation criteria. We made the following assumptions about the construction process in developing our models:

- containment dikes would be constructed to an elevation 1-ft above the top of the pipeline access corridor at the end of construction;
- containment dikes would be constructed approximately two weeks prior to placement of the pipeline access corridor fill material
- pipeline access corridor fill material would be placed in less than or equal to seven days at a specific location;
- process survey would be conducted within approximately 30 days following the completion of fill placement; and
- the period of time between the beginning of placement of the pipeline access corridor fill material and the process survey was considered to be the duration of construction.

7.2 Settlement Analyses of the Pipeline Corridor and Containment Dikes

Moffatt and Nichol provided settlement criteria for the pipeline access corridor fill material as presented in the table below.

Years after	Target Design Elevation of Access					
Construction	Corridor and Marsh Fill Material					
5	+1.3-ft					
20	+0.5- to +0.9-ft					

We evaluated the settlement of the pipeline access corridor and the containment dikes using the upper- and lower-bound mudline elevations presented in the table in Section 7.1. The containment dikes were designed so that the crown of the dike was approximately 1-ft above the top elevation of the pipeline access corridor fill material at the end of construction. The results of our settlement analyses for the access corridor fill material and the containment dikes are presented in the



following tables. Plots of top of fill elevation versus time for the pipeline corridor fill material and the containment dikes are presented on Plates 31 through 35.



Soils Reach 1: Settlement of Access Corridor and Marsh Apron Fill Material (assumed Lower-bound mudline at El. -1.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
3.0	+2.0	0.41	3.41	0.20	0.11	0.72	+1.69	1.09	1.37	+0.60	+0.32
3.5	+2.5	0.44	3.94	0.22	0.12	0.78	+2.14	1.21	1.53	+0.93	+0.61
4.0	+3.0	0.47	4.47	0.22	0.14	0.83	+2.64	1.31	1.69	+1.33	+0.95

Soils Reach 1: Settlement of Access Corridor and Marsh Apron Fill Material (assumed Upper-bound mudline at El. +1.0-ft)

					-					-	
				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
1.0	+2.0	0.14	1.14	0.06	0.04	0.24	+1.90	0.60	0.92	+1.30	+0.98
1.5	+2.5	0.18	1.68	0.08	0.05	0.31	+2.37	0.77	1.20	+1.60	+1.17
2.0	+3.0	0.21	2.21	0.10	0.07	0.38	+2.84	0.91	1.41	+1.93	+1.43

Soils Reach 1: Settlement of Access Corridor and Marsh Apron Fill Material (borrow excavation to El. -9.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
3.0	+2.0	0.02	3.02	0.03	0.33	0.38	+1.64	0.20	0.36	+1.44	+1.28
3.5	+2.5	0.02	3.52	0.03	0.35	0.40	+2.12	0.25	0.43	+1.87	+1.69
4.0	+3.0	0.02	4.02	0.04	0.36	0.42	+2.60	0.28	0.50	+2.32	+2.10



Soils Reach 2: Settlement of Access Corridor and Marsh Apron Fill Material (assumed Lower-bound mudline at El. -2.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
4.0	+2.0	0.36	4.36	0.17	0.14	0.67	+1.70	1.28	1.82	+0.42	-0.12
5.0	+3.0	0.43	5.43	0.18	0.17	0.78	+2.64	1.48	2.13	+1.16	+0.51
5.5	+3.5	0.42	5.92	0.20	0.18	0.80	+3.12	1.52	2.18	+1.60	+0.94

Soils Reach 2: Settlement of Access Corridor and Marsh Apron Fill Material (assumed Upper-bound mudline at El. +1.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
1.0	+2.0	0.12	1.12	0.05	0.04	0.21	+1.91	0.52	0.92	+1.39	+0.99
1.5	+2.5	0.16	1.66	0.07	0.05	0.28	+2.38	0.69	1.19	+1.69	+1.19
2.0	+3.0	0.17	2.17	0.07	0.07	0.31	+2.86	0.74	1.32	+2.12	+1.54

Soils Reach 3: Settlement of Access Corridor and Marsh Apron Fill Material (assumed Lower-bound mudline at El. -2.5-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
4.5	+2.0	0.26	4.76	0.12	0.15	0.53	+1.74	1.00	1.72	+0.74	+0.02
5.0	+2.5	0.27	5.27	0.13	0.16	0.56	+2.22	1.06	1.83	+1.16	+0.39
5.5	+3.0	0.28	5.78	0.13	0.18	0.59	+2.70	1.14	2.02	+1.56	+0.68



Soils Reach 3: Settlement of Access Corridor and Marsh Apron Fill Material (assumed Upper-bound mudline at El. +1.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
1.0	+2.0	0.08	1.08	0.04	0.03	0.15	+1.93	0.35	0.65	+1.58	+1.28
1.5	+2.5	0.11	1.61	0.04	0.05	0.20	+2.41	0.45	0.85	+1.96	+1.56
2.0	+3.0	0.12	2.12	0.05	0.07	0.24	+2.89	0.53	1.03	+2.36	+1.86

Soils Reach 1: Settlement of Containment Dike Fill Material (assumed Lower-bound mudline at El. -1.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
4.5	+3.5	0.44	4.94	0.27	0.52	1.23	+2.71	1.11	1.32	+1.60	+1.39
5.0	+4.0	0.48	5.48	0.26	0.57	1.31	+3.17	1.16	1.40	+2.01	+1.77
5.5	+4.5	0.53	6.03	0.27	0.63	1.43	+3.61	1.29	1.58	+2.32	+2.03

Soils Reach 1: Settlement of Containment Dike Fill Material (assumed Upper-bound mudline at El. +1.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
2.0	+3.0	0.21	3.21	0.09	0.23	0.53	+2.68	0.73	1.08	+1.95	+1.60
2.5	+3.5	0.23	2.73	0.11	0.28	0.62	+3.11	0.84	1.25	+2.27	+1.86
3.0	+4.0	0.25	3.25	0.12	0.34	0.71	+3.54	0.94	1.40	+2.60	+2.14



									/		
				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
6.0	+4.0	0.43	6.43	0.24	0.67	1.34	+3.09	1.41	1.93	+1.68	+1.16
6.5	+4.5	0.45	6.95	0.25	0.72	1.42	+3.53	1.48	2.03	+2.05	+1.50
7.0	+5.0	0.46	7.46	0.24	0.77	1.47	+3.99	1.49	2.05	+2.50	+1.94

Soils Reach 2: Settlement of Containment Dike Fill Material (assumed Lower-bound mudline at El. -2.0-ft)

Soils Reach 2: Settlement of Containment Dike Fill Material (assumed Upper-bound mudline at El. +1.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
2.0	+3.0	0.18	2.18	0.08	0.23	0.49	+2.69	0.66	1.09	+2.03	+1.60
2.5	+3.5	0.20	2.70	0.09	0.28	0.57	+3.13	0.81	1.28	+2.32	+1.85
3.0	+4.0	0.21	3.21	0.11	0.33	0.65	+3.56	0.88	1.44	+2.68	+2.12

Soils Reach 3: Settlement of Containment Dike Fill Material (assumed Lower-bound mudline at El. -2.5-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
6.0	+3.5	0.26	6.26	0.15	0.64	1.05	+2.71	0.94	1.48	+1.77	+1.23
6.5	+4.0	0.26	6.76	0.16	0.69	1.11	+3.15	0.97	1.56	+2.18	+1.59
7.0	+4.5	0.28	7.28	0.15	0.74	1.17	+3.61	0.99	1.57	+2.62	+2.04



Soils Reach 3: Settlement of Containment Dike Fill Material (assumed Upper-bound mudline at El. +1.0-ft)

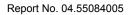
				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
2.0	+3.0	0.11	2.11	0.05	0.22	0.38	+2.73	0.40	0.73	+2.33	+2.00
2.5	+3.5	0.12	2.62	0.06	0.27	0.45	+3.17	0.47	0.86	+2.70	+2.31
3.0	+4.0	0.14	3.14	0.06	0.32	0.52	+3.61	0.53	0.96	+3.08	+2.65



7.3 Settlement of Marsh Creation Areas

In addition to the areas of the pipeline access corridor and containment dikes, Moffatt and Nichol also requested that we perform soil borings in an area of potential additional marsh creation, specifically in the area of borings B-42 and B-43. We performed settlement analyses for the marsh creation area using the compressibility profile developed from Soil Borings B-42 and B-43 and the Soils Reach 2 compressibility profile presented in Section 5.5. We believe the settlement computed using these two compressibility profiles will provide a range of anticipated settlement within the marsh creation area due to the varying soil conditions.

The settlement criteria for the marsh creation area are the same as that presented above in Section 7.2 for the pipeline access corridor fill material. The extent of the marsh creation area was unknown at the time of our analysis. We assumed an area 2,000-ft across to model the marsh creation area. The results of our settlement analysis for the marsh creation area are presented in the tables on the following page. Plots of top of fill elevation versus time for the marsh creation fill material are presented on Plate 36.





Marsh Creation Area: Settlement of Additional Marsh Creation Fill Material – Based on B-42 and B-43

	(assumed mudline at El2.5-ft)										
				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
6.0	+3.5	0.42	6.42	0.22	0.18	0.82	+3.08	1.76	3.04	+1.32	+0.04
6.5	+4.0	0.43	6.93	0.23	0.21	0.87	+3.55	1.85	3.17	+1.70	+0.38
7.0	+4.5	0.44	7.44	0.24	0.23	0.91	+4.02	1.93	3.32	+2.09	+0.70

Marsh Creation Area: Settlement of Additional Marsh Creation Fill Material – Using Soils Reach 2 Compressibility Profile

(assumed mudline at El. -2.5-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
5.5	+3.0	0.40	5.90	0.22	0.18	0.80	+2.60	1.54	2.22	+1.06	+0.38
6.0	+3.5	0.42	6.42	0.22	0.20	0.84	+3.08	1.62	2.35	+1.46	+0.73
6.5	+4.0	0.43	6.93	0.23	0.21	0.87	+3.55	1.68	2.47	+1.87	+1.08



8.0 SLOPE STABILITY ANALYSES

Slope stability analyses were performed for the containment dikes and marsh fill areas to determine the factor of safety for the proposed design. Moffatt and Nichol provided typical cross-sections of the pipeline corridor and containment dikes along the pipeline alignment. The provided cross-sections that were used in our slope stability analyses are presented in Appendix E. We have described which cross-section was evaluated within each Soils Reach in the table below.

Cross-Section No. (see Appendix E)	Description of Section of Alignment Corresponding to Cross-Section	Design Parameters used in Analysis
2	Between BA-39 and Bayou DuPont	Soils Reach 1
4	From BA-48 to the Fish Camp (Sta. 470+28.82)	Soils Reach 2
5	From the Fish Camp to Barataria Waterway	Soils Reach 2 and 3
6	Additional Marsh Creation Area	Soils Reach 2

The factor of safety against stability failure is expected to increase with time as the underlying foundation material consolidates and gains strength, and after placing the dredged material. The analyses were performed using Slope/W Version 7.17 (GeoStudio, 2007). The factor of safety was determined using Spencer's (1967) method of slices where force and moment equilibrium is achieved for each slice in this method. We evaluated circular failure surfaces in our analyses.

8.1 Material Properties

We used the undrained shear strength and total unit weight profiles presented on Plates 28, 29, and 30 for our slope stability analyses. We assumed the containment dike material had a total unit weight of 85 pcf and an undrained shear strength of 80 psf. We assumed the pipeline corridor material and the marsh creation fill material consisted of poorly graded sand with a total unit weight of 105 pcf and an internal angle of friction of 30 degrees.

8.2 Stability Models

We understand temporary containment dikes will be constructed along the portion of the pipeline corridor between BA-39 and Bayou DuPont to contain the fill material as it is placed (see Cross-section 2 in Appendix E). In addition, a containment dike is also planned along the eastern edge of the pipeline corridor adjacent to the existing canal for the section of the alignment south of the fish camp (see Cross-section 5 in Appendix E). We evaluated the stability of the containment dikes assuming a 3 Horizontal to 1 Vertical side slope inclination and a crown width of 6-ft. In addition,



we assumed the crown of the containment dike would be constructed to an elevation 1-ft above the adjacent pipeline corridor fill material at the end of construction. Current plans have the containment dikes constructed of in-situ material excavated from the near-surface materials. We assumed a cut-to-fill ratio of approximately 2.5:1 for the containment dike material. Therefore, we assumed the bottom of the containment dike borrow excavation would be between approximately EI. -9-ft to -11.5-ft depending on the existing mudline in the vicinity of the borrow area. We performed our stability analyses using the lower-bound mudline elevations evaluated in our settlement analyses for each soils reach. Using the lower-bound mudline elevations is a conservative approach for evaluating the stability of the containment dikes and pipeline corridor marsh apron as this would simulate fill placed at higher elevations than using the upper-bound mudline elevations. We assumed the containment dikes would be constructed to an elevation approximately 1-ft above the elevation of the pipeline access corridor fill material at the end of construction.

We understand that the containment dikes and fill along the pipeline corridor between BA-39 and Bayou DuPont will be degraded to an inclination of 20 Horizontal to 1 Vertical after construction of the pipeline corridor (see Cross-section 2 in Appendix E). In addition, the section of the access corridor and marsh apron between Bayou DuPont and the fish camp, the western edge of the corridor south of the fish camp, and the additional marsh creation fill material will also have side slopes of 20 Horizontal to 1 Vertical (see Cross-sections 4, 5, and 6 in Appendix E). We performed a stability analysis to evaluate the side slopes of the pipeline corridor using the appropriate design soil parameters for each cross-section.

8.3 Slope Stability Analysis Results

The results of our slope stability analyses for the various cross-sections and design soil parameters are summarized in the following table. The failure surfaces corresponding to the factors of safety presented in the following table are presented on Plates 37 through 43.

Soils Reach	Cross-Section (from Appendix E)	Description of Analysis	Side Slope Inclination	Elevation of Top of Fill (ft)	Factor of Safety
		Containment Dike			
1	2	adjacent to Borrow Area	3H:1V	+4.5	1.26
1	2	Pipeline Corridor	20H:1V	+3.0	2.99
		Containment Dike			
2	5	adjacent to Canal	3H:1V	+5.0	1.22
2	4	Pipeline Corridor	20H:1V	+3.5	1.72
		Containment Dike			
3	5	adjacent to Canal	3H:1V	+4.0	1.28
3	5	Pipeline Corridor	20H:1V	+3.0	4.39
2	6	Marsh Creation Area	20H:1V	+3.5	1.74

The reported factors of safety presented in the table above and on Plates 37 through 43, are above 1.2, which we believe is an acceptable factor of safety for the application of these structures. Factors of safety less than 1.2 were observed for shallow surficial slip surfaces. These shallow failure surfaces are more indicative of a localized bearing capacity failure and not a global slope stability failure.



9.0 CONSTRUCTION RECOMMENDATIONS

9.1 Containment Dike

The containment dike will be constructed from borrow material excavated and handled within the restoration area. The borrow material will likely be from the upper 10 feet and will comprise primarily of organic fat clays. Since the moisture content in the upper 10 feet ranged from 60 to over 200 percent, a moisture content of 125 percent was assumed to be a representative average value during dredging. Based on published values in similar material, we estimate the cut-to-fill ratio for dike construction for similar materials is in the range of 2.0 to 3.0:1.

In our stability model, a single-staged construction of the dike was assumed. However if the construction schedule permits, multiple-stage construction is preferred. This will significantly reduce possible displacements and shallow bearing capacity failures.

To reduce the potential of ponding of surface water on the containment dike, it is recommended that positive surface gradients be incorporated into the construction of the dike.

9.2 Access Corridor and Marsh Creation Fill Material

The borrow material for the fill area will be dredged from the Mississippi River. We have assumed that the material will be similar in consistency to that placed for BA-39.

We believe the volume of material required to fill the pipeline access corridor area will be approximately 1.2 to 1.5 times the initial calculated fill volume based on pre-construction survey data. The additional volume of material will need to be placed to accommodate potential shallow "mud waves" and settlement of the underlying native materials during construction prior to the process survey. As such, we recommend a cut to fill ratio between 1.2 to 1.5:1 be assumed for the borrow material.

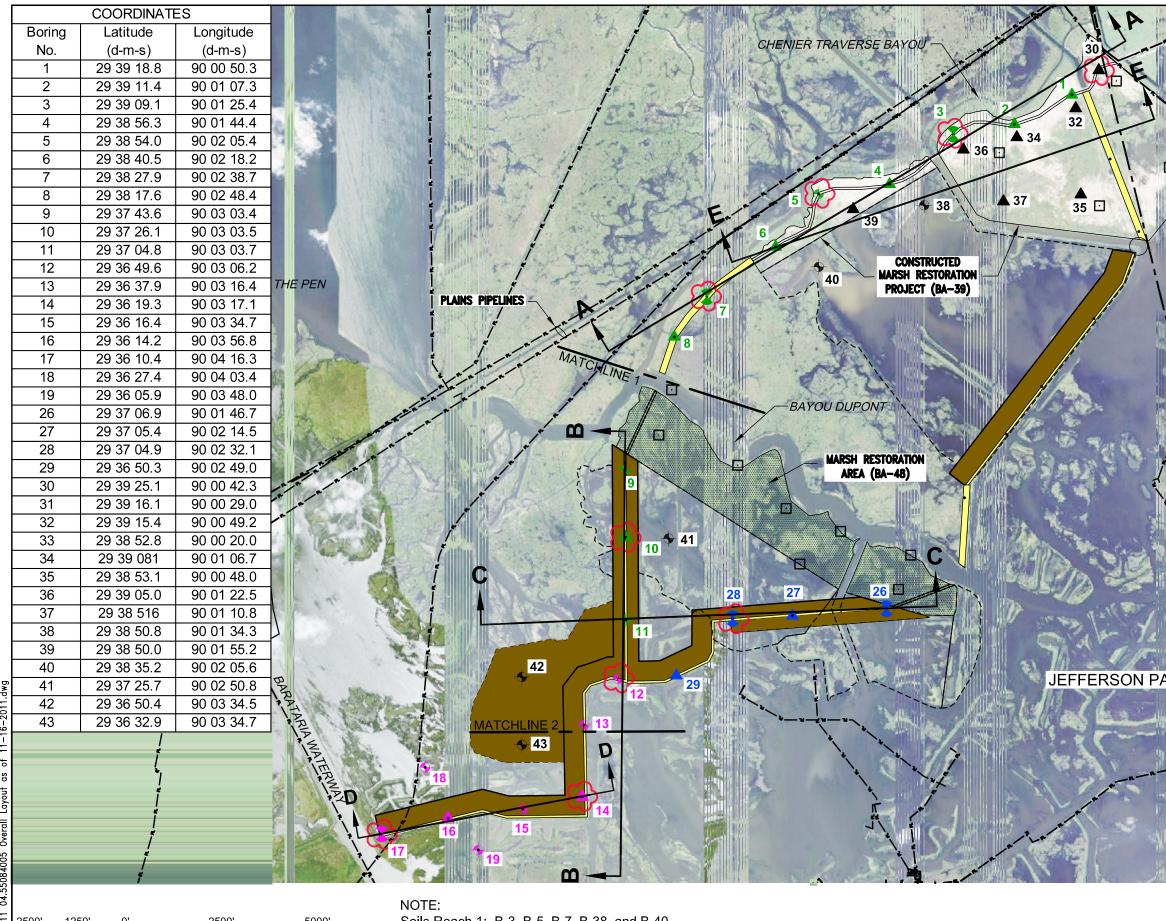
9.3 Additional Construction Considerations

Due to the very soft sediment located in the top 10-ft, it is likely that placement of material for both the containment dikes and marsh creation fill material will generate mud waves, or shallow bearing capacity failures at the site. The design recommendations considered more significant, deeper seated failures. If shallow mud waves are problematic and will not create a stable base for containment dikes, geotextiles or other methods of confinement may be required.



ILLUSTRATIONS





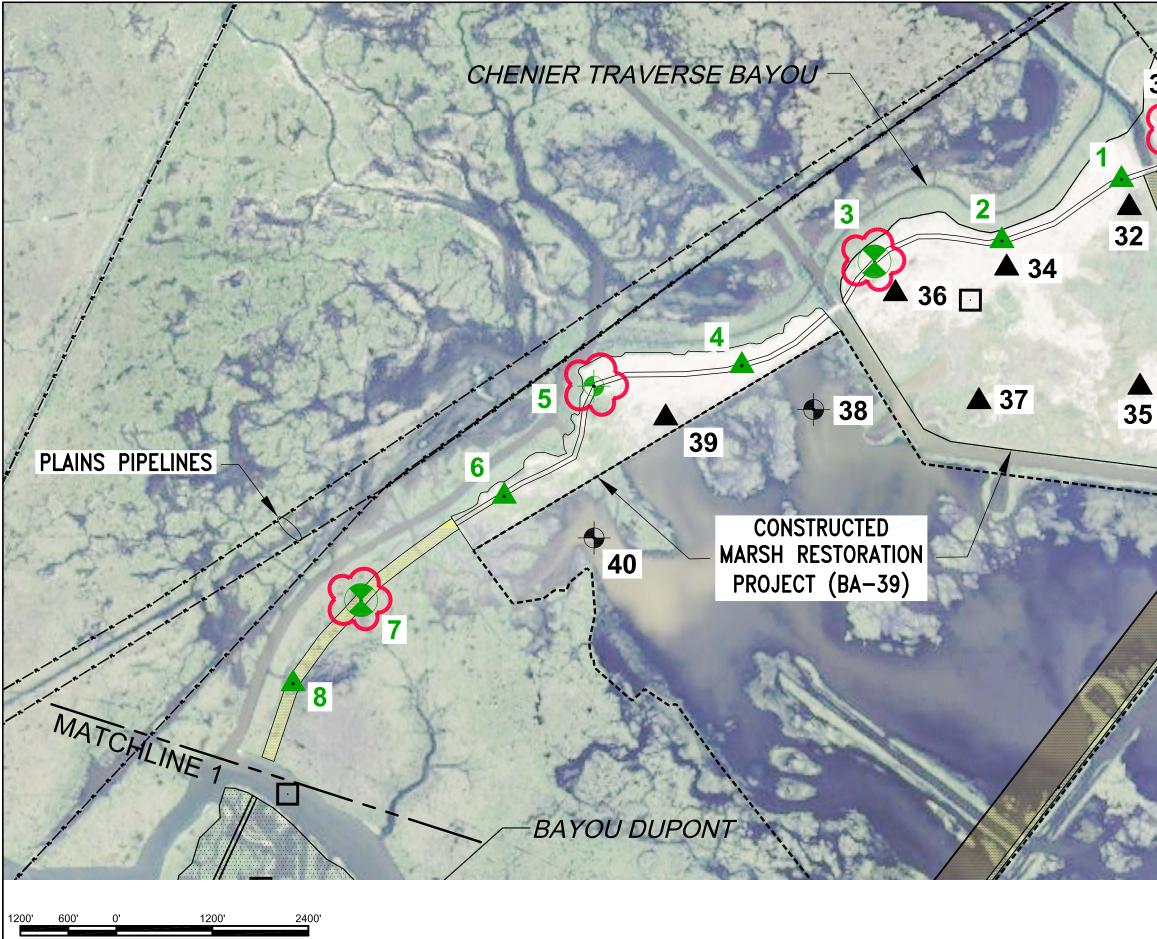


Site Plan provided by Moffatt & Nichol.

Soils Reach 1: B-3, B-5, B-7, B-38, and B-40 Soils Reach 2: B-9, B-11, B-12, B-13, B-19, B-26, B-28, B-41, and B-42. Soils Reach 3: B-15, B-17, B-18, and B-43.

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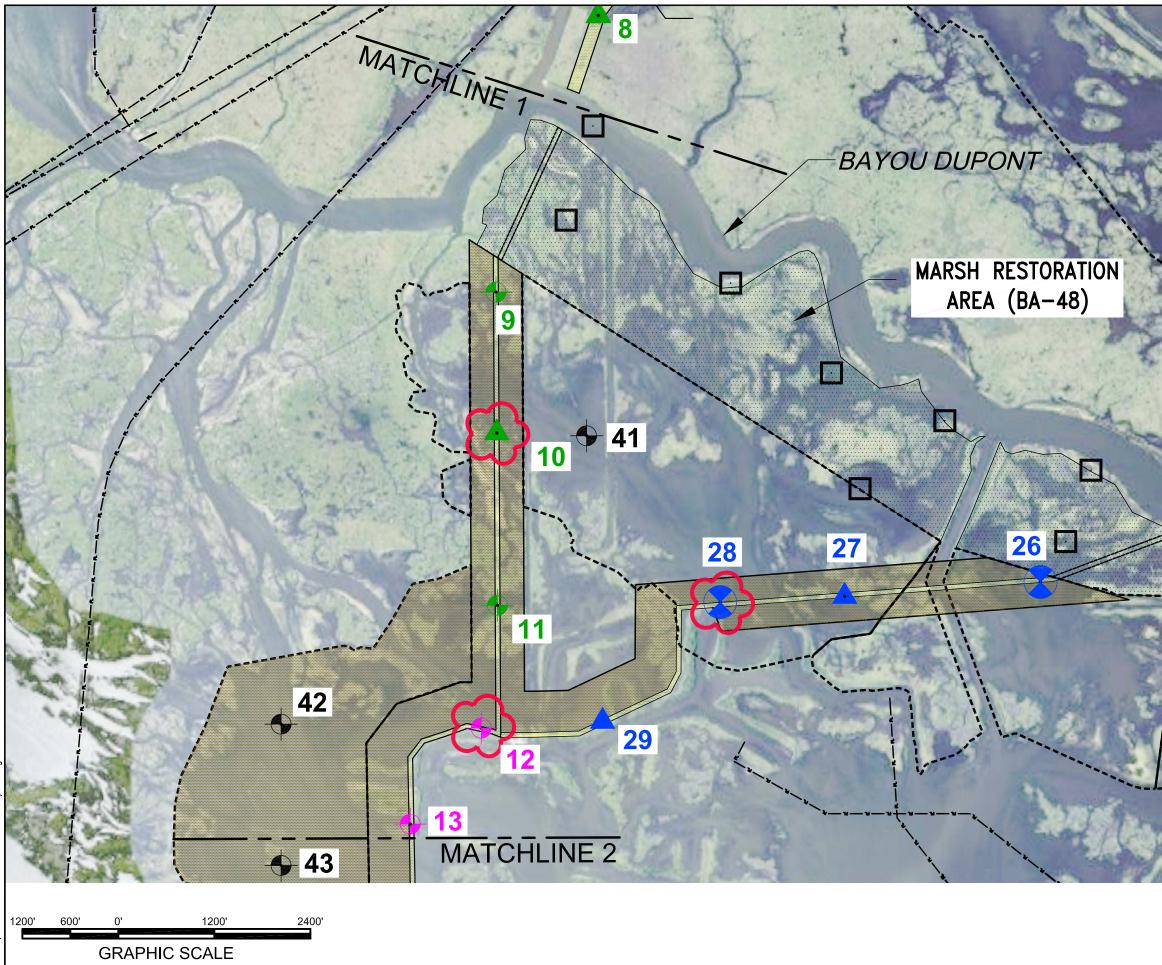


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GRAPHIC SCALE

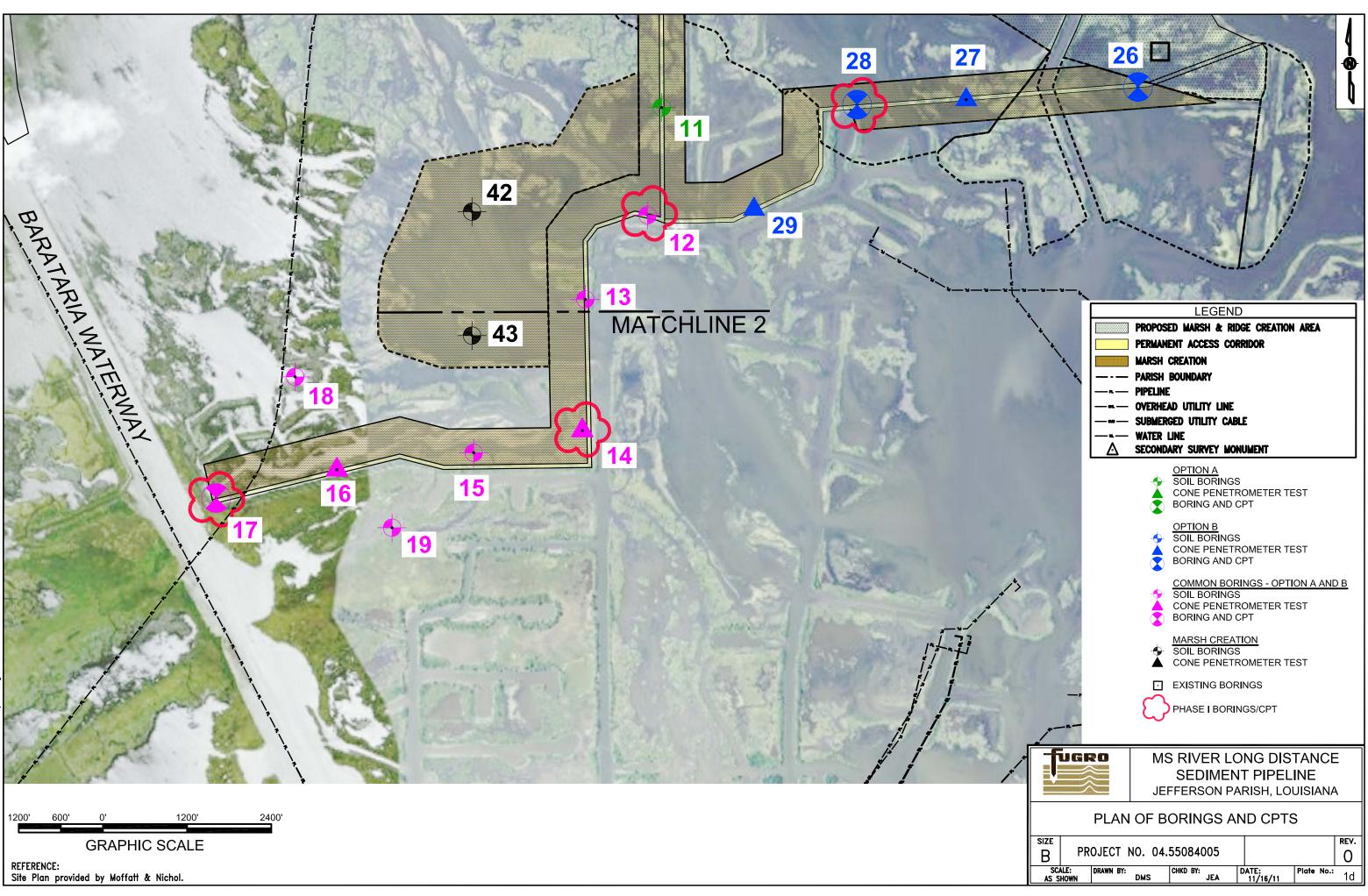
REFERENCE: Site Plan provided by Moffatt & Nichol.

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PLAN OF BORINGS AND CPTS
SIZE PROJECT NO. 04.55084005
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GRAPHIC SCA REFERENCE: Site Plan provided by Moffatt & Nichol.

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			~	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION	1		SHE	AR S	TREN	ЭТН	
DEPTH , FT	WATER LEVEI	SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 39' 09.1" W 90° 01' 25.4" SURFACE EL.: 1.5'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢⊤o	enetron Irvane eld Var	ie	Miniatu		ial 🔴
	Ś	$/ \langle$		STRATUM DESCRIPTION		NN	20 20	ŭ							R SQ FT		,
			N=Pusi	POORLY GRADED SAND (SP), loose, brown, fine-grained - gray below 1.5'		-					-		.2 0	.4 0	.6 0.8	1.0	,
5 -			N=7			-	5	21 18			-	-					
	-		\ <u> 11-7</u>	FAT CLAY (CH), soft, gray, with silt traces and organics	6.0	-	5	53 52 53	73	25	48	-					
- 10	-			- with ferrous nodules below 9'		-		65			-						
				- with sand pockets below 11' POORLY GRADED SAND (SP), gray, fine-grained	12.0	-	55 3	37 20	54	19	35						
- —15 —				LEAN CLAY (CL), very soft, gray	- 14.0	78	88	37	43	23	20		•				
				FAT CLAY (CH), soft, dark gray, with organics	+ 18.0	-		68			-		•				
- 20 -				LEAN CLAY (CL), very soft, gray	- 19.0	 - -		38			 						
					- 24.0	-		83			-	-					
25 - - - - - - - - - - - -				FAT CLAY (CH), soft to firm, gray, with silt layers		_ 55 - - - 59 -	100	68	72	24	- - - 48_ -		AO				
- 						-		80				-					
- - - - - - - - - - - - - - - - - - -	-					- 59		69			- - -			•	•		
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, ug	5.00	mount		Jefferson Parish, Louisiana					04.	550	840	05		۲L	ATE	: Z	d

		۲ ۲	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION	1		SHE	AR S	TREN	GTH	
DEPTH, FT	WATER LEVE SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 39' 09.1" W 90° 01' 25.4" SURFACE EL.: 1.5'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetrom orvane eld Van	e	Miniatu		al 🗨
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		r	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHE	AR S	TREN	GT⊦	ł
DEPTH, FT WATER LEVEI SYMROI	SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 38' 54.0" W 90° 02' 05.4" SURFACE EL.: 1.3' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	⇔ To ∆ Fie		e IPS PE	Miniat	ure Va T	xial 🗨
	· ·)	N=WOH	POORLY GRADED SAND (SP), very loose,			4	21				0	.2 0	.4 0).6 0.8	3 1	.0
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		N=27	- medium-dense at 2.5'		-	5	19			- - -						
			FAT CLAY (CH), very soft to soft, gray, with organics	7.0	59	97	68	81	24	57			•			
			o ganoo		_		54			-						
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			- with silt and sand pockets at 13'	45.0	-		29	66	22	44		Ê				
-15-			LEAN CLAY (CL), very soft to soft, gray - with shell fragments from 16' to 25'	- 15.0	_		39			-						
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					84	97	37	32	25	7						
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 		N=20	LEAN CLAY WITH SAND (CL), gray	- 33.5	- - -	84	31			-						
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			ools defined on Plates 20a and 20b. of Hammer					TOTA CAVE DRY WET BACA	al de Ed di Aug Rot Kfill	epth: Epth Er: N Ary:	40' Not Not Ap 0' to nent-	: Appl oplica 40'	icabl ıble	e Grout	11	
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	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHE	AR S	TRENC	GTH
DEPTH, FT WATER LEVEL SYMBOL SAMPLES BLOWS PER	COORDINATES: N 29° 38' 27.9" W 90° 02' 38.7" SURFACE EL.: -0.8'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢⊺o	enetrom orvane eld Van	e	Miniatu	confined ▼ Triaxial ● re Vane ▲
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	LEAN CLAY (CL), very soft to soft, gray and dark gray	- 5.0	- - - -		33 42 35 37				▲ ▲				
	FAT CLAY (CH), very soft, dark gray	- 11.0	 - -		42 70 73	38	22	- 16					
	- with shell fragments below 14' - with organics below 15'		- - -		155 93 53	99	32	- - 67					
	LEAN CLAY (CL) , very soft, gray, with shell fragments, and sand seams	- 18.0	- - -		36								
	FAT CLAY (CH), soft, gray, with silt seams and lenses	24.0	64 54 	100	62 74	85	27	 - - 58 - -		•			
			57 		75			-		•	•		
					68			- - - -					
	ymbols defined on Plates 20a and 20b. Jline below water surface = 1.3'. Jht of Hammer					TOT/ CAVI DRY WET BACI	al de Ed di Aug Rot Kfill	EPTH: EPTH: ER: N ARY: .: Cen T. Fe	60' Not Iot Ap 0' to nent-l	Appl oplica 60'	icable Ible		1
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Fugro Consultants, In	Jefferson Parish, Louisiana						ect No. 550	840	05		PL	ATE	4a

	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION		;	SHE	AR S	TREN	GTH
DEPTH, FT WATER LEVEL SYMBOL SAMPLES BLOWS PER	COORDINATES: N 29° 38' 27.9" W 90° 02' 38.7" SURFACE EL.: -0.8' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢To	netrom rvane eld Van K	ie		confined ▼ Triaxial ● re Vane ▲
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	and lenses FAT CLAY (CH) , soft to firm, gray, with silt seams and lenses	45.0	- - -		69			-		•			
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			-					-					
			- -					- -	•				
	ymbols defined on Plates 20a and 20b. dline below water surface = 1.3'. ght of Hammer		-			TOT/ CAVI DRY WET BACI	al de Ed di Aug Rot Kfill	TION E EPTH: EPTH: ER: N ARY: .: Cen T. Fe	60' Not Iot Ap 0' to nent-l	Appl oplica 60'	licabl able		11
Fugro Consultants, In	MS River Long Distance Sedime	ent Pip	elin	е		L	OG	OF	BO	RIN	IG I	NO.	B-7
Fugro Consultants, In	^{c.} Jefferson Parish, Louisiana						ect No. 550	840	05		PL	.ATE	5 4b

	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHE/	AR S	TREN	GTH
DEPTH, FT WATER LEVEL SYMBOL SAMPLES BLOWS PER FOOT	COORDINATES: N 29° 37' 43.6" W 90° 03' 03.4" SURFACE EL.: -1.3'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	netrom rvane eld Van	e	Miniatu	confined ▼ Triaxial ● Ire Vane ▲
	STRATUM DESCRIPTION		NN	200 200	8		Ľ	⊒≤				R SQ F	
<u>№//</u> Хм=wон	PEAT (PT), very soft, black, with roots				214				0	.2 0	.4 0	.6 0.8	1.0
		4.0	- 22	47	395 264	191	54	137					
	FAT CLAY (CH), very soft, gray, with organics	4.0	-		53			_					
			-		86			-	•				
10			-		49			-	•				
			- - -		40 68 44	55	24	- 31 _ -	•				
-15-			-		77			-	4				
			_		54			-	▲				
			-		35			-					
	SILT (ML), very soft to soft, gray, with clay pockets, and sand lenses	23.0	74		30 47	25	24	1					
-25	SILTY SAND (SM), gray, fine-grained	- 25.0	- - - - - -	44	28								
35	- loose below 38.5'	- 40.0	- - - - -	44	35				- - - - -				
 Depth to mudline WOH = Weight 6 	ools defined on Plates 20a and 20b. e below water surface = 1.7'. of Hammer recovered with splitspoon due to low recovery with s	ı	ube.	1		TOTA CAVI DRY WET BACI	al de Ed de Augi Rot Kfill	ION E PTH: EPTH: ER: N ARY: : Cen T. Fe	40' Not lot Ap 0' to nent-l	Appl oplica 40'	icable Ible	e	11
TUGRO	MS River Long Distance Sedimer	nt Pip	elin	е		L	OG	OF	BO	RIN	IG N	10.	B-9
Fugro Consultants, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05		P	PLAT	Е 5

L L				~	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION	1		SHEA	AR S	TREN	GTH	
STRATUM DESCRIPTION 2 4 22 04 06 01 0 1	DEPTH , FT	ATER LEVE	SAMPLES	LOWS PEF FOOT	W 90° 03' 03.7"	STRATUM DEPTH, FT	IIT DRY WT, PCF	ASSING NO. 00 SIEVE, %	WATER ONTENT, %	LIQUID	PLASTIC LIMIT	LASTICITY INDEX (PI)	¢To	rvane Id Van	e	Miniatu	Triax ure Va	kial 🔴
12 MeWork PEAT (PT), very soft, black, with, wood pieces 852 1 1 1 913 548 254 294 1 1 2 1 447 1 2 1 1 2 1 3 80 457 121 152 160 1 1 2 1 . with clay layers below 10' 14.0 128 1		Š		Ē	STRATUM DESCRIPTION		N	PA 20	8 8			₫ –	0					.0
1 1		- 1	ΙŇ	N=WOH	PEAT (PT), very soft, black, with, wood pieces		_		852			-						
10 13 80 465 312 152 160 15 0RGANIC CLAY (OH), very soft, gray 14.0 128 275 10 1 15 0RGANIC CLAY (OH), very soft, gray 14.0 128 128 1 1 20 EAM CLAY (CH), very soft, gray 16.0 183 125 35 90 1 20 EAM CLAY (CH), very soft, gray, with sand 19.0 36 1	- - - 5 -			N=Push	- with clay pockets at 6'		- - -			548	254	- 294 _ -						
15 ORGANIC CLAY (CH), very soft, gray 14.0 FAT CLAY (CH), very soft, gray 16.0 -20 LEAN CLAY (CL), very soft, gray, with sand Lenses FAT CLAY (CH), very soft, gray, with sand Lenses FAT CLAY (CH), very soft, gray, with sand Lenses FAT CLAY (CH), very soft, gray, with sand Lenses FAT CLAY (CH), very soft, gray, with sand Lenses FAT CLAY (CH), very soft, gray, with sand -25 -25 -30 -36 -30 -37 -38 -40 -39 -70 40 -70 40 -70 1. Terms and symbols defined on Plates 20a and 20b. 2. Depth to multine below water surface = 2.4'. 3. WOH = Weight of Hammer 4. Push = Sample recovered with splitspoon due to low recovery with shelby tube.	- - 10 - -		<u>\\</u> <u>\</u> <u>\\</u>		- with clay layers below 10'		13 13 	80	465 275	312	152	- 160_ - -		•				
PAT CLAY (CH), very soft, gray 16.0 125 35 90 - with sand lenses below 18" 19.0 36 - - - 20 - LEAN CLAY (CL), very soft, gray, with sand 19.0 36 - - - 20 - FAT CLAY (CH), very soft, gray, with sand 19.0 36 - - - 25 - - - - - - - - 30 - - - - - - - - - 30 - - - - - - - - - - 30 - <td></td> <td></td> <td><u></u>_</td> <td></td> <td>ORGANIC CLAY (OH), very soft, gray</td> <td>- 14.0</td> <td></td> <td></td> <td>320</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>			<u></u> _		ORGANIC CLAY (OH), very soft, gray	- 14.0			320									
20 LEAN CLAY (CL), very soft, gray, with sand 19.0 36 A 20.0 FAT CLAY (CH), very soft, gray, with sand 20.0 58 68 - -25 - 58 68 - - - -30 - 58 68 - - - -30 - 58 68 - - - -30 - 58 68 - - - -30 - 70 49 - - - -30 - 70 49 - - - - -30 - - 70 49 - - - - -31 - - - - 73 -<							_ _ _		130	125	35	90						
-25 -36 -68 -6 -30 -37 -6 -6 -35 -70 49 -6 -35 -70 49 -70 -35 -70 49 -6 -35 -70 49 -6 -35 -70 49 -6 -35 -70 49 -6 -35 -70 49 -6 -35 -70 49 -6 -35 -70 49 -6 -35 -70 49 -70 -40 -70 49 -6 -35 -70 49 -6 -35 -70 49 -70 -40 -70 -70 49 -6 -40 -73 -70 -73 -70 -40 -73 -70 -73 -70 -40 -73 -70 -73 -70 -40 -73 -70 -70 -70 -75 -70 -70					LEAN CLAY (CL), very soft, gray, with sand	1			36									
	- 				FAT CLAY (CH), very soft, gray, with sand		- - - - -		80 58 49 78 73			- - - - - - - - - - - - - - - - - - -		•				
Fugro Consultants, Inc. MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-11 Fugro Consultants, Inc. Jefferson Parish, Louisiana Project No. 04.55084005 PLATE 6		1. Te 2. De 3. W	epth t OH =	o mudlir Weight	e below water surface = 2.4'. of Hammer recovered with splitspoon due to low recovery with s					TOTA CAVE DRY WET BACE LOG	AL DE ED DE AUGI ROT KFILL GER:	EPTH: EPTH: ER: N ARY: : Cen T. Fe	40' Not Ap 0' to nent-l erro	Appl oplica 40' 3entc	icable ble onite (e Grout		
Fugro Consultants, Inc.Jefferson Parish, LouisianaProject No.04.55084005PLATE 6	Fugi	īu		20	MS River Long Distance Sedime	nt Pip	elin	e					BOR	ING	S NO	О. E	3-1 [,]	1
	Fug	ro Cor	nsulta	nts, Inc.	Jefferson Parish, Louisiana								05		Ρ	LAT	Е	6

			LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHEA	R ST	RENG	ЭТΗ
DEPTH, FT	WATER LEVE SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 36' 49.6" W 90° 03' 06.2" SURFACE EL.: -2.8'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢⊺o	netrom rvane eld Vane			onfined ▼ Triaxial ● e Vane ▲
	MA S	В	STRATUM DESCRIPTION	ο Ω	INU	PAS 200	> 00		E	EL R				R SQ FT	
	<u><u> </u></u>		PEAT (PT) , very soft, black, with roots and								0	.2 0.	4 0.	6 0.8	1.0
 - 5			grass		- - -		533 179 221	175	35	- 140 _ -	•				
	$\frac{1}{\sqrt{2}} \frac{\sqrt{2}}{\sqrt{2}}$		- with organic clay lenses below 6'		- _ 18 -	28	230 283 183	287	57	230	•				
					- - -		243			-		•			
			FAT CLAY (CH), very soft, gray	- 14.0			271								
 				40.0	-		77 92 52	77	23	54	•				
20			LEAN CLAY (CL), very soft, gray FAT CLAY (CH), soft, gray	+ 19.0 + 20.0	_		33								
		N=Push		- 40.0	- - - - - - - - - - - - - - - - - - -		53 57 55			- - - - - - - - - - - - - - - - - - -		•	•		
2	1. Terms a 2. Depth to	o mudline	ools defined on Plates 20a and 20b. e below water surface = 3.0'. recovered with splitspoon due to low recovery with s	_				TOTA CAVE DRY WET BACE LOG	AL DE ED DE AUGI ROT, KFILL GER:	PTH: EPTH: ER: N ARY: Cen T. Fe	40' Not lot Ap 0' to nent-lerro	Appli oplica 40' Bento	cable ble nite (Grout	
	UGE	20	MS River Long Distance Sedimer	nt Pip	elin	e				of e	BOR	RING	6 NC). В	-12
Fugro	o Consultar	nts, Inc.	Jefferson Parish, Louisiana						ct No. 550	840	05		Ρ	LAT	E 7

H H <th>БТН</th>	БТН
STRATUM DESCRIPTION 0.2 0.4 0.6 0.8 N=WOR ORGANIC CLAY (OH), very soft, black 412 1 1 1 1 -5 - 205 187 47 140 1 <td< td=""><td>onfined ▼ Triaxial ● e Vane ▲</td></td<>	onfined ▼ Triaxial ● e Vane ▲
N=WOR ORGANIC CLAY (OH), very soft, black 412 -5 - -5 - - -	1.0
- with wood pieces at 11'	
FAT CLAY (CH), very soft, gray 13.0 13.0 13.0 13.0	
-20- N=Push -25- -30- -30- -30- -30- -30- -35-	
NOTES: 1. Terms and symbols defined on Plates 20a and 20b. 2. Depth to mudline below water surface = 4.0'. 3. WOR = Weight of Rod 4. Push = Sample recovered with splitspoon due to low recovery with shelby tube. COMPLETION DATE: August 28, 2011 TOTAL DEPTH: 40' CAVED DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 40' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro	
Fugro Consultants, Inc.Jefferson Parish, LouisianaProject No.04.55084005PLATE	E 8

			~	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHE	AR S	TREN	GTH	1
DEPTH , FT	WATER LEVE SYMBOL	SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 36' 16.4" W 90° 03' 34.7" SURFACE EL.: -1.0'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢To	netrom rvane eld Van		Un Miniati		xial 🔴
	ΜΝ	$\left(\right)$	B	STRATUM DESCRIPTION		-IN N	PAS 200	-0		μ.	⊒≚				R SQ F		
			N=WOR	FAT CLAY (CH), very soft, black, with roots				61				0.	.2 0	.4 0	.6 0.8	3 1.	.0
		Ĥ				-					-						
				LEAN CLAY (CL), soft to firm, gray - with silt traces at 4'	- 3.0	-		36			-		•				
				- with roots at 6'		86	94	34	45	18	27						
						-		39 42			-	-					
						-		36			-						
				- with organics at 12'		-		35			-		•				
- 				SILTY CLAY (CL-ML), very soft to soft, gray	15.0			29			-						
	-					-	92	34 31	34	24	10	-	A				
- 20				FAT CLAY (CH), soft, gray, with organics	- 19.0	_		65			_		•				
											-						
- 25						-	96	93	142	37	105_		A				
						-					-						
- 30 -				- with silt layers below 28' - very soft to soft at 29'		64 		60			-			•			
- - - 				- with silt lenses from 33' to 35'		- - -		52 26	52	20	32		▲				
- - - - - - - - - - - - - - - - - - -				soft to firm, with silt layers below 39'	- 40.0	- - - <u>62</u> -		_64_			- - - -	- - 		_ • .			
i -	1. Ter 2. Dej	pth to		ools defined on Plates 20a and 20b. e below water surface = 2.0'. of Rod	1	1	1		TOTA CAVI DRY WET BACI	al de Ed di Aug Rot Kfill	ION E PTH: EPTH: ER: N ARY: : Cen T. Fe	40' Not Iot Ap 0' to nent-l	Appl oplica 40'	icable Ible	9	11	
	Ū		20	MS River Long Distance Sedimer	nt Pip	elin	е	1	LC)G (of e	BOR	INC	g No	0. E	3-1 :	5
Fugi	ro Cons	sultar	nts, Inc.	Jefferson Parish, Louisiana						ect No.	840	05		F	PLA1	F	9
									U- 1 .	550	070	55			_/ \ I	_	

			r	LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION			SHE	AR S	TRENG	GTH
DEPTH, FT	WATER LEVEI	SYMBOL	BLOWS PER FOOT	COORDINATES: N 29° 36' 10.4" W 90° 04' 16.3" SURFACE EL.: -2.3' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	⇔ Τα Δ Fi		ie IPS PE	Miniatur R SQ FT	
				FAT CLAY (CH), black				63				C	0.2 0	0.4 0	.6 0.8	1.0
-						F		47	66	21	45					
- 5 -				LEAN CLAY (CL), soft to firm, gray, with organics and roots	3.0	 		36 40								
· -						-		40 41 33			-					
-10				- very soft at 9'		- -		32 32 35	39	21	18_					
 -15						-		43 41 37			-	-		A		
· -						82	89	38	44	21	- 23					
						-		39			-					
-20						-					-					
-25				- with organics at 24'		39 		127			-	-				
-30			N=WOI	н		- - -						-				
-35						- - -	98	40 58			- - - -	•				
-40						- - -		58			- - -	-				
						-					-	1	<u> </u>			
2	1. T 2. C 3. V	erms Pepth VOH	to mudli = Weigh	mbols defined on Plates 20a and 20b. ine below water surface = 2.8'. it of Hammer e recovered with splitspoon due to low recovery w	vith shelby t	ube.			TOTA CAV DRY WET BAC	al de Ed di Aug Rot Kfill	ION E PTH: EPTH: ER: N ARY: .: Cen T. Fe	60' Not Not A 0' to nent-	t Appl pplica 60'	licable able		1
- f	ī	G	RO	MS River Long Distance Sedir	nent Pip	elin	е		LC)G (OF E	BOF	RING	g No	О. В	-17
V									Proie	ect No.						
Fuar	o Co	onsulta	ants, Inc.	Jefferson Parish, Louisiana							840				ΔTE	102

		~	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHEA	AR ST	RENG	STH
DEPTH, FT	WATER LEVEL SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 36' 10.4" W 90° 04' 16.3" SURFACE EL.: -2.3'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢⊺o	netrom rvane eld Van Kl	е		onfined ▼ Triaxial ● e Vane ▲
			STRATUM DESCRIPTION			10					0.			6 0.8	1.0
			LEAN CLAY (CL) , soft to firm, gray, with organics and roots		-		41			-					
			FAT CLAY (CH), soft to firm, gray	45.0	-										
 50					_ 64		60			-				•	
					-					-					
—55 — 					- -	100	62	85	27	58_ -					
 				- 60.0	- 69		_51			- - 					_+
					-					-					
65 					-					-					
 70					-					-					
					-					-					
 75 					- 										
					-					-					
					- -					- -					
 <u>NOT</u>	FS [.]				-			СОМ	PLET			: Aug	gust 2	21, 201	1
	1. Terms 2. Depth 3. WOH =	to mudlin = Weight	bols defined on Plates 20a and 20b. e below water surface = 2.8'. of Hammer recovered with splitspoon due to low recovery with s	shelby ti	ube.			CAVI DRY WET BACI	ed di Augi Rot Kfill	EPTH: EPTH: ER: N ARY: : Cen T. Fe	: Not lot Ap 0' to nent-l	oplica 60'	ble		
			1												
	UG	RO	MS River Long Distance Sedimer	nt Pip	belin	e		LC)G (of B	BOR	ING	S NO). В	-17
Fugro	o Consulta	ants, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05	I	⊃LA	TE	10b

		~	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHE	AR ST	TREN	GTH	
DEPTH, FT	WATER LEVEL SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 36' 27.4" W 90° 04' 03.4" SURFACE EL.: -2.5'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetrom orvane eld Van K	e		confined Triaxial re Vane	•
	$ \rangle $		STRATUM DESCRIPTION								0			6 0.8		
		N=WOR	PEAT (PT) , very soft, black, with organic clay, shells, roots, and wood		-		653			-	-					
 - 5		N=Push	ORGANIC CLAY (OH) , very soft, gray, with wood and roots	- 3.0	 - -		809 180 206									
			FAT CLAY (CH) , soft, gray, with silt pockets, organics, and wood	- 7.0	_ 61 _	99	60 54	94	30	64 _ _		▲ ▲				
- - -					- - -		57 82 58	83	27	- - - 56	-					
			- very soft from 17' to 20'		- - -		56 76 93	03	21	- ⁵⁰ - -						
 					- - -		31									
-25		N=WOR			- - -						-					
-30			- with silt layers at 28'		58 		73			-	-	•				
		N=Push			- - -		66			- - - -	-					
-40			- very soft below 38'	- 40.0	- - 		_72_			- - 	 '	 			_ + -	
2 3	I. Terms 2. Depth 3. WOR :	to mudline = Weight o	ools defined on Plates 20a and 20b. e below water surface = 3.0'. of Rod recovered with splitspoon due to low recovery with	 shelby t	ube.	<u> </u>		TOTA CAVI DRY WET BACI	al de Ed di Aug Rot Kfill	TION E EPTH: EPTH: ER: N ARY: .: Cen T. Fe	40' : Not Not Aj 0' to nent-	: Appl oplica 40'	icable ible	9		
J	UGI	RO	MS River Long Distance Sedime	nt Pip	elin	е		LC)G (of e	BOR	RINC	g No	Э. E	8-18	_
Fugro	o Consulta	ants, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05		PL	ATE	E 11	-

			LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHEA	AR S	TREN	GTH	1
DEPTH , FT	WATER LEVE SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 36' 05.9" W 90° 03 48.0" SURFACE EL.: -1.0'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢⊺o	netrom rvane eld Van		Un Miniatu		xial 🔴
	× (B	STRATUM DESCRIPTION		NN	200 200	8		Ľ	⊒≤				R SQ F		0
_		N=WOR	ORGANIC CLAY (OH), very soft, black, with				230				0.	.2 0	.4 0	.0 0.6) I.	
-		7	roots, grass, and wood		ŀ					-						
-		N=Push		- 5.0	-		256	189	43	146 - -						
- 5 - -			FAT CLAY (CH), very soft, gray, with organics and roots	- 5.0	-		70			-						
-			- with silt seams and traces from 7' to 10'		73	100	49	70	23	47						
- 					F		58			_						
_					È		56			-						
-				+ 14.0	_		55			-						
- 	\neg		LEAN CLAY (CL), very soft, gray, with silt layers	14.0	-		37			_						
-					-		40	43	18	25						
_					L		78			-						
-20 -					F		41			-	^					
					_					-						
-			SILTY SAND (SM), gray, fine-grained	24.0			26	NP	NP	NP						
25 - - - - - - - - - - -				- 33.5	- - - -	13	24									
- 		N=5	POORLY GRADED SAND WITH CLAY (SP-SC), loose to medium, gray, fine-grained	00.0	L					-						
					F					-						
- -					-					-						
- - 		N=25		40.0	- 	9	_24									
-					-					-						
NOTES: 1. Terms and symbols defined on Plates 20a and 20b. 2. Depth to mudline below water surface = 1.1'. 3. WOR = Weight of Rod. 4. Push = Sample recovered with splitspoon due to low recovery with shelby tube.													icable ble	e	11	
Fugi	ŪGI	RO	MS River Long Distance Sedimer	nt Pip	belin	е		LC)G (of e	BOR	INC	G NO). E	3-19	9
Fugi	ro Consulta	ants, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05		PL	.ATE	Ξ 1	2
L												1				

	<u>ب</u>		~	LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION	•		SHE	AR S	TREN	GTH	1
DEPTH , FT	WATER LEVEI SYMBOL	SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 37' 06.9" W 90° 01' 46.7" SURFACE EL.: -3.5'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢⊤c	enetron orvane eld Var		Ur Miniat		xial 🔴
DE	VAT	SA			R T		PASSI 200 SI	NOC	27	PLA	PLAS		к	IPS PE	R SQ F	т	
	>			STRATUM DESCRIPTION								0			.6 0.		.0
		XN	=WOH	ORGANIC CLAY (OH), very soft to soft, black		ŀ		264			-						
 - 5 -						- - -		158 145 198 357	185	39	146 - -		•				
				FAT CLAY (CH), very soft, black and gray, -	- 7.0	42	99	110	115	34	81						
 —10 —				with silt pockets at 7' - dark gray, with sand pockets and layers from 9' to 13'		-		29			-	-					
 				- gray below 12' - with organics from 12' to 18'		-	72	49 54 73	54	20	34 _						
						F		42			-	4	1				
						-		77 78 70	82	25	57						
				LEAN CLAY (CL), gray, with silty sand pockets	- 20.0	-					-	-					
				- very stiff at 24'		97		26			-						1.8
- 25 -				FAT CLAY (CH), soft, gray	- 25.0	-					-						
 30 		X	N=2	- with silt pockets below 28.5'		- - - -		58				-					
 35 		N	=Push			- - -		46			-	•					
 			N=8	SILTY CLAY (CL-ML), firm, gray, with sand pockets	- 38.0	- - -	96	38			-						
	1. Term 2. Dept 3. WOH	th to H = V	mudline Veight o	ools defined on Plates 20a and 20b. e below water surface = 3.4'. of Hammer. recovered with splitspoon due to low recovery with s	ube.	1		TOTA CAVI DRY WET BACI	al de Ed di Aug Rot Kfill	ION E PTH: EPTH: ER: N ARY: .: Cen T. Fe	60' Not Not Aj 0' to nent-	t Appl pplica 60'	icabl Ible	e			
	UG			MS River Long Distance Sedimer	nt Pip	belin	е		LC)G (of e	BOF	RING	g N	0. I	3-2	6
Fugr	o Consu	Itant	s, Inc.	Jefferson Parish, Louisiana						ect No.	840	05		PI 4	ATE	1.3	3a
L				,					.	200	0.0						

		~	LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION			SHEA	AR S	TREN	GTH	1
DEPTH , FT	WATER LEVEL SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 37' 06.9" W 90° 01' 46.7" SURFACE EL.: -3.5'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢To	netrom rvane eld Van	e	Uno Miniatu R SQ FT	ire Va	xial 🔴
			STRATUM DESCRIPTION		5	й Ъ	0			Ľ	0.			.6 0.8		.0
	-		SILTY CLAY WITH SAND (CL-ML), firm, gray	42.0	-					_						
		N=14		45.0	-	72	32			-						
- 40 -			FAT CLAY (CH), firm, gray, with silt layers	45.0	-					_						
					L					-						
					73		49			-						
-50 -							49			_						
					-					_						
					E		41			-						
					F		58			_						
					È					-						
					-					-						
60				60.0	66		56		L					•		
				00.0	F					-						
					È					-						
	$\left \right $				-					-						
65					F					_						
					-					-						
					È					-						
—70 —	$\left \right $				-					_						
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75					Ĺ					-						
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					Ē					-						
					F					-						
- 80 -					F											
<u>-</u> -					F					-						
	1				[<u> </u>									
NOT										'ION E PTH:		: Aug	gust 2	27, 201	11	
			bols defined on Plates 20a and 20b. e below water surface = 3.4'.							EPTH:		Appl	icable	Э		
	3. WOH :	= Weight	of Hammer.							ER: N			ble			
. 2	4. Push =	Sample	recovered with splitspoon due to low recovery with s	shelby t	ube.					ARY: : Cen			onite (Grout		
										T. Fe			-			
																ĺ
	UGI	RO	MS River Long Distance Sedimer	nt Pip	belin	е		LC)G ()F B	BOR	ING	G NO	Э. E	8-20	6
Fuar	o Consulta	ants, Inc.	Jefferson Parish, Louisiana						ect No.	040	0E			TE	12	≷h
		•						04.	000	840	00		L/-		10	<i>.</i> 0

		~	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHE	AR S	TREN	GTH	1
DEPTH , FT	WATER LEVE SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 37' 04.9" W 90° 02' 32.1" SURFACE EL.: -2.9'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢To	enetrom rvane eld Van	ie	Ur Miniati R SQ F	ure Va	xial 🗨
		ш	STRATUM DESCRIPTION		5	й Ъ	0			H	0			.6 0.8		.0
 		N=WOH	ORGANIC CLAY (OH) , very soft, dark gray, with roots, peat, and shells		-		182 185 208	158	36	- 122 _ -						
			LEAN CLAY (CL), very soft, dark gray, with organics	6.0	60	96	72	44	20	24						
 10			FAT CLAY (CH), very soft to soft, gray, with organics and roots	- 8.0	_		81 169	78	24	54		•				
			- dark gray below 10' ORGANIC CLAY (OH), soft, dark gray, with	- 12.0	-	27	83 119			-						
 			FAT CLAY (CH), very soft, gray, with organics	+ 13.0 + 15.0	53	98	80	86	28	58						
			LEAN CLAY (CL), gray	13.0	-		35			-						
 20 		N=4	- with sand seams at 18.5'		- - -	87	31			-	-					
 25 		N=2			- - - -		41			- - - -	-					
 		N=Push	SILTY SAND (SM), very loose to medium-dense, gray	- 28.0	- - - -	27	27									
 35 	- - -	N=15			- - -	12	22			-	•					
 		N=WOH	LEAN CLAY (CL), very soft, gray	- 38.0	-						-					
	 Terms Depth t WOH = 	o mudline Weight o	ools defined on Plates 20a and 20b. e below water surface = 3.6'. of Hammer. recovered with splitspoon due to low recovery with s	 helby t	[ube.			TOTA CAVE DRY WET BACA	al de Ed de Augi Rot Kfill	TION E PTH: EPTH: ER: N ARY: : Cen T. Fe	60' Not Not Ap 0' to nent-l	Appl oplica 60'	icable	е		
Fugr	UG	20	MS River Long Distance Sedimer	nt Pip	pelin	е		LC)G (of e	BOR	RINC	g No	0. E	3-2	8
Fugr	o Consulta	nts, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05		PLA	ΛTE	14	la

			LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHEA	AR ST	RENG	σтн
DEPTH , FT	WATER LEVEL SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 37' 04.9" W 90° 02' 32.1" SURFACE EL.: -2.9'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢To	netrom rvane eld Van	e	Miniatur	onfined ▼ Triaxial ● e Vane ▲
		Ξ	STRATUM DESCRIPTION		N	PA 20	8 8			<u> </u>	0			R SQ FT 6 0.8	1.0
			LEAN CLAY (CL), very soft, gray		-		31 26	37	19	18	-				
			FAT CLAY (CH), firm, gray, with organics and roots	- 45.0	- - -					-					
- 50 - 					64 		62			-	-				
 55 					- - -	100	50	69	23	46_					
 				- 60.0	- - 71_		49			- - 				•_•	
					-					-					
65 					-					-	-				
- 70 - - 70 -					- - -					-	-				
- · - · 75					- - -					-	•				
 					- - -					-	•				
					- -					-					
	1. Terms 2. Depth 3. WOH :	to mudlin = Weight	bols defined on Plates 20a and 20b. e below water surface = 3.6'. of Hammer. recovered with splitspoon due to low recovery with s	shelby ti	ube.			TOTA CAVI DRY WET BACI	al de Ed de Augi Rot Kfill	TION E PTH: EPTH: ER: N ARY: : Cen T. Fe	60' Not Not Ap 0' to nent-l	Appl oplica 60'	icable ble		1
	UG	20	MS River Long Distance Sedimer	nt Pip	elin	e		LC)G (of e	BOR	INC	g NG). В	-28
Fugr	o Consulta	ants, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05		PLA	TE	14b

		LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHE	AR SI	RENG	στΗ
DEPTH, FT	WATER LEVEL SYMBOL SAMPLES BLOWS PER FOOT	COORDINATES: N 29° 38' 50.8" W 90° 01' 34.3" SURFACE EL.: -1.8'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetrom orvane eld Van	e	Miniatur	onfined ▼ Triaxial ● e Vane ▲
		STRATUM DESCRIPTION		Ŋ	200	8		-	ਛੱ≝			PS PE	R SQ FT 6 0.8	1.0
	 N=WOH	ORGANIC CLAY (OH), very soft, black, with				170			-		.2 0	.4 0.	0 0.8	1.0
		roots - with peat at 2'		-		322	150		-					
5		LEAN CLAY (CL), very soft, gray, with silt seams	4.0	39	98	130 62	152	41	111					
				-		69			-					
		FAT CLAY (CH), soft, gray, with peat and organics	- 8.0	-		00			-					
—10 — 		organioo		- - -		68 97 103	89	30	59_					
		- very soft, with shell fragments at 13'		-		77			-					
—15 — - ·				-		105			-					
				-		49			-					
—20 —				_ 68 -	100	53	54	21	³³ _					
	N=Push			-		50	52	21	- - 31 -					
25 				-					-					
		SILTY SAND (SM), gray	28.0							1				
		SILTT SAIND (SIM), gray		- - - - -	16	21								
_			- 38.0	-					-					
 40		FAT CLAY (CH) , very soft to soft, gray - with silt pockets at 39'		_ 59 _		73 32			-					
	 Terms and symbols Depth to mudling WOH = Weight of 	ools defined on Plates 20a and 20b. e below water surface = 1.9'. of Hammer. recovered with splitspoon due to low recovery with s	 shelby t	ube.	<u> </u>		TOTA CAVE DRY WET BACE	al de Ed de Augi Rot Kfill	TION E EPTH: EPTH: ER: N ARY: .: Cen T. Fe	60' : Not Not Ap 0' to nent-	: Appl oplica 60'	icable ble		1
	UGRO	MS River Long Distance Sedime	nt Pip	belin	е		LC)G (of e	BOR	RINC	9 NC). В	-38
Fugr	ro Consultants, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05		PLA	TE	15a
L		·												

	LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION		5	SHEA	R STI	RENG	TH
DEPTH, FT WATER LEVEL SYMBOL SAMPLES BLOWS PER FOOT	COORDINATES: N 29° 38' 50.8" W 90° 01' 34.3" SURFACE EL.: -1.8' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	UNIT DRY WT. PCF PASSING NO. 200 SIEVE, % WATER			PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦Tor	ld Vane		- Miniature	onfined ▼ Triaxial ● e Vane ▲
	FAT CLAY (CH), soft, gray	42.0							0.:	2 0.4	4 0.6	0.8	1.0
	- with organic traces at 43'		- - - -		44 64			- - - -					
			65 - - -		59			- - - -		•	•		
			- - -		58			-					
	soft to firm below 59'	- 60.0	<u>63</u> _		_64_			- 					
			-					-					
65 			-					-					
 70			_					-					
			-					-					
-75								-					
			-					-					
			-					-					
 Depth to mudlin WOH = Weight 	ools defined on Plates 20a and 20b. e below water surface = 1.9'. of Hammer. recovered with splitspoon due to low recovery with s	helby ti	ube.			TOT/ CAVI DRY WET BACI	al de Ed de Augi Rot Kfill	TON E PTH: EPTH: ER: N ARY: : Cen T. Fe	60' Not lot Ap 0' to 0 nent-E	Appli plical 60'	cable ble		1
FUGRO	MS River Long Distance Sedimer	nt Pip	elin	е		LC)G (of B	BOR	ING	6 NO). В [.]	-38
Fugro Consultants, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05	F		TE	15b

L Under Note See Fraits 1 W 00 20 56 * Visit 1 W 00			-	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHEA	AR S	FRENC	STH	
New OR ORGANIC CLAY (OH, very soft, Biack, with rots and grass, grass, and grass,	DEPTH, FT	WATER LEVE SYMBOL SAMPLES	BLOWS PEF FOOT	W 90° 02' 05.6" SURFACE EL.: -1.5'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢To	rvane eld Van	e	Miniatu	Triaxia re Van	al 🜒
Nervice roots and grass 2.0 338 232 64 168								101				0	.2 0	.4 0.	6 0.8	1.0	
1 Point (P1) (gray), with organics, grass, and points, grass, grass, and points, grass, grass, and points, grass, gras, grass, gras, grass, grass, grass, grass,	_		N=WOR	roots and grass	2.0	-		191									
10	-	$= \frac{\sqrt{\sqrt{2}}}{\sqrt{2}}$				-		338	232	64	168 - -						
-10 -with silt fraces and shells from 12 to 19' - dark gray from 14' to 16' -gray below 16' - gray below 16' -with organics at 18' -20 -with organics at 18' -20 -with silt layers below 28' -30 -soft, with silt layers below 28' -30 -soft, with silt layers below 28' -31 -soft, with silt layers below 28' -32 -soft, with silt layers below 28' -33 -soft, with silt layers below 28' -34 -soft, with silt layers below 28' -35 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -37 -soft, with silt layers below 28' -38 -soft, with silt layers below 28' -39 -soft, with silt layers below 28' -30 -soft, with silt layers below 28' -40 -soft, with silt layers below 28' -53	- 5 -			FAT CLAY (CH), very soft, gray, with peat	- 5.0	-		55			-						
- with silt races and shells from 12' to 19' - 48 99 88 82 26 56 - - dark gray from 14' to 16' - gray below 16' - 96 96 97 - - - 20 - with organics at 18' - 96 97 - - - - 20 - - - 97 105 28 77 - - 20 - - - 53 82 - - - - 20 - - - 53 82 - - - - 20 - - - 53 82 - - - - 25 -	- - - 10 -					- - -											
- dark gray from 14' to 15' - dark gray from 14' to 15' - gray below 16' - with organics at 18' - with organics at 18' - 63 - as oft, with silt layers below 28' - 53 - 36 - 50, with silt layers below 28' - 36 - 67 - 36 - 53 - 400 - 60 - 53 82 - 53 82 - 53 82 - 53 82 - 78 - 67 - 78 - 67 - 78 - 67 - 78 - 67 - 78 - 67 - 78 - 67 - 78 - 67 - 78 - 78 - 78 - 78 - 78 - 78 - 78 - 78 - 78 - 78 - 78 - 78 - 79 - 78 - 79 - 78 - 70 - 78 - 90 - 77 - 90 - 78 - 90 - 77 - 90 - 78	-					_		80			-	▲					
	-	- //		- with silt traces and shells from 12' to 19'		48	99	88	82	26	56						
- gray below 16' - with organics at 18' - soft, with sill layers below 28' - soft, with soft below 28' - soft below 28' - soft b	- —15 -			- dark gray from 14' to 16'						20							
- with organics at 18' - with organics at 18' - with organics at 18'	E			- gray below 16'		F		96			-						
20 Image: Second Se	-	- //		- with organics at 18'		-			105	28	77	▲					
Soft, with silt layers below 28' -soft, with silt layers below 28' -soft, with silt layers below 28' -30 -soft, with silt layers below 28' -30 -soft, with silt layers below 28' -35 -soft, with silt layers below 28' -35 -soft, with silt layers below 28' -35 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -37 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -37 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -40 -soft, with silt layers below 28' -40 -soft, with silt layers below 28' -53 82 -40 -soft, with silt layers below 28' -53 -53 -54 -57 -57 -57 -57 -57 -57	- —20 -			, i i i i i i i i i i i i i i i i i i i		-											
Soft, with silt layers below 28' -soft, with silt layers below 28' -soft, with silt layers below 28' -30 -soft, with silt layers below 28' -30 -soft, with silt layers below 28' -35 -soft, with silt layers below 28' -35 -soft, with silt layers below 28' -35 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -37 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -37 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -40 -soft, with silt layers below 28' -40 -soft, with silt layers below 28' -53 82 -40 -soft, with silt layers below 28' -53 -53 -54 -57 -57 -57 -57 -57 -57	E					-					-						
Soft, with silt layers below 28' -soft, with silt layers below 28' -soft, with silt layers below 28' -30 -soft, with silt layers below 28' -30 -soft, with silt layers below 28' -35 -soft, with silt layers below 28' -35 -soft, with silt layers below 28' -35 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -37 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -37 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -36 -soft, with silt layers below 28' -40 -soft, with silt layers below 28' -40 -soft, with silt layers below 28' -53 82 -40 -soft, with silt layers below 28' -53 -53 -54 -57 -57 -57 -57 -57 -57	-					-					-						
30 53 82 1 1 35 61 78 61 1 40 40.0 60 67 1 40 40.0 60 67 1 1 Terms and symbols defined on Plates 20a and 20b. 2. Depth to mudline below water surface = 2.1'. 2. Weight of Rod. 3. WOR = Weight of Rod. 4. Push = Sample recovered with splitspoon due to low recovery with shelby tube. COMPLETION DATE: August 25, 2011 TOTAL DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 40' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-40	- 25 -		N=Push			-		53			-	1					
30 53 82 1 1 35 61 78 61 1 40 40.0 60 67 1 40 40.0 60 67 1 1 Terms and symbols defined on Plates 20a and 20b. 2. Depth to mudline below water surface = 2.1'. 2. Weight of Rod. 3. WOR = Weight of Rod. 4. Push = Sample recovered with splitspoon due to low recovery with shelby tube. COMPLETION DATE: August 25, 2011 TOTAL DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 40' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-40	E					-					-						
30 53 82 1 1 35 61 78 61 1 40 40.0 60 67 1 40 40.0 60 67 1 1 Terms and symbols defined on Plates 20a and 20b. 2. Depth to mudline below water surface = 2.1'. 2. Weight of Rod. 3. WOR = Weight of Rod. 4. Push = Sample recovered with splitspoon due to low recovery with shelby tube. COMPLETION DATE: August 25, 2011 TOTAL DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 40' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-40	-			- soft, with silt layers below 28'		-					-						
-35 -35 -40 -61 -40 -61 -40 -61 -40 -61 -40 -60 -67 -40 -40 -60 -67 -40 -40 -60 -67 -40 -40 -60 -67 -40 -60 -67 -40 -60 -67 -60 -67 -60 -67 -60 -67 -60 -67 -7	- 					53		82			-	1	-				
-35 -35 -40 -61 -40 -61 -40 -61 -40 -61 -40 -60 -67 -40 -40 -60 -67 -40 -40 -60 -67 -40 -40 -60 -67 -40 -60 -67 -40 -60 -67 -60 -67 -60 -67 -60 -67 -60 -67 -7	-					-					-						
-35 -35 -40 -61 -40 -61 -40 -61 -40 -61 -40 -60 -67 -40 -40 -60 -67 -40 -40 -60 -67 -40 -40 -60 -67 -40 -60 -67 -40 -60 -67 -60 -67 -60 -67 -60 -67 -60 -67 -7	-					-		78			-						
40 40.0 NOTES: 1. Terms and symbols defined on Plates 20a and 20b. 2. Depth to mudline below water surface = 2.1'. COMPLETION DATE: August 25, 2011 3. WOR = Weight of Rod. TOTAL DEPTH: Not Applicable 4. Push = Sample recovered with splitspoon due to low recovery with shelby tube. DRY AUGER: Not Applicable WET ROTARY: 0' to 40' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-40	- 					-					-	1	•				
40 40.0 NOTES: 1. Terms and symbols defined on Plates 20a and 20b. 2. Depth to mudline below water surface = 2.1'. COMPLETION DATE: August 25, 2011 3. WOR = Weight of Rod. TOTAL DEPTH: Not Applicable 4. Push = Sample recovered with splitspoon due to low recovery with shelby tube. DRY AUGER: Not Applicable WET ROTARY: 0' to 40' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-40	; - -					-					-						
40 40.0 NOTES: 1. Terms and symbols defined on Plates 20a and 20b. 2. Depth to mudline below water surface = 2.1'. COMPLETION DATE: August 25, 2011 3. WOR = Weight of Rod. TOTAL DEPTH: Not Applicable 4. Push = Sample recovered with splitspoon due to low recovery with shelby tube. DRY AUGER: Not Applicable WET ROTARY: 0' to 40' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-40	-					-					-						
NOTES. 1. Terms and symbols defined on Plates 20a and 20b. TOTAL DEPTH: 40' 2. Depth to mudline below water surface = 2.1'. WOR = Weight of Rod. CAVED DEPTH: Not Applicable 3. WOR = Weight of Rod. WET ROTARY: 0' to 40' BACKFILL: Cement-Bentonite Grout 4. Push = Sample recovered with splitspoon due to low recovery with shelby tube. WET ROTARY: 0' to 40' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro Image: MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-40 Project No. Project No.	- 40 -				40.0	60	<u> </u>	_67_				L	• •		+	_+	
NOTES. 1. Terms and symbols defined on Plates 20a and 20b. TOTAL DEPTH: 40' 2. Depth to mudline below water surface = 2.1'. WOR = Weight of Rod. CAVED DEPTH: Not Applicable 3. WOR = Weight of Rod. WET ROTARY: 0' to 40' BACKFILL: Cement-Bentonite Grout 4. Push = Sample recovered with splitspoon due to low recovery with shelby tube. WET ROTARY: 0' to 40' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro Image: MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-40 Project No. Project No.	-					-					-						
Project No.		 Terms a Depth t WOR = 	o mudline Weight	e below water surface = 2.1'. of Rod.	helby t	ube.			TOTA CAVE DRY WET BACA	al de Ed de Augi Rot Kfill	EPTH: EPTH ER: N ARY: .: Cer	40' Not Not Ap 0' to nent-l	Appl oplica 40'	icable ble	9	1	
	·	Fugi	20	MS River Long Distance Sedimer	nt Pip	elin	е		LC	G C	of e	BOR		S NO	О. В	-40)
	Fug								Deci	ot N-							
	Fug	ro Consulta	nts, Inc.	Jefferson Parish, Louisiana								05		PL	ATE	1	6

			~	LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION			SHE	AR ST	RENG	στΗ
DEPTH, FT	WATER LEVEI SYMBOL		BLOWS PER FOOT	COORDINATES: N 29° 37' 25.7" W 90° 02' 50.8" SURFACE EL.: -2.5'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢⊺o	netrom rvane eld Van	e	Miniatur	onfined ▼ Triaxial ● e Vane ▲
	$ \mathbf{S} $		ш	STRATUM DESCRIPTION		Ň	20 20	Ŭ			₫ –	0			R SQ FT 6 0.8	1.0
		Xn=	=WOH	PEAT (PT), very soft, black		-		378			_		_			
		 N:	=Push			-		221			-					
- 5 -		Xn:	=Push	FAT CLAY (CH), dark gray	4.0	_		115	68	20	48 -					
	<u><u> </u></u>	/ \		PEAT (PT), very soft, dark gray	- 6.0											
- ·						- - -		240			- - -					
	1/ 1/				- 13.0	_		250	295	77	218					
				FAT CLAY (PT), very soft, gray, with organics	13.0	_		65			-					
—15 —						-		97			-	▲				
						-		89			-					
F .						F		82			_					
						- -		02			-					
Ŀ					- 23.0	_					-					
				LEAN CLAY (CL), very soft to soft, gray, with silt layers	- 23.0	62	99	62	37	17	20			•		
- · · 30 - ·		× N=	=WOR			- - - -		65			- - - -					
				FAT CLAY (CH), soft to firm, gray	- 34.0	56		75								
- 35 – 				TAT OLAT (OI), solt to limit, gray		- 50		/5			-		AO			
						-		36 32			-		•			
	1. Term 2. Depth 3. WOH 4. WOR	to = V = V	mudline Veight Veight	ools defined on Plates 20a and 20b. e below water surface = 3.0'. of Hammer. of Rod. recovered with splitspoon due to low recovery with s	 shelby t	ube.	<u> </u>		TOTA CAVI DRY WET BACI	al de Ed de Augi Rot, Kfill	TION E PTH: EPTH: ER: N ARY: : Cen T. Fe	60' Not Iot Ap 0' to nent-l	Appl oplica 60'	icable ble		1
	UG	\vdots		MS River Long Distance Sedime	nt Pip	elin	е		LC)G (of e	BOR	RING	9 NG	Э. В	-41
Fugr	o Consul	tants	s, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05		PLA	TE	17a

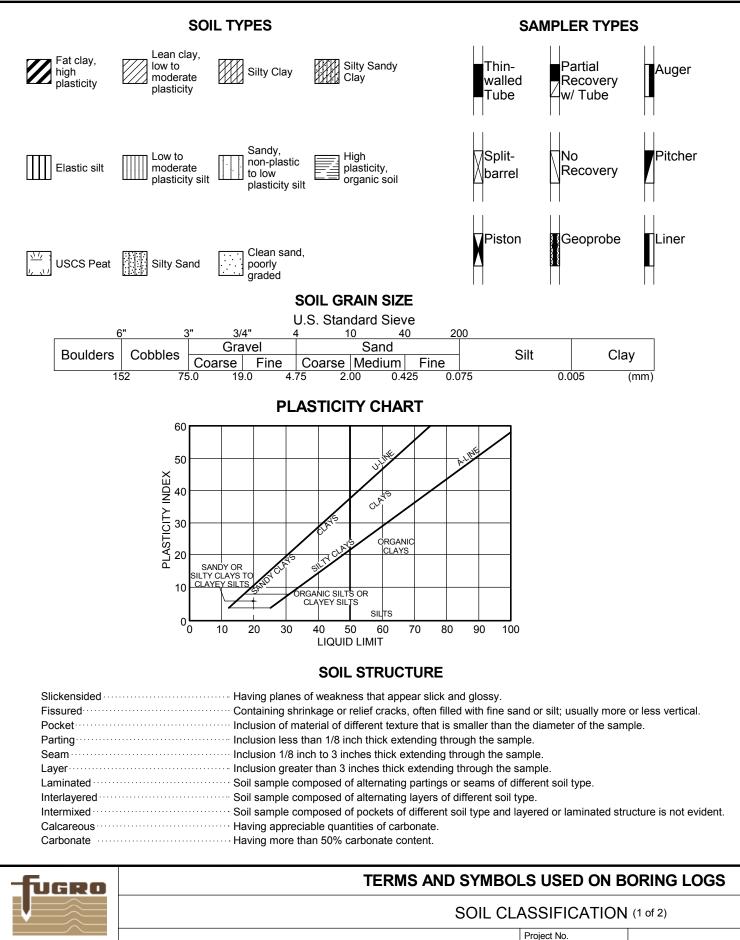
FCBR_LOG (FINAL) 0 TO 1_04 55084005.GPJ_FUGRO DATA TEMPLATE 042610.GDT_11/16/11

			LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHE	AR S	TREN	GTH	
DEPTH, FT	WATER LEVE SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 37' 25.7" W 90° 02' 50.8" SURFACE EL.: -2.5' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	⇔ To △ Fie		e IPS PE	Miniatu R SQ F1	г	ial ● ne ▲
			FAT CLAY (CH), soft to firm, gray								0.	.2 0	.4 0	.6 0.8	1.0	0
 45 					- - 85 - -		34 60			- - - - -		•	•			
50 - 					- - - _ 73		51 49						•			
- · · - · · - 60 -				- 60.0	- - - -		55 67			- - - - -				• +		
 65 					- - - -											
					- - - -											
					- - - -					-						
	1. Terms 2. Depth 3. WOH : 4. WOR :	to mudlin = Weight = Weight	ools defined on Plates 20a and 20b. e below water surface = 3.0'. of Hammer. of Rod. recovered with splitspoon due to low recovery with s	 helby tu	ube.			TOT/ CAVI DRY WET BACI	al de Ed de Augi Rot Kfill	ION E PTH: EPTH: ER: N ARY: : Cen T. Fe	60' Not Iot Ap 0' to nent-l	Appl oplica 60'	icabl Ible		11	
	ŪG	20	MS River Long Distance Sedimer	nt Pip	elin	е					BOR		g N	0. E	8-41	1
Fugr	o Consulta	ints, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05		PLA	ΛTE	17	b

	_	Ļ				LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHE	AR S	TREN	GTH	1
DEPTH , FT			SAMPLES		FOOT	COORDINATES: N 29° 36' 50.4" W 90° 03' 34.5" SURFACE EL.: -2.8'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetrom orvane eld Van		Un Miniati		xial 🔴
	11/1				5	STRATUM DESCRIPTION			PAS 200	> õ		Ч	ΞΞ				R SQ F		
	-	1	z N	NI_1	NOR	PEAT (PT) , very soft, black, with roots				748				0	.2 0	.4 0	.6 0.8	3 1	.0
		<u>v</u> <u>v</u> <u>v</u>			, i ci c	- with wood pieces below 4' - soft at 7' - dark gray below 8'		-		215	242	68	- - 174_ - - - -						
	_		<u>、) /</u>					24	83	222	150	40	110						
	-	<u>v</u>	<u>'</u> :			- with sand pockets below 12'	100	- 24	83	223	159	40	119						
- · ·	_					LEAN CLAY (CL), very soft, dark gray, with sand pockets	- 13.0	-		33			-						
	-	H				FAT CLAY (CH), very soft to soft, gray	+ 16.0			35									
	-							- - - -		98 77 72	66	23	43 _						
				N=	Push			- - - 54		84					•				
- · ·	-							- - -		73 91									
							- 40.0	_ <u>57</u> _		_75_			- - 	 	A •				
	1. 2. 3.	Te De Wo	pth 1 DR =	to m = W	nudlin eight	bols defined on Plates 20a and 20b. e below water surface = 3.3'. of Rod. recovered with splitspoon due to low recovery with	shelby t	ube.			TOTA CAVE DRY WET BACE	al de Ed di Aug Rot Kfill	TION E EPTH: EPTH: ER: N TARY: .: Cen T. Fe	40' : Not Not Ap 0' to nent-	: Appl oplica 40'	icable Ible	9	11	
	F	J	Ŀ	: .		MS River Long Distance Sedime	nt Pip	belin	е		LC)G (of e	BOR	RINC	G NO	O. E	3-4	2
Fugr	ro (Con	sulta	nts,	Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05		PL	.ATE	Ξ 1	8

Line Line COORDINATES: N 297 297 397 397 397 397 397 397 397 397 397 3					LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHE/	AR S	TREN	GTH	
STRATUM DESCRIPTION D	ОЕРТН, FT	ATER LEVE	SYMBUL	LOWS PEF FOOT	COORDINATES: N 29° 36' 32.9" W 90° 03' 34.7"	STRATUM DEPTH, FT	IT DRY WT, PCF	SSING NO. 0 SIEVE, %	WATER DNTENT, %	LIQUID	PLASTIC LIMIT	LASTICITY NDEX (PI)	♦To	ervane eld Van	e	Miniatu	Triaxia ire Van	al 🔴
122 N=Push PEAT (FT), very soft, dark gray and black, with organics and roots 379 379 379 -5 -5 -5 -61 -61 - -10 - - - 61 - -10 - - 61 - - -10 - - - 61 - - -10 - - - - - - - -10 - - - - - - - - -10 - <		Ś		В	STRATUM DESCRIPTION		Ŋ	20 20	8			= =						
-5 - LEAN CLAY (CL), soft to firm, gray, with organics and wood 4.0 25 63 518 203 55 148 - - - - - 61 -		- <u>``</u>	— 1XI	N=Push	PEAT (PT) , very soft, dark gray and black, with organics and roots		-		379			_		.2 0	.4 0	.6 0.6	1.0	_
-5 organics and wood - 61 -			<u></u> 			40	25	63		203	55	148						
FAT CLAY (CH), soft to firm, gray, with organics and wood 8.0 106 88 36 52 - with shell fragments at 14' - with shell fragments at 14' 15.0 94	- 5 -				LEAN CLAY (CL), soft to firm, gray, with organics and wood	4.0	-		61			-						
10					FAT CLAY (CH) soft to firm grav with	8.0			40									
-15 	 						- - -		64	88	36	52	-					
-20 - 153 - - - -20 - - 171 - - -20 - - - - - - -20 - - - - - - - -20 - - - - - - - - -20 -						15.0	-		94			-						
-20 - - 171 - <td></td> <td>┨╞</td> <td></td> <td></td> <td></td> <td>- 15.0</td> <td>_</td> <td></td> <td>153</td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>		┨╞				- 15.0	_		153			-						
-20 FAT CLAY (CH), very soft to soft, gray 20.0 -25 67 62 22 40 -25 - 67 62 22 40 -30 - 78 - - - -30 - - - - - - -30 - - - - - - - -30 - - - - - - - - -30 - <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td><td>171</td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td></t<>							-		171			-						
N=Push -25	- 20 -		7		FAT CLAY (CH), very soft to soft, grav	- 20.0	31	73	156	200	52	148						
-25 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -							-					-						
	 25		X	N=Push			-		67	62	22	40 -						
				N-Duch			-		70			-						
	—30 —			IN-FUSII			-		70			-	-					
							55		77			-		•				
Image: Project No. Image: Project No. Image: Project							-					-						
NOTES: 1. Terms and symbols defined on Plates 20a and 20b. COMPLETION DATE: August 28, 2011 2. Depth to mudline below water surface = 3.0'. TOTAL DEPTH: Not Applicable 3. Push = Sample recovered with splitspoon due to low recovery with shelby tube. DRY AUGER: Not Applicable WET ROTARY: 0' to 60' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-43	 						-					-	-					
2. Depth to mudline below water surface = 3.0'. 3. Push = Sample recovered with splitspoon due to low recovery with shelby tube. CAVED DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 60' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-43 Fugre Consultants, Inc. Lefferson Parish Louisiana	NOT		erms	and syml	bols defined on Plates 20a and 20b.		-			тот	AL DE	EPTH:	60'		-		11	
Fugre Consultants, Inc. MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-43						shelby t	ube.			DRY WET BACI	AUGI ROT KFILL	ER: N ARY: .: Cen	lot Ap 0' to nent-	oplica 60'	ble			
Fugre Consultants, Inc. MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-43 Fugre Consultants, Inc. Infferson Parish, Louisiana Project No. DIATE 100	5555 E																	
Fugre Consultants, Inc. Afferson Parish Quisiana Project No.		Ū	GI	20	MS River Long Distance Sedime	nt Pip	elin	е		LC)G (of e	Bor	RINC	g No	0. E	8-43	
Fugro Consultants, Inc. Jefferson Parish, Louisiana 04.55084005 PLATE 19a	Fugr	o Cor	nsulta	nts, Inc.	Jefferson Parish, Louisiana								05		PLA	TE	19a	 a

		~	LOCATION: See Plate 1								SHEAR STRENGTH						
DEPTH , FT	WATER LEVE SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 36' 32.9" W 90° 03' 34.7" SURFACE EL.: -2.6'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	¢⊺o	enetrom irvane eld Van			onfined ▼ Triaxial ● e Vane ▲		
	AN C	BL	STRATUM DESCRIPTION	ΩΞ	UNIT	PAS 200	S 20		д_			к	IPS PE	R SQ FT			
			FAT CLAY (CH), very soft to soft, gray								0	.2 0	.4 0	.6 0.8	1.0		
			- with silt layers below 53'		- 55 - 55 		74 61 61 73 72					•	•				
 				60.0	-		63 69			-							
	1. Terms 2. Depth	to mudlin	bols defined on Plates 20a and 20b. e below water surface = 3.0'. recovered with splitspoon due to low recovery with s	shelby ti	ube.			TOTA CAVI DRY WET BACI	al de Ed de Augi Rot, Kfill	ION E PTH: EPTH: ER: N ARY: : Cen T. Fe	60' Not lot Ap 0' to nent-l	Appl oplica 60'	icable Ible		1		
	ŪG	RO	MS River Long Distance Sedimer	nt Pip	elin	e		LC	G C	OF B	BOR	RINC	G NO	0. B	-43		
Fugr	o Consult	ants, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05		PLA	TE	19b		



Fugro Consultants, Inc.

04.55084005 | PLATE 20a

STANDARD PENETRATION TEST (SPT)

A 2-in.-OD, 1-3/8-ID split spoon sampler is driven 1.5 ft into undisturbed soil with a 140-pound hammer free falling 30 in. After the sampler is seated 6 in. into undisturbed soil, the number of blows required to drive the sampler the last 12 in. is the Standard Penetration Resistance or "N" value, which is recorded as blows per foot as described below.

SPLIT-BARREL SAMPLER DRIVING RECORD

NOTE: To avoid damage to sampling tools, driving is limited to 50 blows during or after seating interval.

DENSITY OF GRANULAR SOILS

Descriptive Term	*Relative Density, %	**Blows Per Foot (SPT)	Term	Undrained Shear Strength, ksf	Blows Per Foot (SP (approximate)
Very Loose	< 15	·····0 to 4	Very Soft	·····< 0.25 ·····	·····0 to 2
Loose	······15 to 35 ·····	·····5 to 10	Soft	······0.25 to 0.50 ······	······2 to 4
Medium Dense ····	······-35 to 65 ·····	······11 to 30	Firm	0.50 to 1.00	·····4 to 8
Dense	······65 to 85 ·····	······31 to 50	Stiff ·····	······1.00 to 2.00 ······	······8 to 16
Very Dense	· · · · · · > 85 · · · ·	> 50	Very Stiff ·····	······2.00 to 4.00 ······	······16 to 32
-			Hard	> 1 00	> 32

*Estimated from sampler driving record.

Blows Per Foot

**Requires correction for depth, groundwater level, and grain size.

STRENGTH OF COHESIVE SOILS

Description

Term	Undrained Shear Strength, ksf	Blows Per Foot (SPT) (approximate)
Very Soft ······	< 0.25	······0 to 2
Soft	0.25 to 0.50	·····2 to 4
Firm	······0.50 to 1.00 ······	·····4 to 8
Stiff ·····	······1.00 to 2.00 ······	······8 to 16
Very Stiff ······	·····2.00 to 4.00 ······	······16 to 32
Hard ·····	·····> 4.00 ······	> 32

SHEAR STRENGTH TEST METHOD

U = Unconfined Q = Unconsolidated - Undrained Triaxial

P = Pocket Penetrometer T = Torvane V = Miniature Vane F = Field Vane

HAND PENETROMETER CORRECTION

Our experience has shown that the hand penetrometer generally overestimates the in-situ undrained shear strength of over consolidated Pleistocene Gulf Coast clays. These strengths are partially controlled by the presence of macroscopic soil defects such as slickensides, which generally do not influence smaller scale tests like the hand penetrometer. Based on our experience, we have adjusted these field estimates of the undrained shear strength of natural, overconsolidated Pleistocene Gulf Coast soils by multiplying the measured penetrometer reading by a factor of 0.6. These adjusted strength estimates are recorded in the "Shear Strength" column on the boring logs. Except as described in the text, we have not adjusted estimates of the undrained shear strength for projects located outside of the Pleistocene Gulf Coast formations.

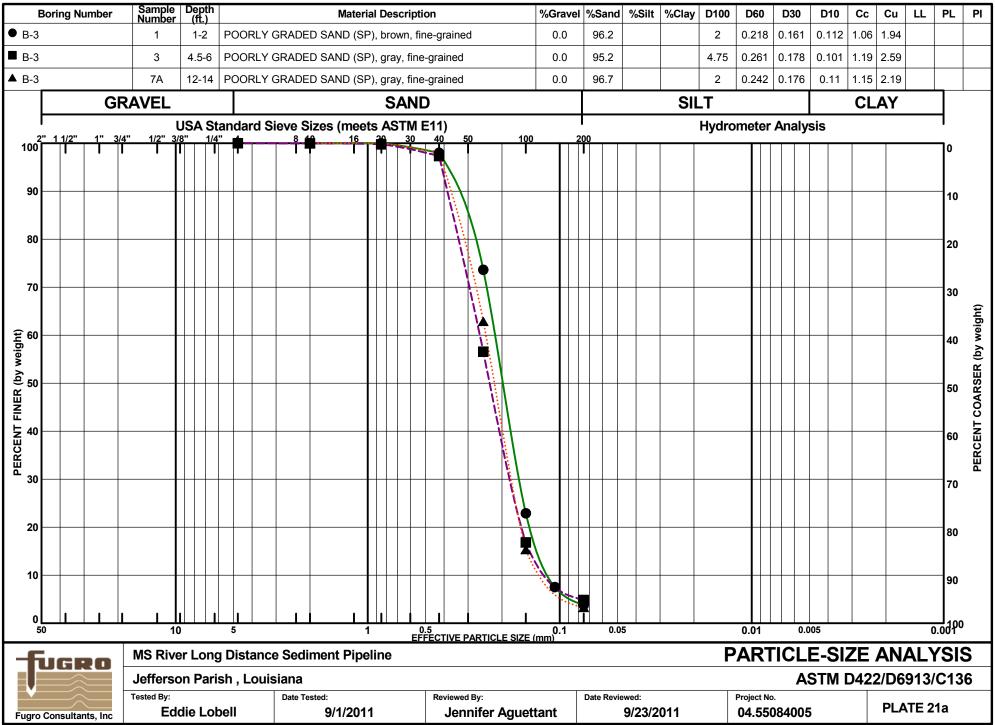
Information on each boring log is a compilation of subsurface conditions and soil or rock classifications obtained from the field as well as from laboratory testing of samples. Strata have been interpreted by commonly accepted procedures. The stratum lines on the logs may be transitional and approximate in nature. Water level measurements refer only to those observed at the time and places indicated, and can vary with time, geologic condition, or construction activity.



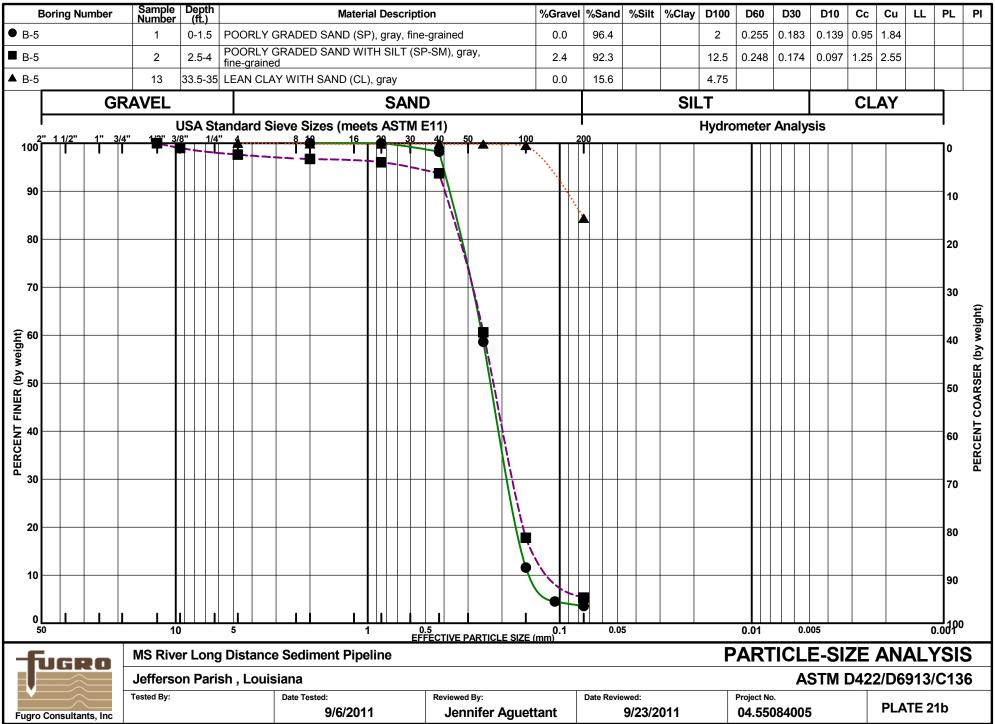
TERMS AND SYMBOLS USED ON BORING LOGS

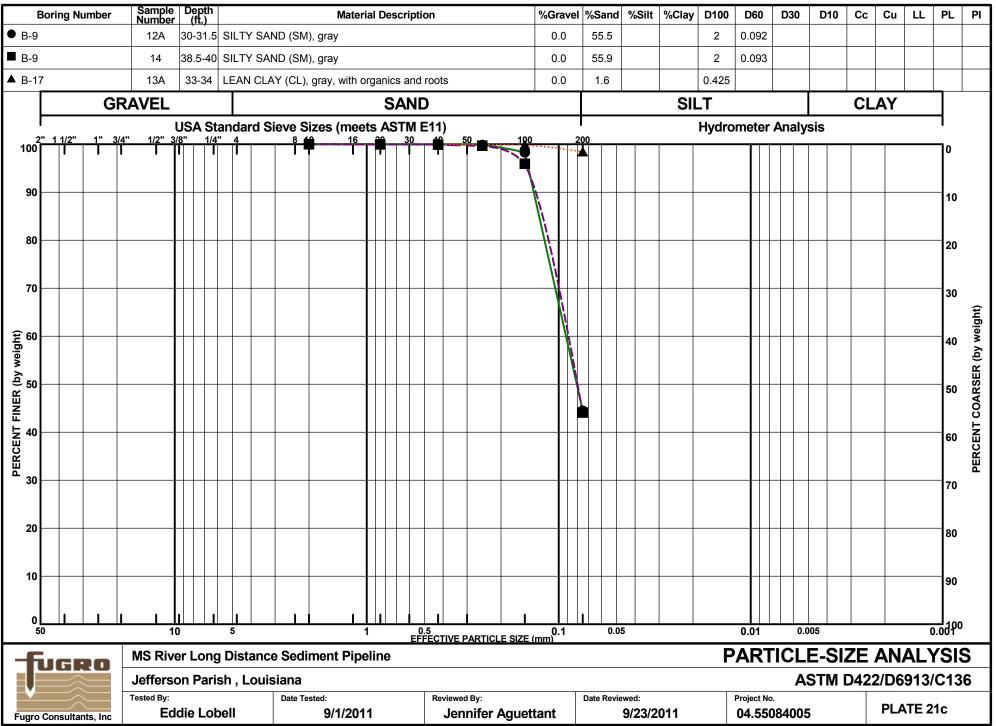
SOIL CLASSIFICATION (2 of 2)

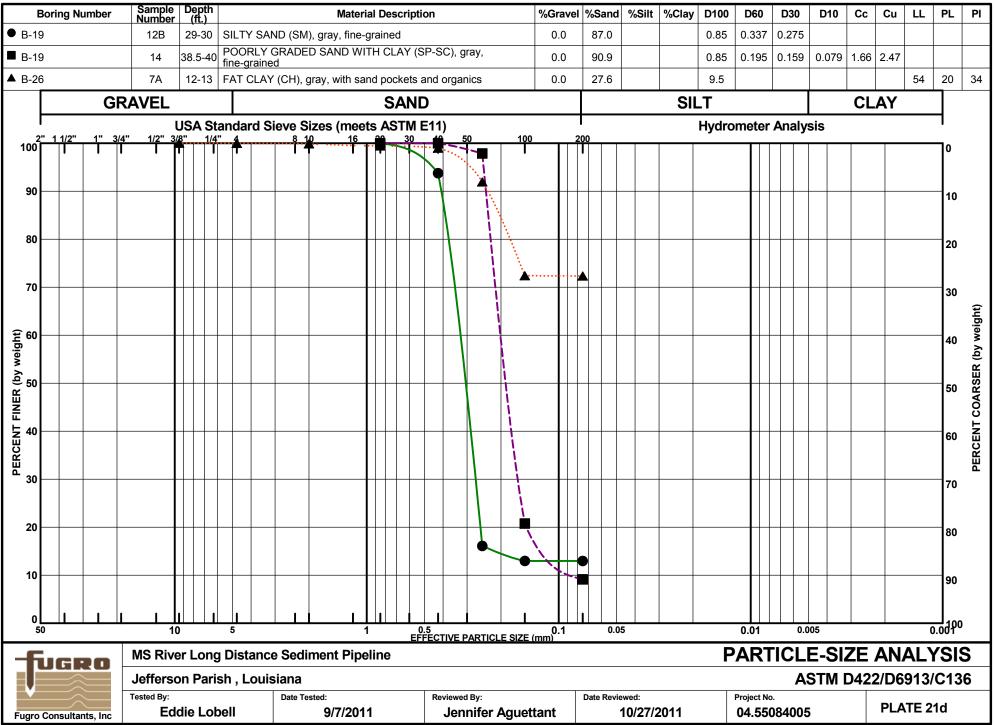
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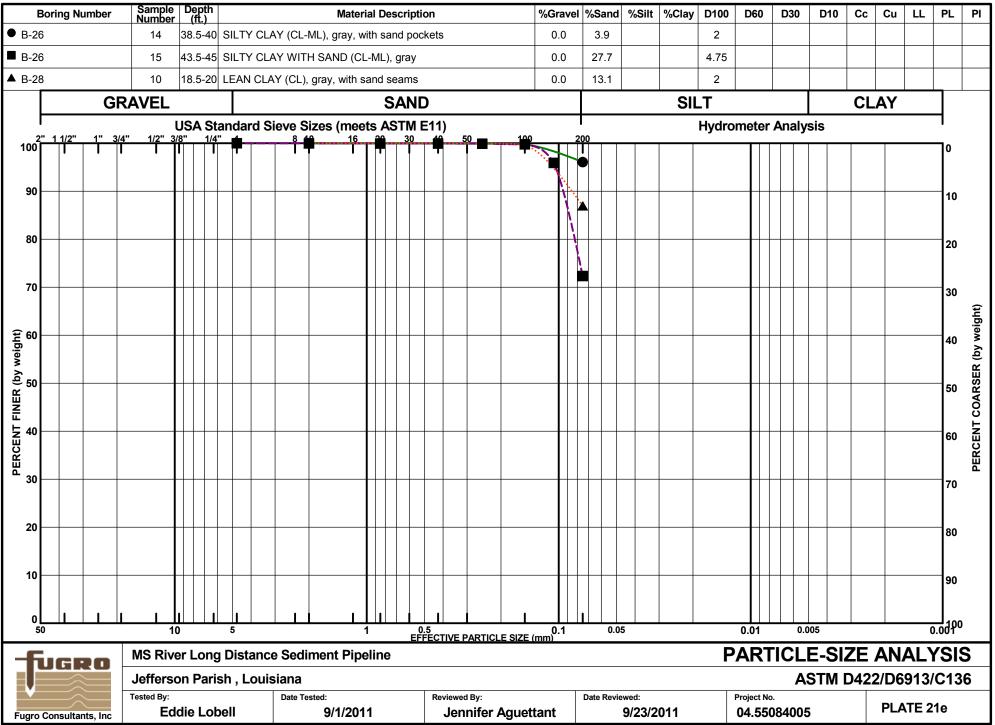


FCBR GSA LANDSCAPE 04.55084005.GPJ FUGRO DATA TEMPLATE 042610.GDT 11/16/11

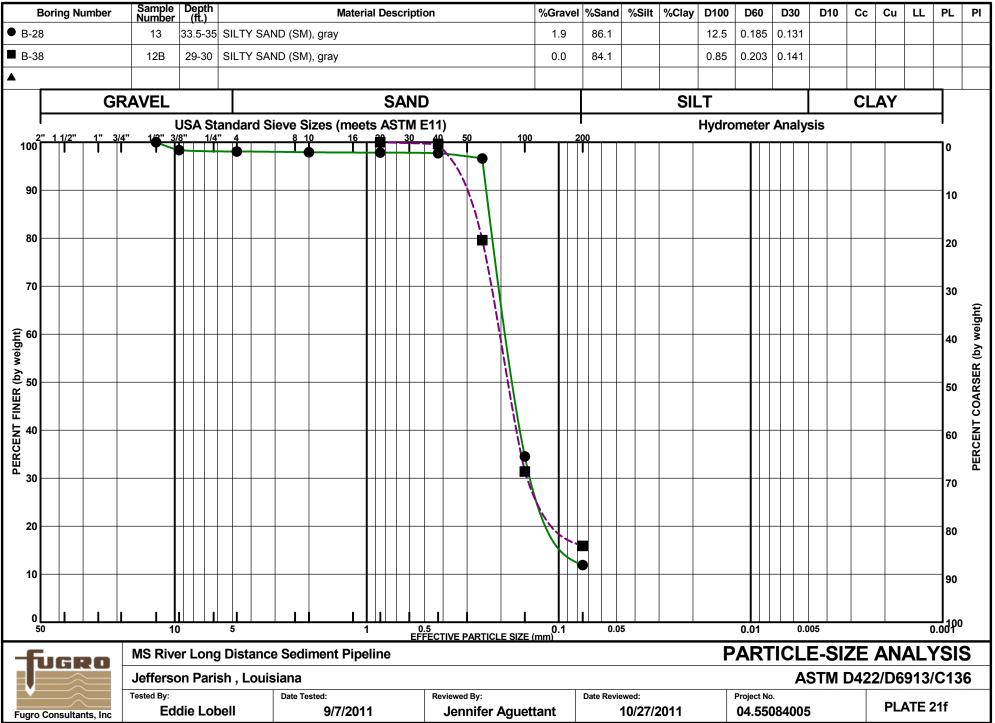




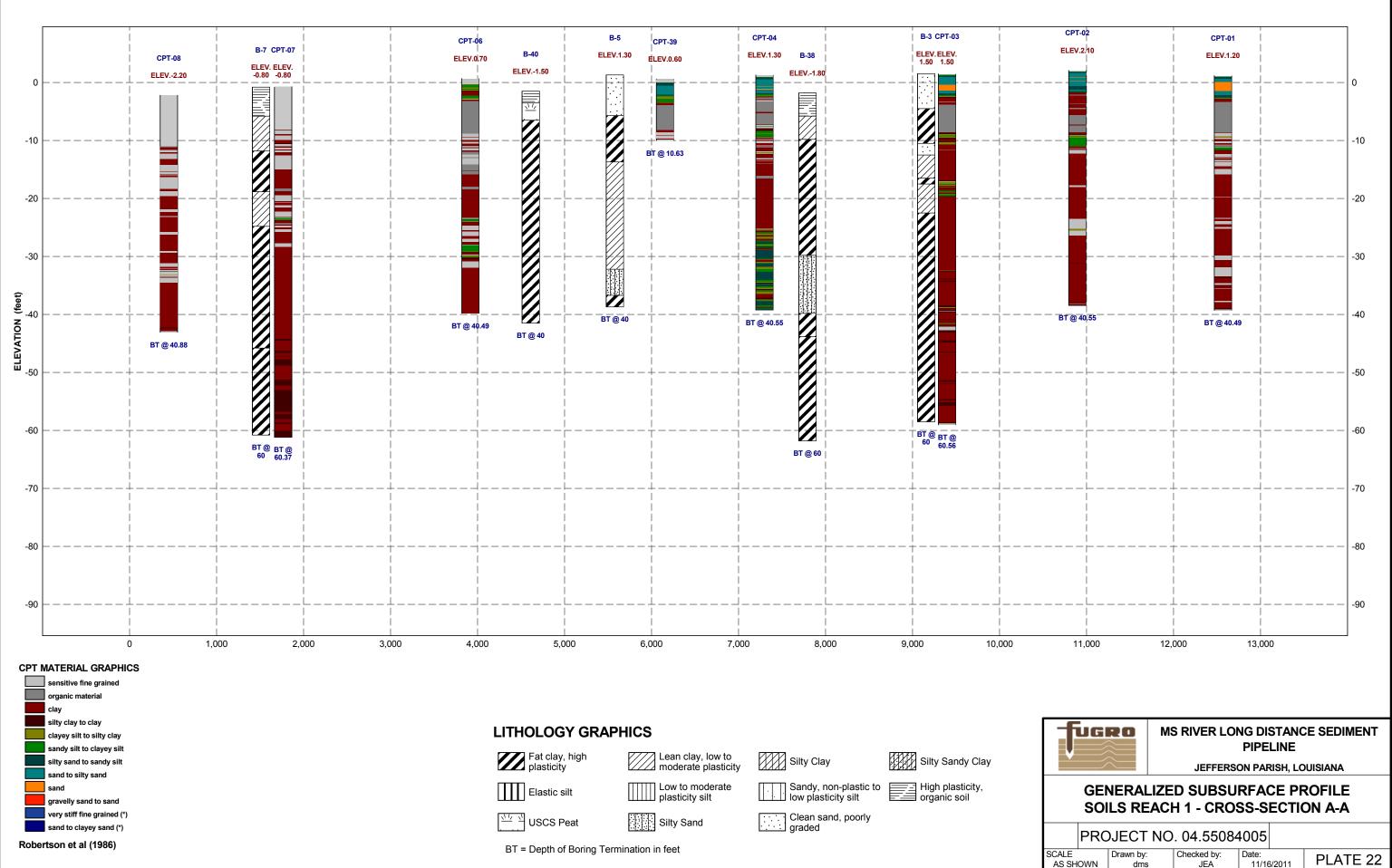


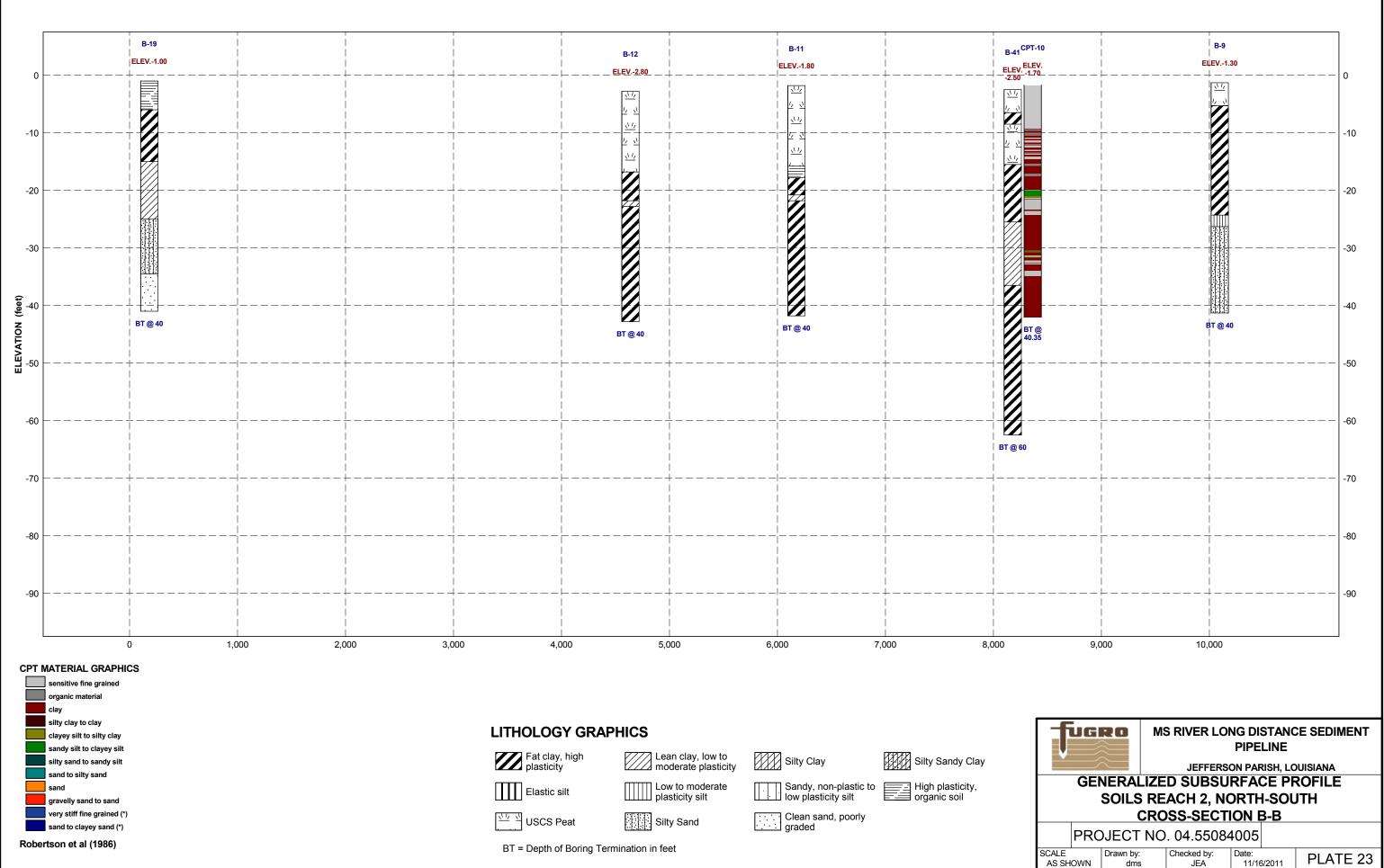


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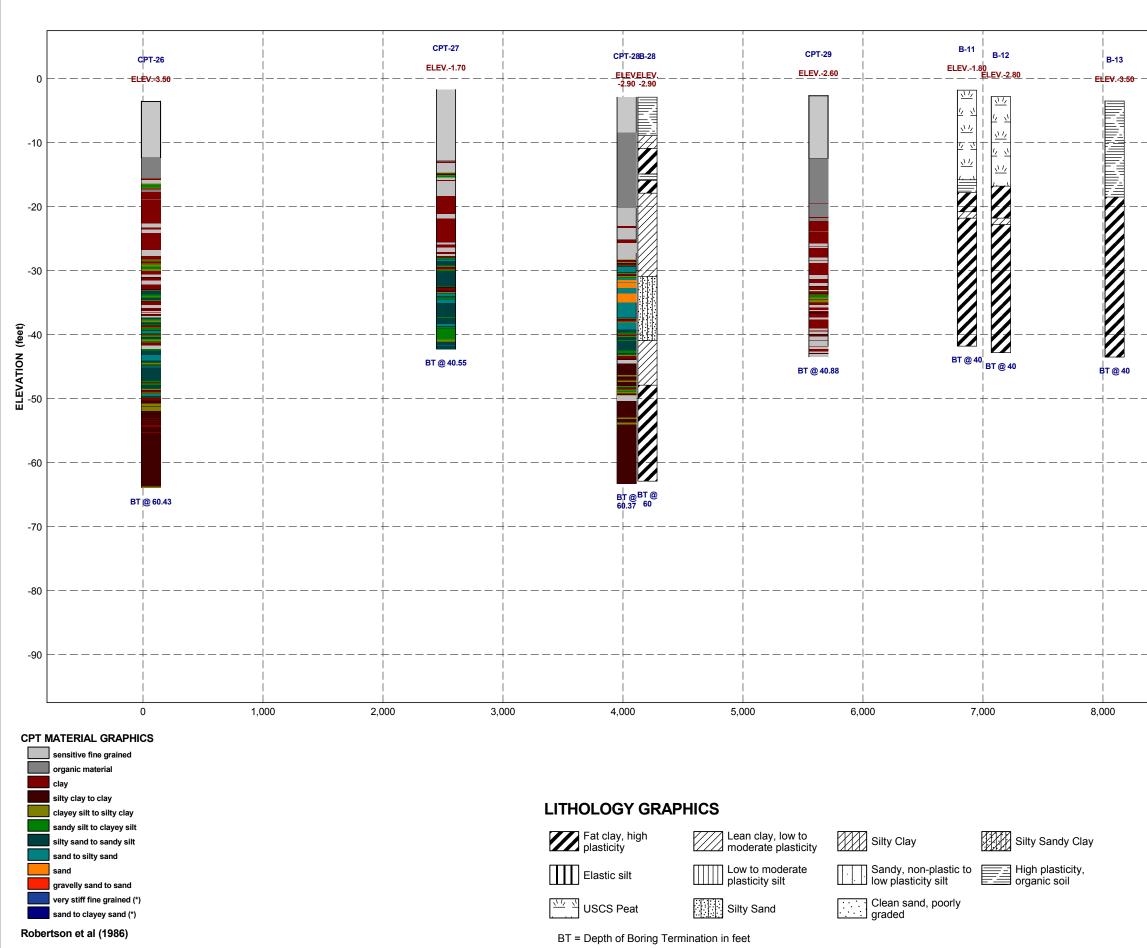


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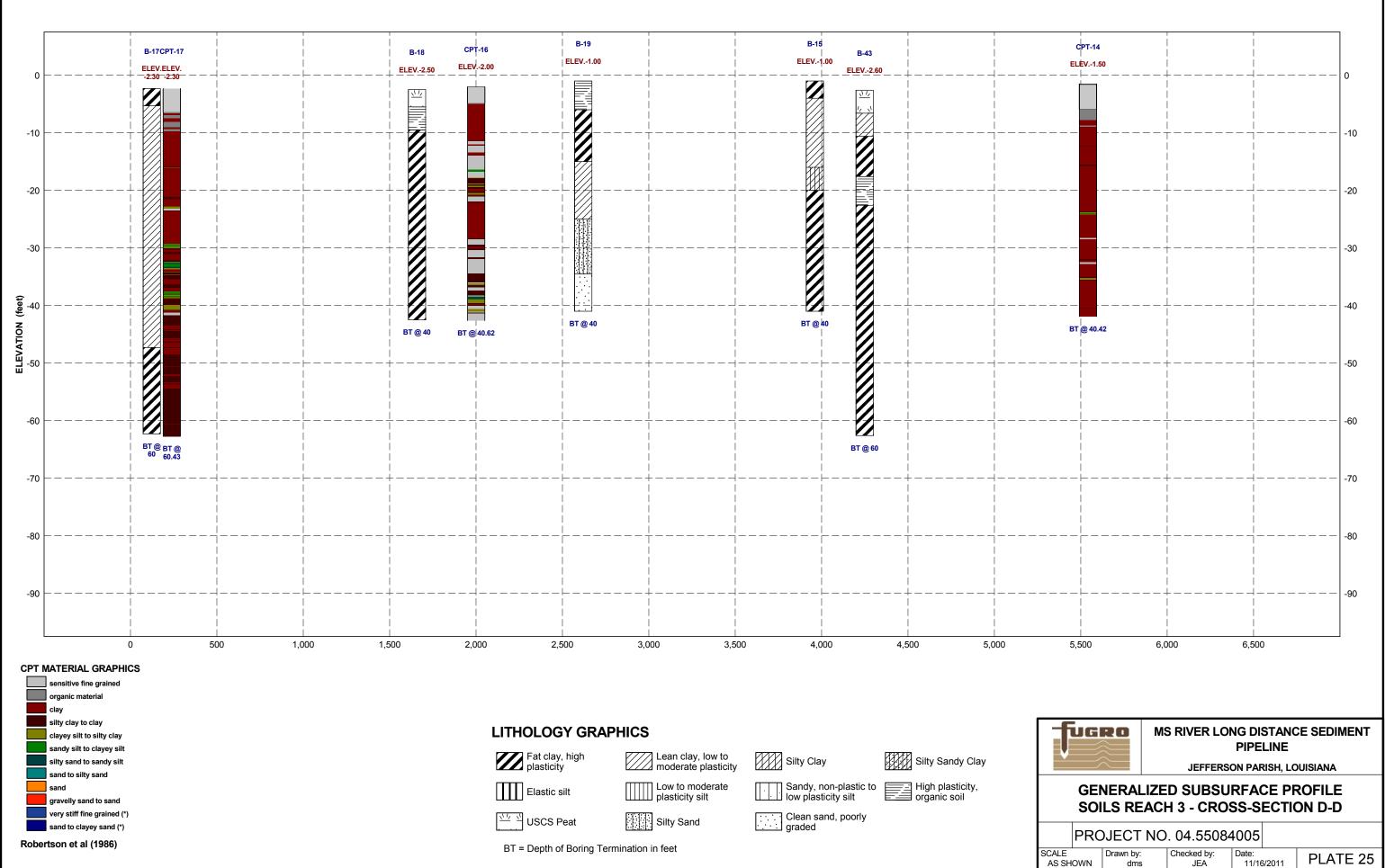




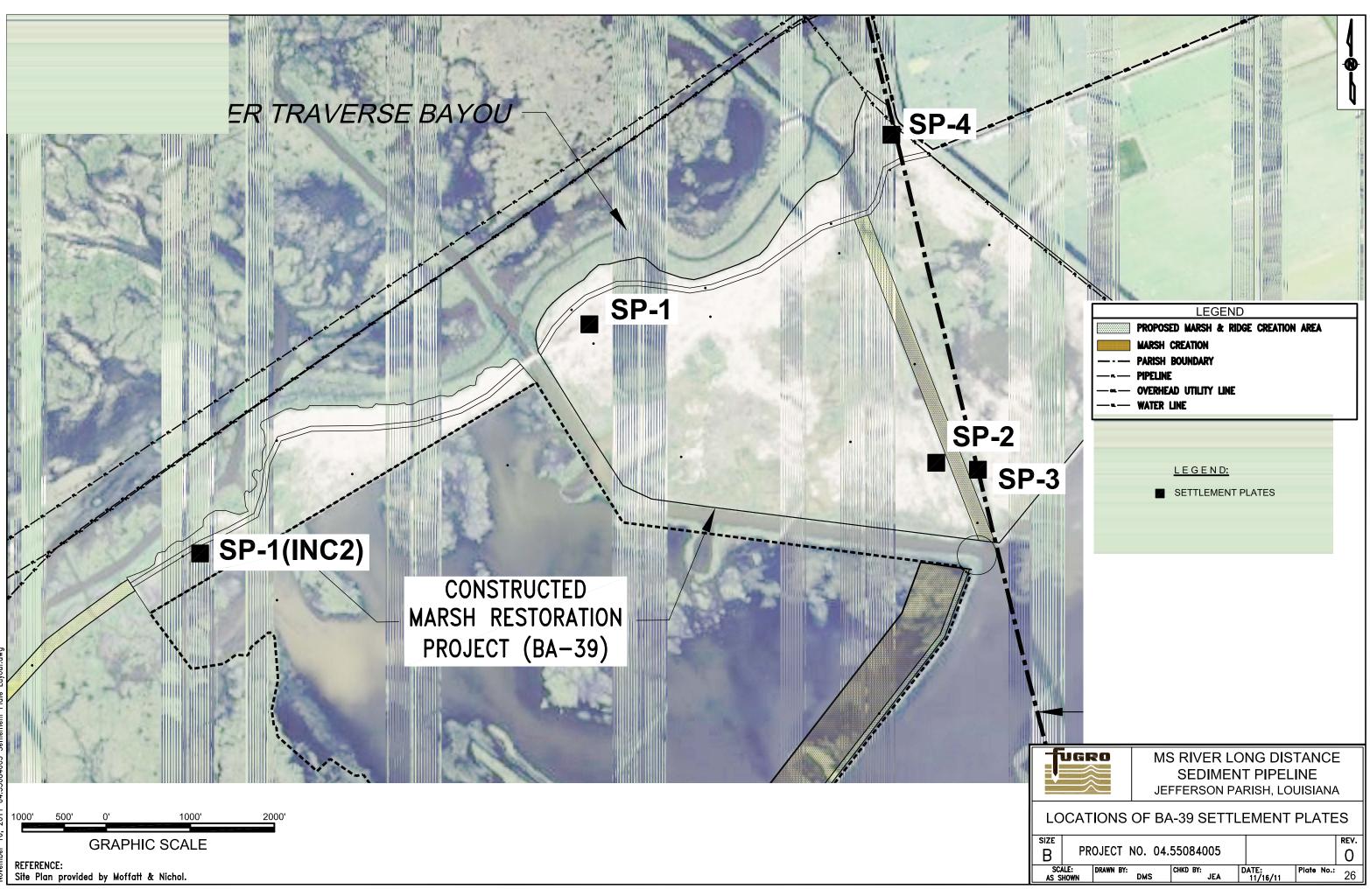
CPT AND BOREHOLE DATA 11X17 04.55084005.GPJ FUGRO DATA TEMPLATE 042610.GDT 1

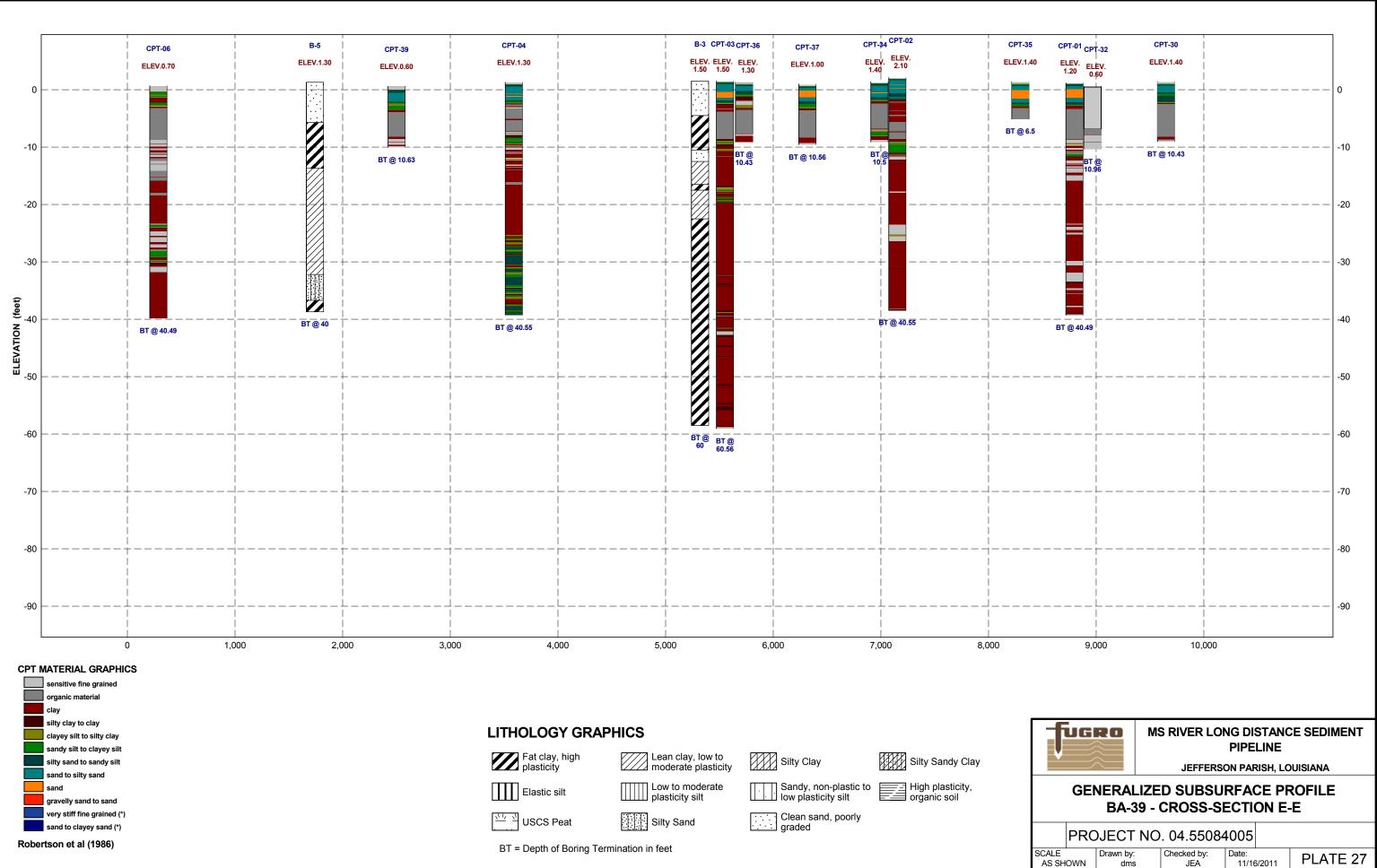


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MS RIVER LONG DISTANCE SEDIMENT PIPELINE JEFFERSON PARISH, LOUISIANA				
GENERALIZED SUBSURFACE PROFILE SOILS REACH 2, EAST-WEST CROSS-SECTION C-C				
SCALE Drawn by:	NO. 04.5508			
AS SHOWN dms		11/16/2011	PLATE 24	

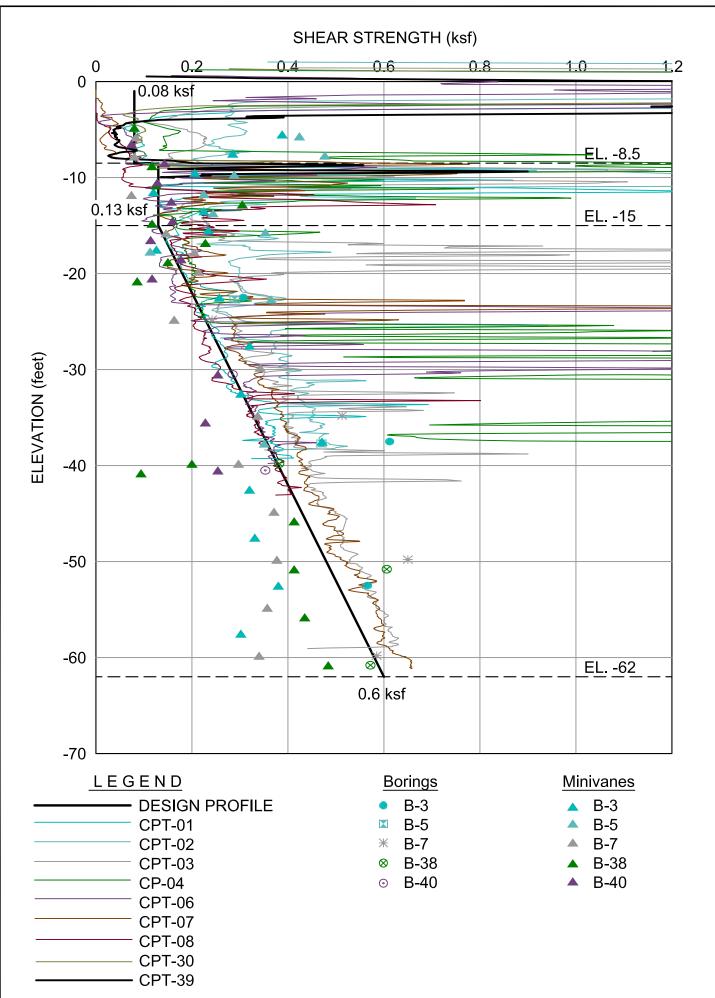


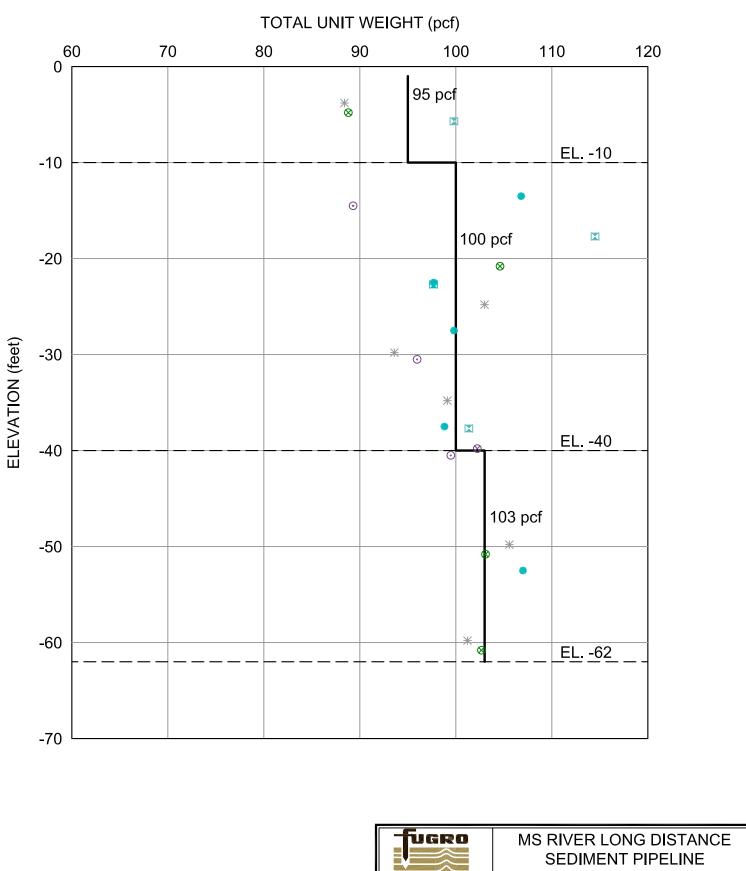
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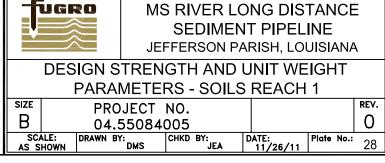


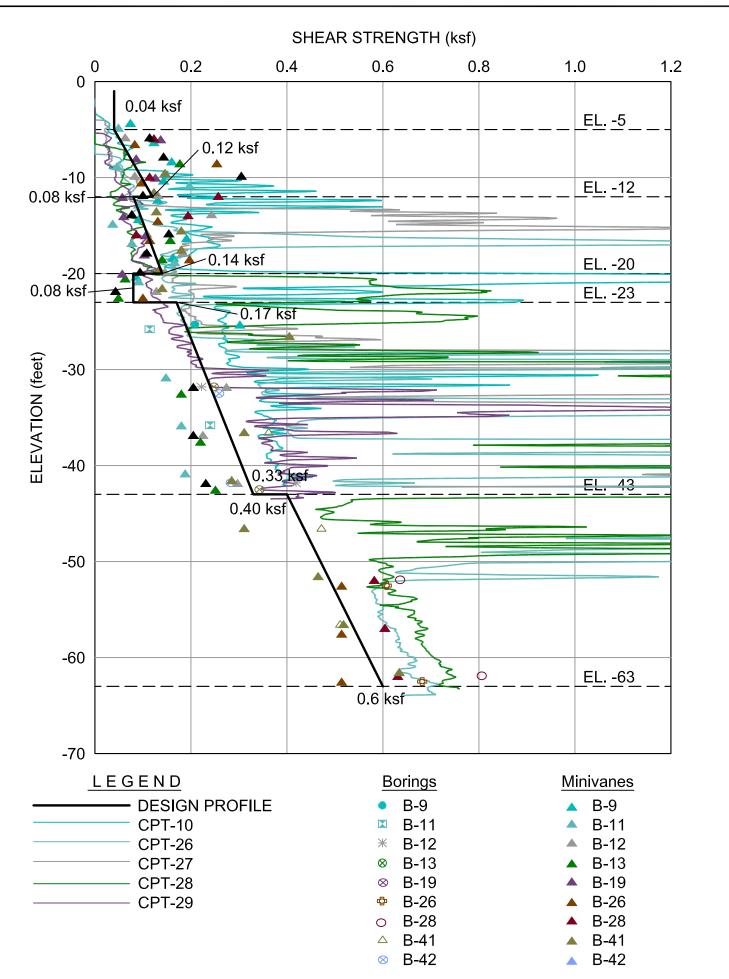


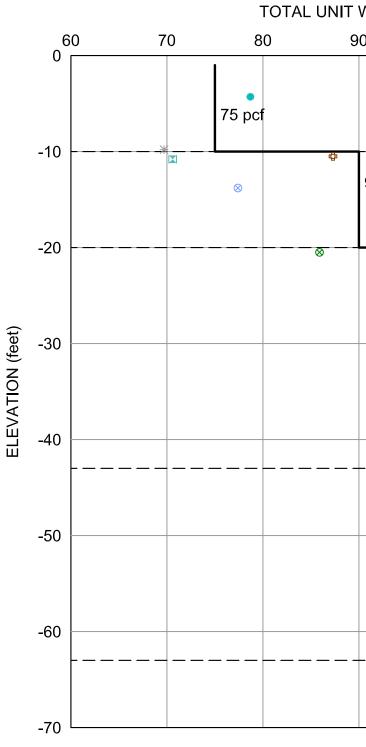
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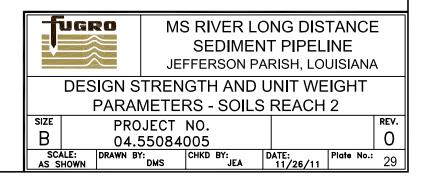


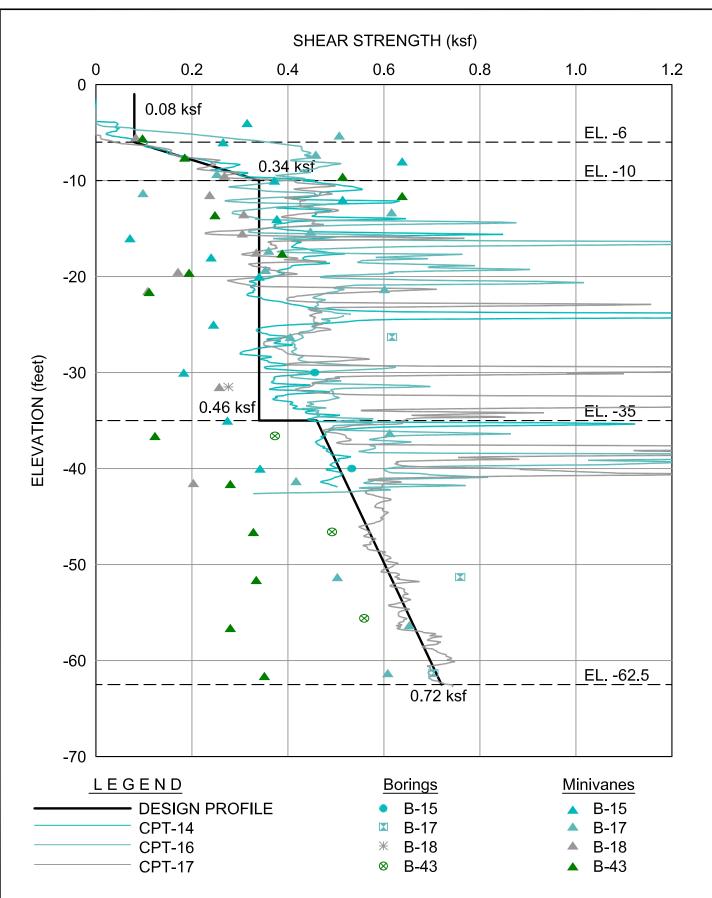


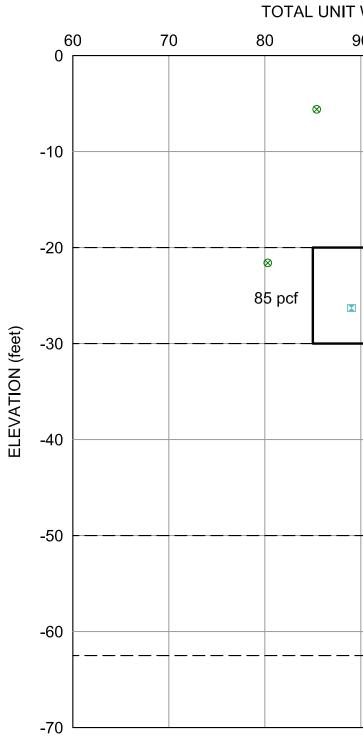




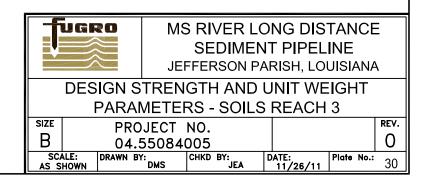
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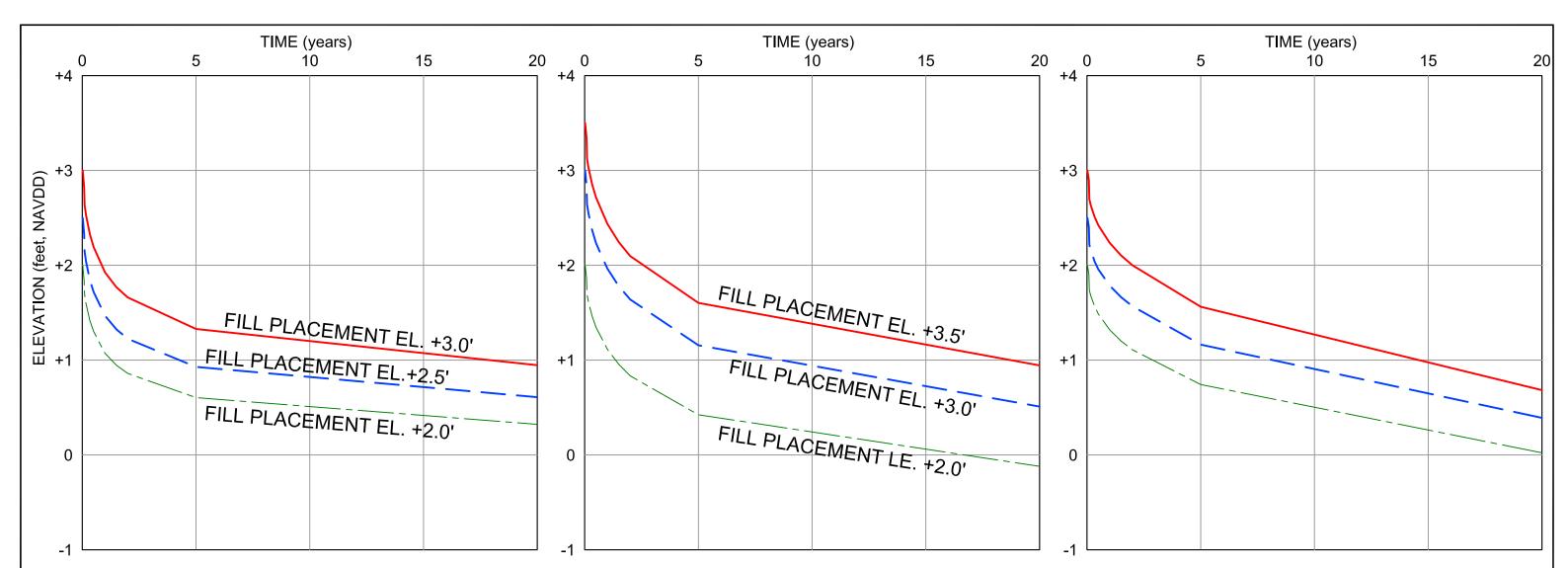






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		EL <u></u> -20	
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SOILS REACH 1 - MUDLINE EL. -1.0'

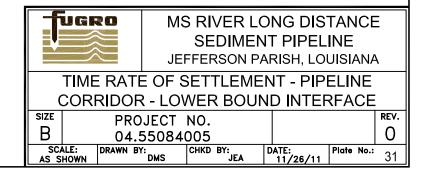
Time (months)	Description of Activity	Top of Fill Elevation (feet)		
(montino)		EL. +3.0	EL. +2.5	EL. +2.0
0.25	End of Fill Placement	3.00	2.50	2.00
1.25	Process Survey	2.64	2.14	1.69
60	5 yr Post Const.	1.33	0.93	0.60
240	20 yr Post Const.	0.95	0.61	0.32

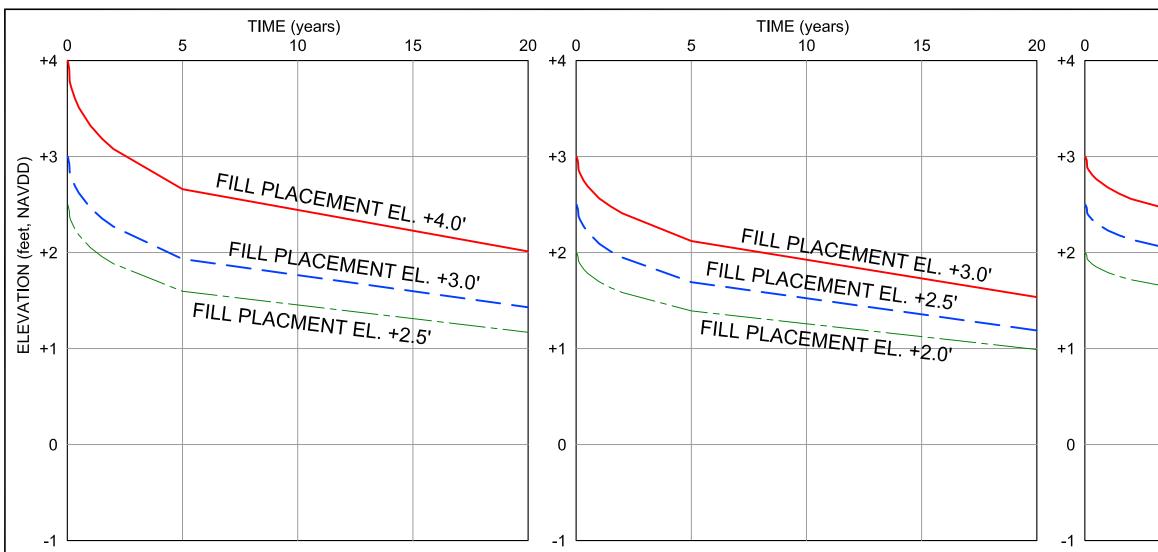
SOILS REACH 2 - MUDLINE AT EL. -2.0'

Time (months)	Description of Activity	Top of Fill Elevation (feet)		
		EL. +3.5	EL. +3.0	EL. +2.0
0.25	End of Fill Placement	3.50	3.00	2.00
1.25	Process Survey	3.12	2.64	1.70
60	5 yr Post Const.	1.60	1.16	0.42
240	20 yr Post Const.	0.94	0.51	-0.12

Time (months)	Description of Activity	Top of Fill Elevation (feet)		
		EL. +3.0	EL. +2.5	EL. +2.0
0.25	End of Fill Placement	3.00	2.50	2.00
1.25	Process Survey	2.70	2.22	1.74
60	5 yr Post Const.	1.56	1.16	0.74
240	20 yr Post Const.	0.68	0.39	0.02

SOILS REACH 3 - MUDLINE AT EL. -2.5'





SOILS REACH 1- MUDLINE EL. +1.0'

Time (months)	Description of Activity	Top of Fill Elevation (feet)		
(monulo)		EL. +4.0	EL. +3.0	EL. +2.5
0.25	End of Fill Placement	4.00	3.00	2.50
1.25	Process Survey	3.78	2.84	2.37
60	5 yr Post Const.	2.66	1.93	1.60
240	20 yr Post Const.	2.01	1.43	1.17

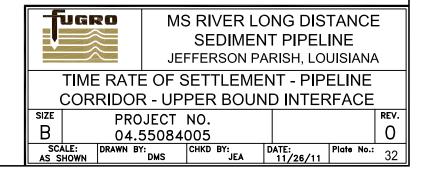
SOILS REACH 2 - MUDLINE EL. +1.0'

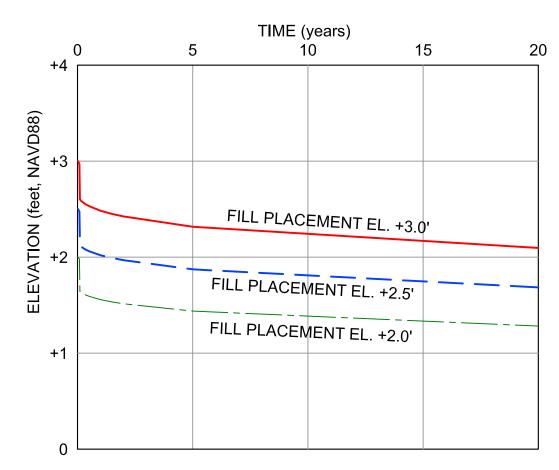
Time (months)	Description of Activity	Top of Fill Elevation (feet)		
		EL. +3.0	EL. +2.5	EL. +2.0
0.25	End of Fill Placement	3.00	2.50	2.00
1.25	Process Survey	2.86	2.38	1.91
60	5 yr Post Const.	2.12	1.69	1.39
240	20 yr Post Const.	1.54	1.19	0.99

Time (months)	Description of Activity	Top of Fill Elevation (feet)		
(montino)		EL. +3.0'	EL. +2.5	EL. +2.0
0.25	End of Fill Placement	3.00	2.50	2.00
1.25	Process Survey	2.89	2.41	1.93
60	5 yr Post Const.	2.36	1.96	1.58
240	20 yr Post Const.	1.86	1.56	1.28

į	TIME () 5 1		5 20
		EMENT EL. +2 MENT EL. +2 MENT EL. +	2.5'

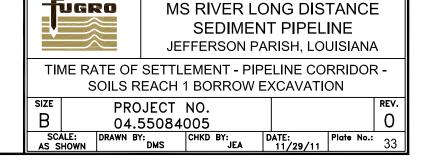
SOILS REACH 3 - MUDLINE EL. +1.0'

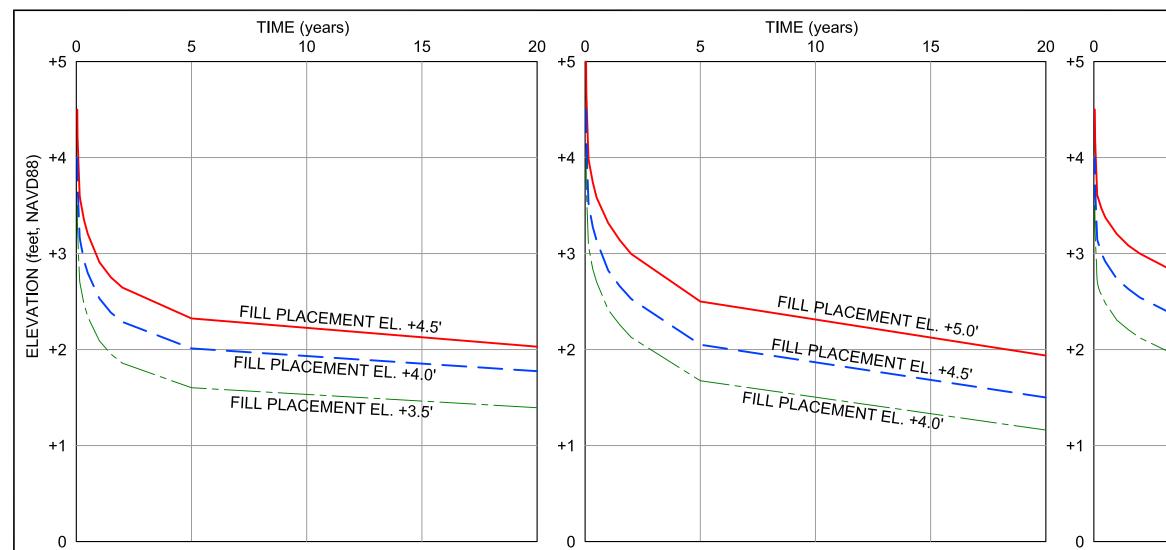




SOILS REACH 1- MUDLINE EL. -9.0'

Time (months)	Description of Activity	Top of Fill Elevation (feet)		
		EL. +3.0	EL. +2.5	EL. +2.0
0.25	End of Fill Placement	3.00	2.50	2.00
1.25	Process Survey	2.60	2.12	1.64
60	5 yr Post Const.	2.32	1.87	1.44
240	20 yr Post Const.	2.10	1.69	1.28





SOILS REACH 1- MUDLINE EL. -1.0'

Time (months)	Description of Activity	Top of F	Fill Elevation (feet)			
(EL. +4.5	EL. +4.0	EL. +3.5		
0.25	End of Fill Placement	4.50	4.00	3.50		
1.25	Process Survey	3.61	3.17	2.71		
60	5 yr Post Const.	2.32	2.01	1.60		
240	20 yr Post Const.	2.03	1.77	1.39		

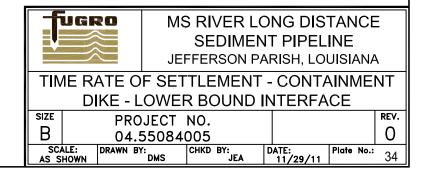
SOILS REACH 2- MUDLINE EL. -2.0'

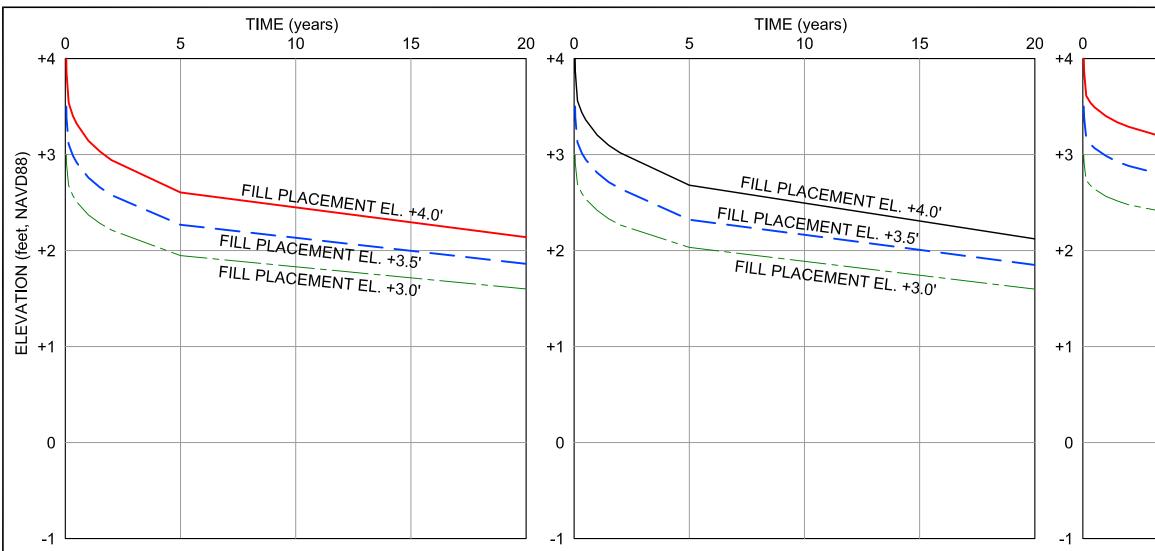
Time (months)	Description of Activity	Top of Fill Elevation (feet)					
(EL. +5.0 EL. +4.5 EL. +4					
0.25	End of Fill Placement	5.00	4.50	4.00			
1.25	Process Survey	3.99	3.53	3.09			
60	5 yr Post Const.	2.50	2.05	1.68			
240	20 yr Post Const.	1.94	1.50	1.16			

Time (months)	Description of Activity	Top of F	Fill Elevation (feet)			
(EL. +4.5	EL. +4.0	EL. +3.5		
0.25	End of Fill Placement	4.50	4.00	3.50		
1.25	Process Survey	2.61	3.15	2.71		
60	5 yr Post Const.	2.62	2.18	1.77		
240	20 yr Post Const.	2.04	1.59	1.23		

Ę	TIME (5 1		5 20
	FILL PL	ACEMENT EL. ACEMENT EL. MENT EL. +3.5'	

SOILS REACH 3- MUDLINE EL. -2.5'





SOILS REACH 1 - MUDLINE AT EL. +1.0'

Time (months)	Description of Activity	Top of F	Fill Elevation (feet)			
(EL. +4.0	EL. +3.5	EL. +3.0		
0.25	End of Fill Placement	4.00	3.50	3.00		
1.25	Process Survey	3.54	3.11	2.68		
60	5 yr Post Const.	2.60	2.27	1.95		
240	20 yr Post Const.	2.14	1.86	1.60		

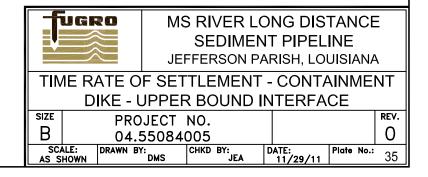
SOILS REACH 2 - MUDLINE AT EL. +1.0'

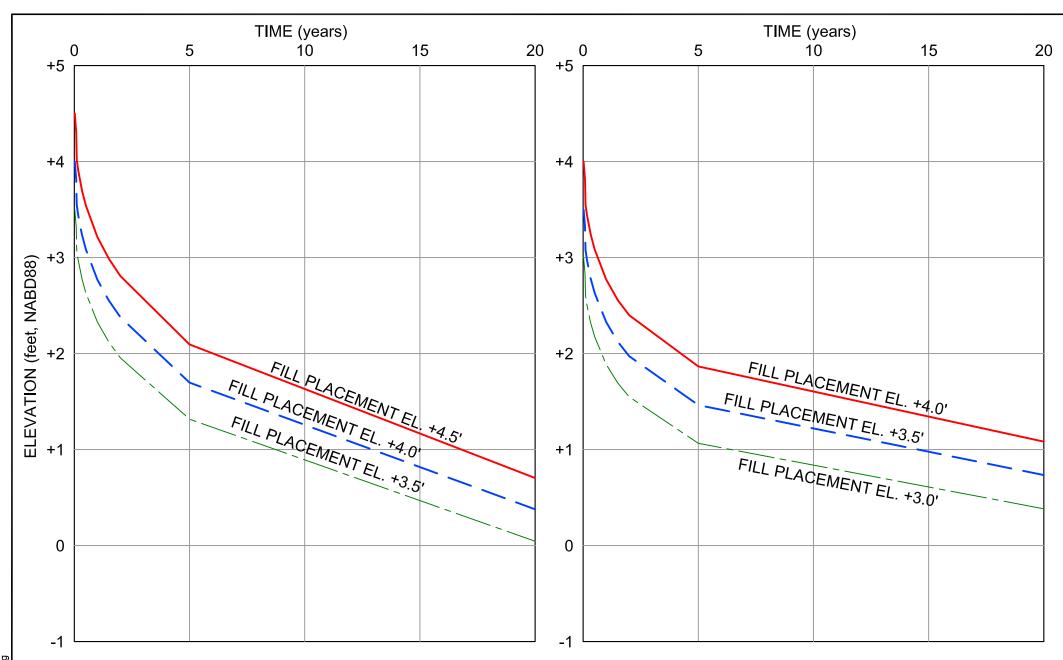
Time (months)	Description of Activity	Top of Fill Elevation (feet)					
(EL. +4.0	EL. +3.5	EL. +3.0			
0.25	End of Fill Placement	4.00	3.50	3.00			
1.25	Process Survey	3.56	3.13	2.69			
60	5 yr Post Const.	2.68	2.32	2.03			
240	20 yr Post Const.	2.12	1.85	1.60			

Time (months)	Description of Activity	Top of F	Fill Elevation (feet)			
(EL. +4.0	EL. +3.5	EL. +3.0		
0.25	End of Fill Placement	4.00	3.50	3.00		
1.25	Process Survey	3.61	3.17	2.73		
60	5 yr Post Const.	3.08	2.70	2.33		
240	20 yr Post Const.	2.65	2.13	2.00		

TIME (<u>1</u> 5 1	years) 0 1	5 2	20
5 1 FILL PLACEN FILL PLACEM	0 1	5 2	

SOILS REACH 3 - MUDLINE AT EL. +1.0'





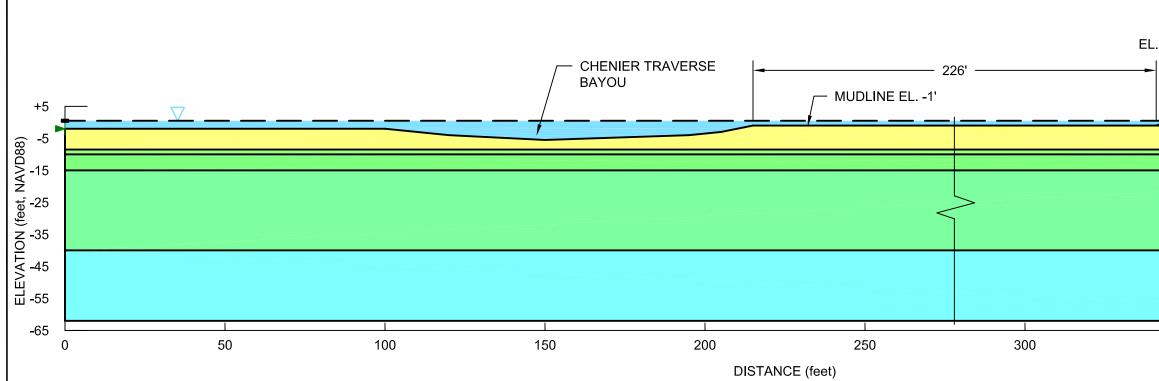
B-42 AND B-43 PROFILE

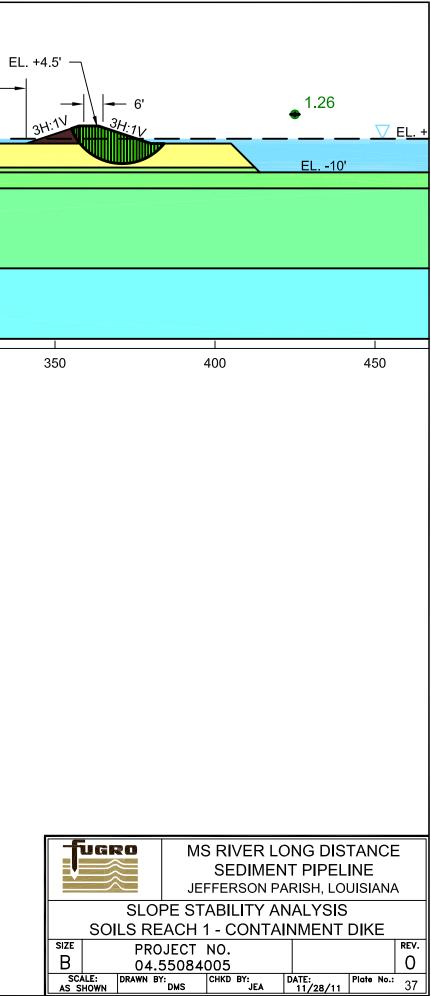
Time (months)	Description of Activity	Top of F	Fill Elevation (feet)			
(montina)		EL. +4.5'	EL. +4.0'	EL. +3.5'		
0.25	End of Fill Placement	4.50	4.00	3.50		
1.25	Process Survey	4.02	3.55	3.08		
60	5 yr Post Const.	2.09	1.70	1.32		
240	20 yr Post Const.	0.70	0.38	0.04		

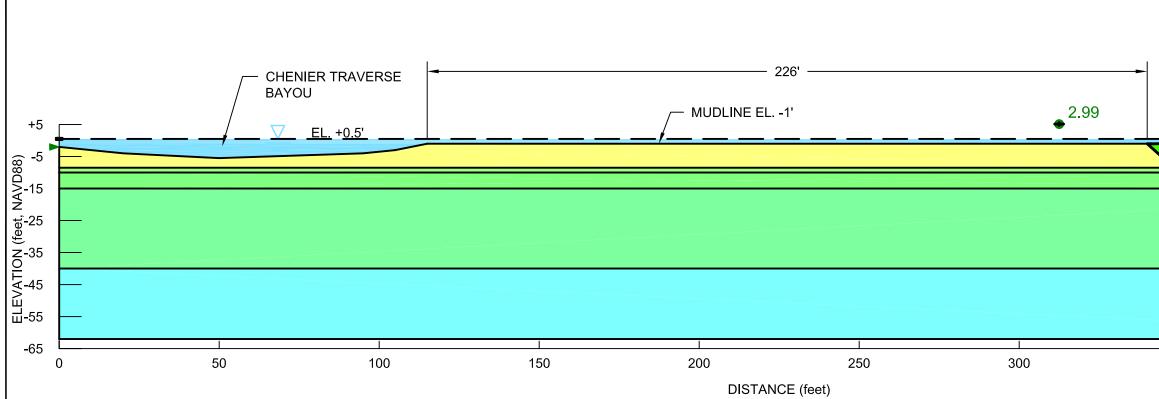
SOILS REACH 2 PROFILE

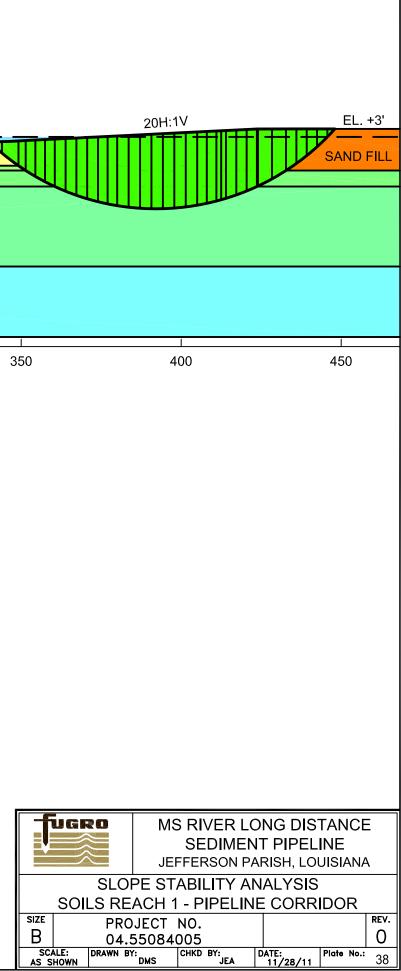
Time (months)	Description of Activity	Top of F	Fill Elevation (feet)				
		EL. +4.0'	EL. +3.5'	EL. +3.0'			
0.25	End of Fill Placement	4.00	3.50	3.00			
1.25	Process Survey	3.55	3.08	2.60			
60	5 yr Post Const.	1.87	1.46	1.06			
240	20 yr Post Const.	1.08	0.73	0.38			

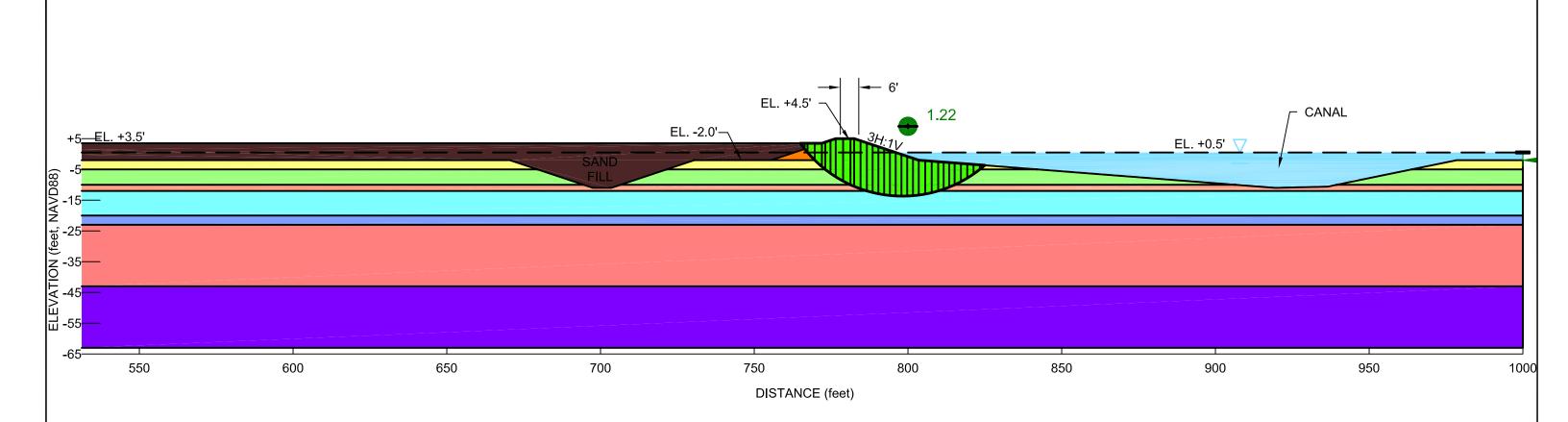
	ugr	20	MS	MS RIVER LONG DISTANCE						
				SEDIMEN	IT PIPEL	INE				
			JEF	FERSON PA	ARISH, LO	UISIANA	۹.			
		TIME	RATE	OF SETT	LEMENT	•				
		MA	RSH (CREATION	AREA					
SIZE		PRO	JECT	NO.			REV.			
B	04.55084005									
	ÁLE: HOWN	DRAWN BY	': DMS	CHKD BY: JEA	DATE: 11/29/11	Plate No.:	36			



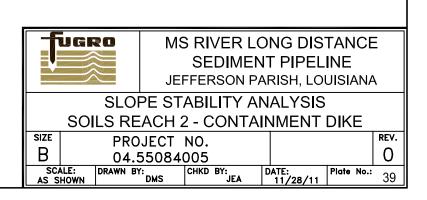


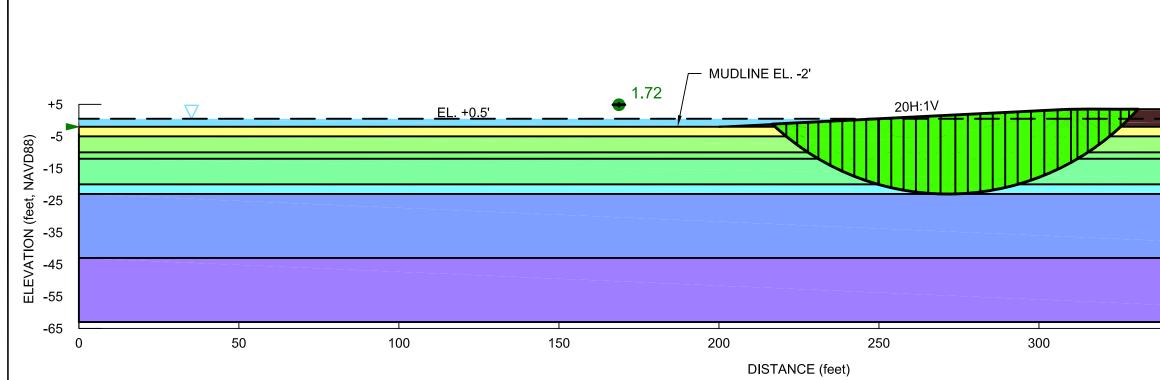


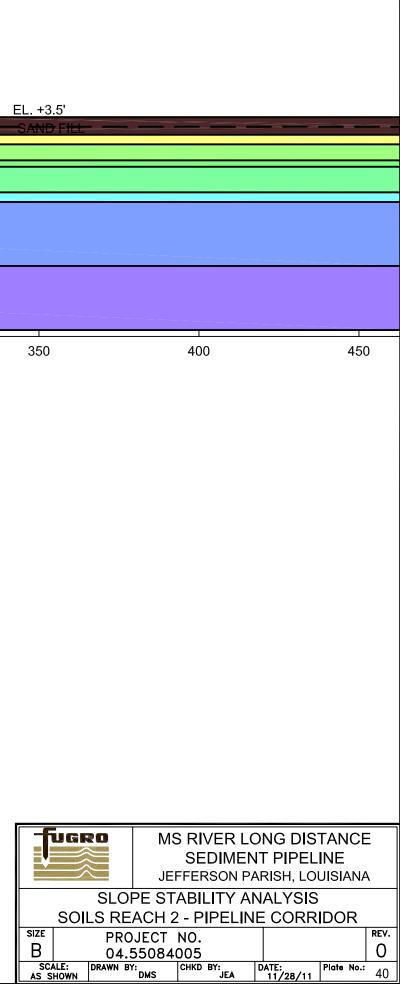


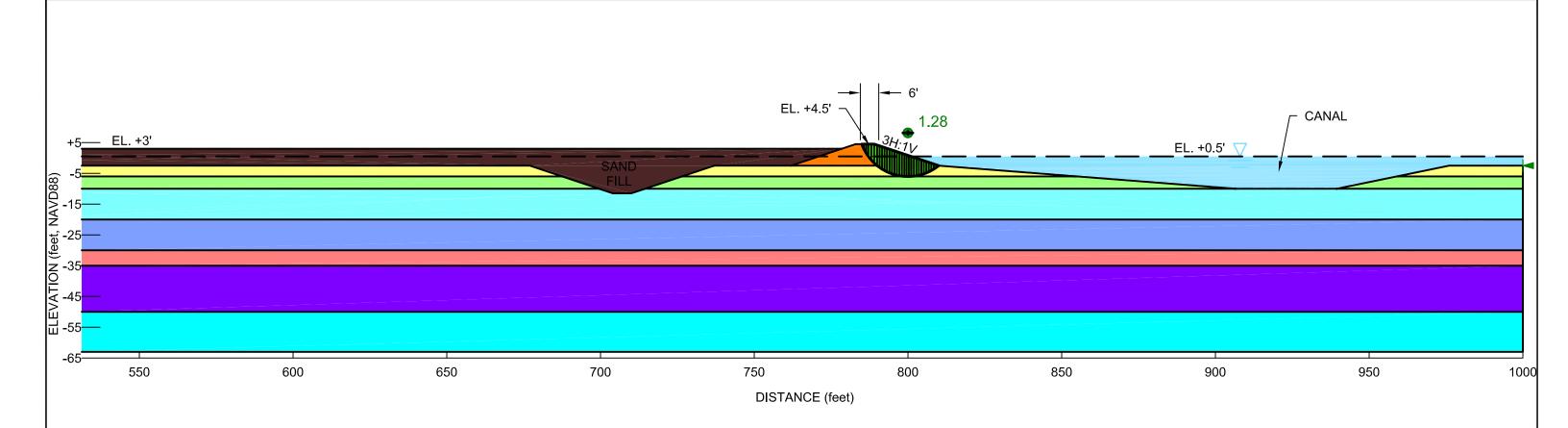


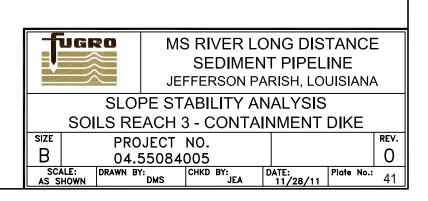


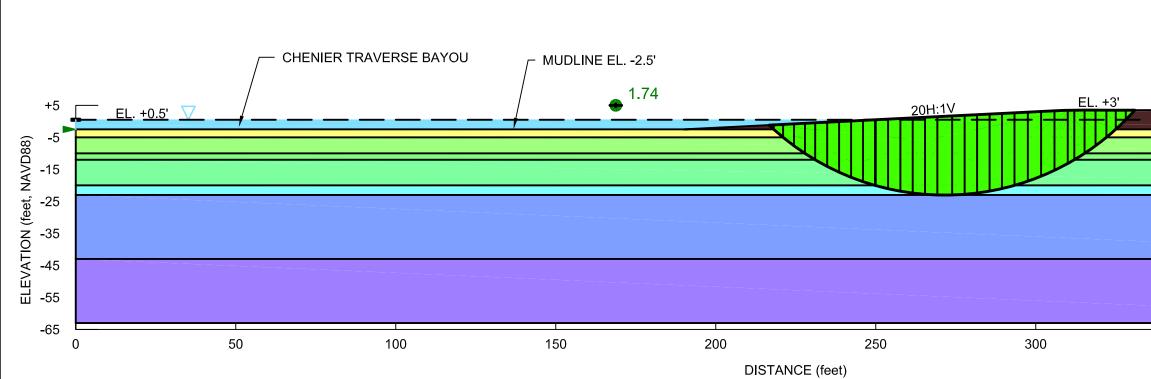


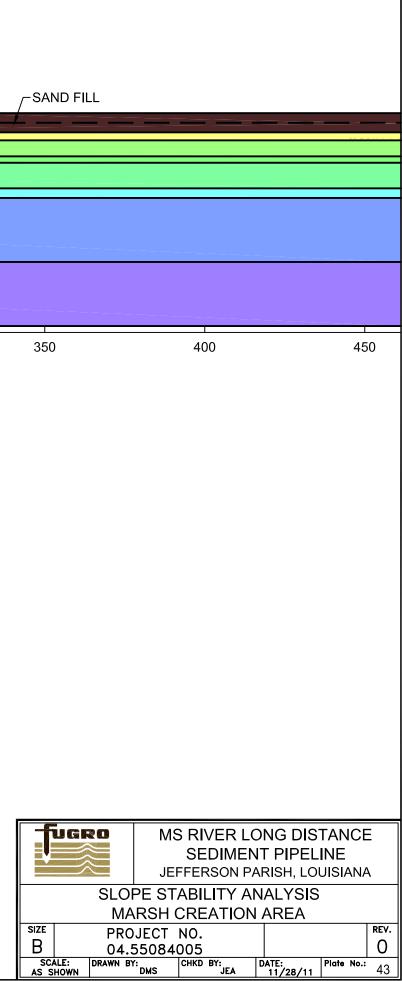


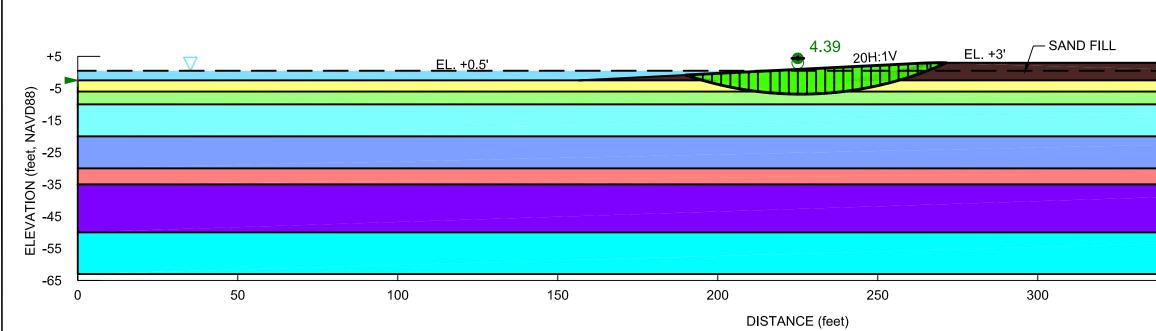


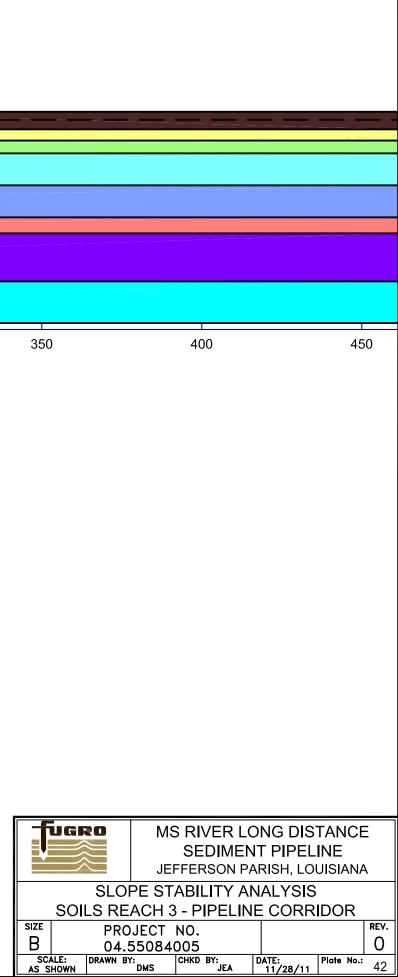


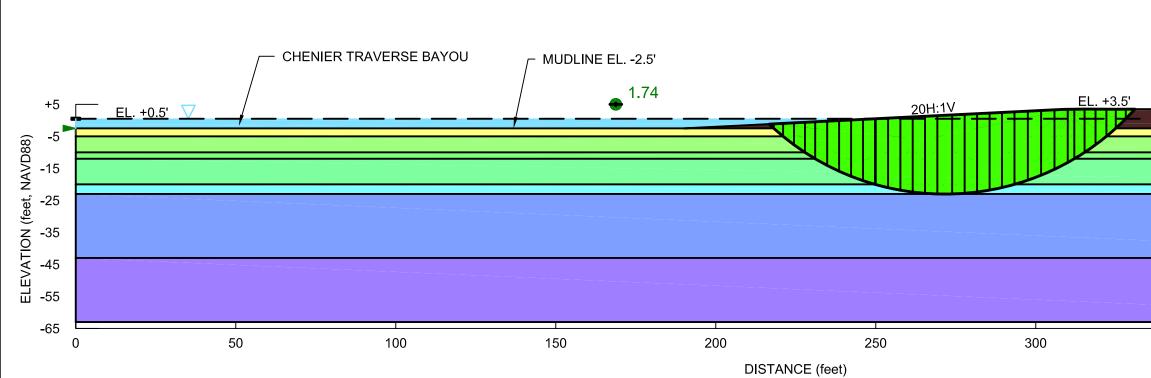


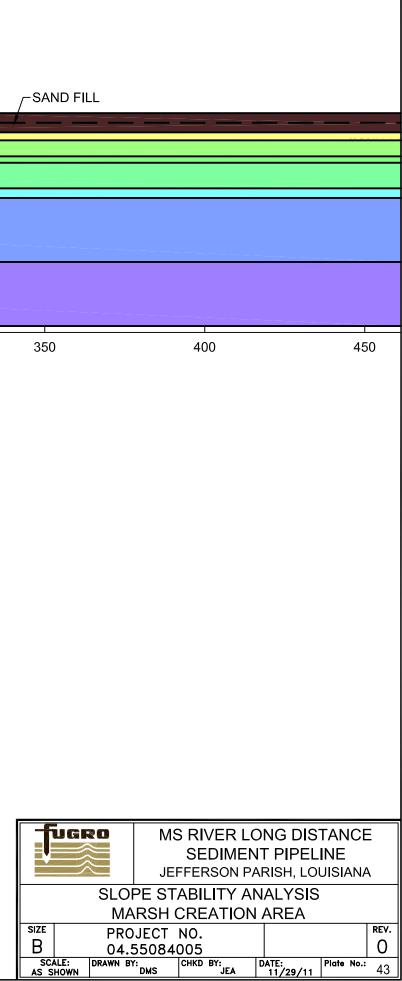














APPENDIX A SUMMARY OF TEST RESULTS



			lde	entificat	tion Tes	sts		Field She Strength Est		Miniatu Te		Compression Tests								
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	_	Torvane (ksf)		Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	1-2				14		4													
2	2-4				21															
3	4.5-6				18		5													
4A	6-7	0.59	73	25	53															
4B	7-8				52					0.39										
5A	8-9				53															
5B	9-10				65					0.29	0.36									
6A	10-11																			
6B	11-12	0.51	54	19	37		55			0.21										
7A	12-14				20		3													
7B	13-14				22					0.12										
8B	15-16	0.69	43	23	37	78	88			0.23										
9B	17-18				68					0.23										
10A	18-19							0.50												
10B	19-20				38					0.13										
11A	23-24				83															
11B	24-25				78	55				0.26		UU	78	17	0.31		0.8	55	6.9	А
12A	28-29																			
12B	29-30	0.92	72	24	68	59	100			0.32										
13A	33-34																			
13B	34-35				80					0.30										
14B	39-40				69	59				0.47		UU	69	22	0.61		0.8	59	2.7	В
15B	44-45				61					0.32										
16A	48-49																			
NF *C	Notes: TYPE OF TEST TYPE OF FAILURE NP = Non-Plastic Material U - Unconfined Compression A - Bulge NP = Non-Plastic Material UU - Unconsolidated - Undrained Triaxial B - Single Shear Plane *Corrected as described on Terms and CU - Consolidated - Undrained Triaxial C - Multiple Shear Plane Symbols Used on Boring Logs. D - Vertical Fracture																			
	JGRO				Distan	ice Se	diment	Pipeline						UMMA	RY OF	TEST F	RESUL	TS - B	ORING	B-3
V																		LEL	AP Lab ID	#10001
Fugro C	Consultants, In	c Je	ffersor	n Paris	h, Lou	isiana										Project N 04.55	。. 084005			

			lde	entificat	tion Tes	sts		Field Shear Miniature Var Strength Estimate Tests				e Compression Tests								
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing	-			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
16B	49-50				58					0.33										
17B	54-55				56	69				0.38		UU	56	38	0.57		0.8	69	4.7	В
18A	58-59																			
18B	59-60				60					0.30										
NP *Co	tes: = Non-Pla prrected as mbols Usec	describ	bed on ⁻	Terms a gs.	and	U UU	I - Unco	TEST onfined Componsolidated - solidated - Ur	Undrai	ned Tria	A xial B II C	YPE OF FAI - Bulge - Single She - Multiple S - Vertical Fr	ear Plane hear Plar	e ne						
	Symbols Used on Boring Logs. D - Vertical Fracture MS River Long Distance Sediment Pipeline SUMMARY OF TE														TEST F	RESUL	TS - B	ORING	B-3	
LELAP Lab ID													#10001							
Fugro C	onsultants, In	c Je	ffersor	n Paris	h, Lou	isiana										Project N 04.55	。. 084005			

			ld	entificat	tion Tes	sts		Field She Strength Est		Miniatu Te	re Vane sts		Compress	sion Tests						
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	Penetrometer* (ksf)			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				21		4													
2	2.5-4				19		5													
4B	7-8	0.78	81	24	68	59	97			0.42										
5	8-9																			
5B	9-10				54					0.48	0.24									
6B	11-12				15					0.29										
7B	13-14	0.15	66	22	29					0.23										
8B	15-16				39					0.24										
9B	17-18				37					0.35	0.24									
10B	19-20	1.69	32	25	37	84	97			0.11										
11B	24-25				77	55				0.37		UU	77	17	0.29		0.9	55	8.4	A
12	28-30	0.70	46	22	39															
12	29-30																			
13	33.5-35				31		84													
14B	39-40				71	59				0.35		UU	71	27	0.47		0.7	59	4.0	В
NF *C	tes: ? = Non-Pla orrected as mbols Used	descril	bed on [·]	Terms a gs	and	U UU	I - Unco	TEST onfined Componsolidated - solidated - Ur	Undrai	ned Tria	A xial B II C	PE OF FA - Bulge - Single Sh - Multiple S - Vertical Fi	ear Plane hear Plar							
	JGRO	bols Used on Boring Logs. D - Vertical Fracture MS River Long Distance Sediment Pipeline SUMMARY C														TEST F	RESUL	TS - B	ORING	B-5
																LELAP Lab ID #1000				
Fugro C	o Consultants, Inc Jefferson Parish, Louisiana													Project No. 04.55084005						

			ld	entificat	tion Tes	sts		Field Shear Miniature Vane Strength Estimate Tests				Compression Tests								
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	Penetrometer* (ksf)			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0.5-2				135															
2A	2-3				184															
2B	3-4	0.92	133	35	125	39	89			0.02										
3A	4-5																			
3B	5-6				33			0.50		0.08										
4A	6-7				42															
4B	7-8				35					0.08	0.10									
5A	8-9																			
5B	9-10				37															
6A	10-11	1.28	38	22	42															
6B	11-12				70					0.07										
7B	13-14				73															
8A	14-15																			
8B	15-16				155					0.15										
9A	16-17	0.91	99	32	93															
9B	17-18				53					0.21										
10A	18-19																			
10B	19-20				36					0.21										
11B	24-25				62	64				0.16		UU	62	17	0.24		1.8	64	11.9	A
12B	29-30	0.81	85	27	74	54	100			0.34										
13B	34-35				75	57				0.34		UU	75	24	0.51		0.9	57	4.3	В
14A	38-39																			
14B	39-40				68					0.30										
15A	43-44																			
NP *Ce	tes: ? = Non-Pla orrected as mbols Usec	describ	bed on [·]		and	U UU	- Unco	TEST onfined Componsolidated - solidated - Ur	Undrai	ned Tria	A xial B Il C	YPE OF FAI - Bulge - Single Sho - Multiple S - Vertical Fi	ear Plane hear Plar	e ne						
Image: Subscription Subscription MS River Long Distance Sediment Pipeline SUMMARY OF TEST RESULTS													TS - B	ORING	B-7					
LELAP La													AP Lab ID	#10001						
Fugro C	consultants, In	Je	fferso	n Paris	h, Lou	isiana										Project N 04.55	^{io.} 084005			

			lde	entificat	tion Tes	sts		Field Shear Miniature Va Strength Estimate Tests				ne Compression Tests								
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing	_	Torvane (ksf)		Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
15B	44-45				69			0.50		0.37										
16B	49-50				54	69				0.38		UU	54	34	0.65		0.6	69	1.9	В
17A	53-54																			
17B	54-55				49			0.50		0.36										
18B	59-60				61	63				0.34		UU	61	41	0.59		0.6	63	5.1	В
Not	es:					TY	PE OF	TEST			т	I YPE OF FAI	II URF							
NP *Co	= Non-Pla prrected as mbols Usec	describ	bed on ⁻	Terms a gs.	and	U UU	- Unco I - Unco	onfined Componsolidated - solidated - Ur	Undraii	ned Tria	A xial B I C	- Bulge - Single Sho - Multiple S - Vertical Fi	ear Plane hear Plai	e ne						
-fu	Image of the bining Logo. Description MS River Long Distance Sediment Pipeline SUMMARY OF TEST RESU													TEST F	RESUL	TS - B	ORING	B-7		
V															LEL	LELAP Lab ID #10001				
Fugro C	onsultants, In	c Je	ffersor	n Paris	h, Lou	isiana										Project N 04.55	^{io.} 084005			

			ld	entificat	tion Tes	sts		Field Shear Miniature Va Strength Estimate Tests				ne Compression Tests								
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	Penetrometer* (ksf)			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				214															
2A	2-3				395															
2B	3-4	1.54	191	54	264	22	47			0.07										
3B	5-6				53					0.12	0.12									
4B	7-8				86					0.16										
5B	9-10				49					0.14										
6B	11-12				40					0.13										
7A	12-13	1.42	55	24	68															
7B	13-14				44					0.09										
8B	15-16				77					0.19										
9B	17-18				54					0.16										
10B	19-20				35					0.09										
11A	23-24	7.10	25	24	30															
11B	24-25				47	74				0.30		UU	47	18	0.21		2.5	74	13.9	A
12A	30-31.5				28		44													
14	38.5-40				35		44													
NF *C	otes: P = Non-Pla orrected as mbols Usec	descrit	bed on [•]	Terms a gs.	and	U UU	I - Unco	TEST onfined Com onsolidated - solidated - Ur	Undrai	ned Tria	A xial B al C	YPE OF FA - Bulge - Single Sh - Multiple S - Vertical Fi	ear Plane hear Plar	e ne						
	UGRO MS River Long Distance Sediment Pipeline SUMMARY OF													ry of	TEST F	RESUL	TS - B	ORING	B-9	
V															LELAP Lab ID #10001					
Fugro C	gro Consultants, Inc Jefferson Parish, Louisiana													Project N 04.55	. No. 5084005					

			lde	entificat	tion Tes	sts		Field She Strength Est		re Vane sts			(Compres	sion Test	S				
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	_	Torvane (ksf)		Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				852															
2a	2-3																			
2B	3-4	2.24	548	254	913					0.05										
3	4-6				447															
4b	7-8				266					0.05										
5a	8-9																			
5b	9-10	1.95	312	152	465	13	80			0.20										
6b	11-12				275					0.09										
7b	13-14				320					0.04										
8b	15-16				128					0.08										
9b	16-17	1.06	125	35	130															
9b	17-18				83					0.17										
10b	19-20				36					0.09	0.15									
11b	24-25				68	58						UU	68	18	0.11		1.0	58	14.6	A
12a	28-29				80															
12b	29-30				58					0.15										
13b	34-35				49	70				0.18		UU	49	26	0.24		1.2	70	9.3	A
14a	38-39				78					0.40										
14b	39-40				73					0.19										
						TV		тгот												
NP *Ce	tes: ? = Non-Pla orrected as mbols Usec	describ	bed on ⁻	Terms a gs.	and	U UU	I - Unco	Dest onfined Componsolidated - solidated - Ur	Undrai	ned Tria	A xial B al C	PE OF FA - Bulge - Single Sh - Multiple S - Vertical F	ear Plane Shear Plai	e ne						
_fi	JGRO	M	S River Long Distance Sediment Pipeline SUMMARY OF TE													EST R	ESULT	S - BO	RING	3-11
																		LEL	AP Lab ID	#10001
Fugro C	consultants, In	c Je	ffersor	n Paris	h, Lou	isiana										Project N 04.55	。 084005			

			ld	entifica	tion Tes	sts		Field She Strength Est		Miniatu Te				(Compres	sion Test	S			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	Penetrometer* (ksf)			Remolded Shear	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-2				533															
2	2-3	1.03	175	35	179															
2B	3-4				221					0.06										
3	4-6																			
4A	6-7				230															
4B	7-8	0.98	287	57	283	18	28			0.08										
5A	8-9																			
5B	9-10				183					0.13										
6B	11-12				243					0.24	0.20									
7A	12-13																			
7B	13-14				271					0.11										
8A	14-15																			
8B	15-16				77					0.18										
9A	16-17	1.28	77	23	92															
9B	17-18				52					0.15										
10A	18-19																			
10B	19-20				33					0.13										
11	23-25																			
12B	29-30				53	69				0.27		UU	53	20	0.22		1.1	69	10.4	A
13A	33-34																			
13B	34-35				57					0.23										
14B	39-40				55	68				0.30		UU	55	27	0.42		0.8	68	4.3	A,B
NF *C	tes: ? = Non-Pla orrected as mbols Usec	describ	bed on [·]		and	U UU	- Unco	TEST onfined Com onsolidated - solidated - Ur	Undrai	ned Tria	A xial B al C	YPE OF FA - Bulge - Single Sh - Multiple S - Vertical Fi	ear Plane hear Plai	 e						
-6	JGRO	M	S River	Long	Distan	ce Sec	diment	Pipeline					SU	MMAR	Y OF T	EST R	ESULT	S - BO	RING I	3-12
U								-											AP Lab ID	
Fugro C	Consultants, In	Je	fferso	n Paris	h, Lou	isiana										Project N 04.55	。 084005			

			lde	entificat	tion Tes	sts		Field She Strength Est			re Vane sts			(Compres	sion Tests	S			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	_	Torvane (ksf)		Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				412															
3A	4-5	1.13	187	47	205															
3B	5-6				92					0.18										
4B	7-8				101															
5B	9-10				157						0.24									
6B	11-12				151															
7A	12-13	1.49	125	38	168															
7B	13-14				176					0.16										
8B	15-16				138					0.14										
9B	17-18	1.30	76	26	91	45	87			0.06										
10B	19-20				82					0.05										
11	23-25	0.79	58	22	51															
12B	29-30				77	56				0.18		UU	77	20	0.26		0.8	56	11.1	A
13A	33-34				79															
13B	34-35				77					0.22										
14B	39-40				67	60				0.25		UU	67	27	0.34		0.7	60	6.6	A
NF *C	tes: P = Non-Pla orrected as mbols Usec	describ	bed on ⁻	Terms a gs.	and	U UU	I - Unco	TEST onfined Componsolidated - solidated - Ur	Undrai	ned Tria	A xial B al C	/PE OF FA - Bulge - Single Sh - Multiple S - Vertical F	ear Plane Shear Plai	e ne						
-fi	JGRO	M	S River	Long	Distan	ce Sec	diment	Pipeline					SU	MMAR	Y OF T	EST R	ESULT	S - BO	RING	3-13
V	=																	LEL	AP Lab ID	#10001
Fugro C	Consultants, In	c Je	ffersor	n Paris	h, Lou	isiana										Project N 04.55	。. 084005			

			ld	entifica	tion Tes	sts		Field She Strength Est		Miniatu Te	re Vane sts			(Compres	sion Tests	6			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	Penetrometer* (ksf)			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				61															
2B	3-4				36					0.32	0.25									
3B	5-6	0.60	45	18	34	86	94			0.27										
4B	7-8				39					0.64										
5B	9-10				42					0.37										
6B	11-12				36					0.51										
7B	13-14				35					0.38										
8B	15-16				29					0.07										
9A	16-17	1.10	34	24	34		92													
9B	17-18				31					0.24										
10B	19-20				65					0.34										
11B	24-25	0.53	142	37	93		96			0.25										
12B	29-30				60	64				0.18		UU	60	20	0.46		0.8	64	3.8	С
13A	33-34	0.99	52	20	52															
13B	34-35				26					0.27										
14B	39-40				64	62				0.34		UU	64	27	0.53		0.8	62	5.6	В
NF *C	otes: P = Non-Pla orrected as mbols Used	descril	bed on [•]		and	U UU	I - Unco	TEST onfined Com onsolidated - solidated - Ur	Undrai	ned Tria	A xial E al C	YPE OF FA - Bulge - Single Sh - Multiple S - Vertical Fi	ear Plane hear Plar	e ne						
	JGRO				Distan	ice Sec	diment	Pipeline					SU	MMAR	Y OF T	EST R	ESULT	S - BO	RING E	3-15
V																		LEL	AP Lab ID	#10001
Fugro C	Consultants, In	c Je	fferso	n Paris	h, Lou	isiana										Project N 04.55	。. 084005			

			ld	entificat	tion Tes	sts		Field She Strength Est		Miniatu Te				(Compres	sion Tests	S			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing	Penetrometer* (ksf)			Remolded Shear	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1				63															
2A	2-3	0.58	66	21	47															
2B	3-4				36					0.51										
3A	4-5																			
3B	5-6				40					0.46										
4A	6-7				41															
4B	7-8				33					0.25	0.53									
5B	9-10				32					0.10										
6A	10-11	0.63	39	21	32															
6B	11-12				35					0.62										
7A	12-13																			
7B	13-14				43					0.45										
8A	14-15				41															
8B	15-16				37					0.36										
9B	17-18	0.73	44	21	38	82	89			0.35										
10B	19-20				39					0.60										
11B	24-25				127	39				0.41		UU	127	17	0.62		0.9	39	2.7	A
12	28.5-30																			
13A	33-34				40		98	0.50												
13B	34-35				58					0.61										
14A	38-39							0.50												
14B	39-40				58					0.42										
15A	43-44																			
15B	44-45				41															
NF *C	tes: ? = Non-Pla orrected as mbols Usec	describ	bed on [·]		and	U UU	- Unco	TEST onfined Com onsolidated - solidated - Ur	Undrai	ned Tria	A xial B al C	YPE OF FA - Bulge - Single Sh - Multiple S - Vertical Fi	ear Plane hear Plai	e ne						
-fi	JGRO	M	S Rive	r Long	Distan	ice Sec	diment	Pipeline					SU	MMAR	Y OF T	EST R	ESULT	S - BO	RING	3-17
V																		LEL	AP Lab ID	#10001
Fugro C	consultants, In	Je	fferso	n Paris	h, Lou	isiana										Project N 04.55	o. 084005			

			ld	entificat	tion Tes	sts		Field She Strength Est		Miniatu Te	re Vane sts			(Compres	sion Tests	6			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	Penetrometer* (ksf)			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				653															
2A	2-3				809															
2B	3-4				180					0.08										
3	4-6				206															
4B	7-8	0.47	94	30	60	61	99			0.27										
5B	9-10				54					0.24										
6B	11-12				57					0.31										
7B	13-14	0.55	00	07	82					0.31										
8A	14-15	0.55	83	27	58					0.22										
8B 9B	15-16 17-18				76 93					0.33	0.15									
9B 10B	19-20				31					0.17	0.15									
11	23-25				47					0.11										
12B	29-30				73	58				0.26		UU	73	20	0.28		1.1	58	8.1	A,B
13	33-35				66					0.20			10	20	0.20				0.1	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
14B	39-40				72					0.20										
NF *C	otes: P = Non-Pla orrected as mbols Used	descril	bed on [•]		and	U UU	I - Unco	TEST onfined Com onsolidated - solidated - Ur	Undrai	ned Tria	A xial B al C	YPE OF FA - Bulge - Single Sh - Multiple S - Vertical F	ear Plane Shear Plar	e ne						
	JGRO				Distan	ce Sec	diment	Pipeline					SU	MMAR	Y OF T	EST R	ESULT	S - BO	RING E	3-18
V																		LEL	AP Lab ID	#10001
Fugro C	Consultants, In	lc Je	fferso	n Paris	h, Lou	isiana										Project N 04.55	。. 084005			

			ld	entifica	tion Tes	sts		Field She Strength Est		Miniatu Te	re Vane sts			(Compres	sion Tests	6			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	Penetrometer* (ksf)			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				230															
2	2-4	1.46	189	43	256															
3B	5-6				70					0.14										
4B	7-8	0.56	70	23	49	73	100			0.09										
5B	9-10				58					0.13										
6B	11-12				56					0.06										
7B	13-14				55					0.06	0.06									
8B	15-16				37					0.11										
9A	16-17	0.86	43	18	40															
9B	17-18				78					0.10										
10B	19-20				41					0.06										
11B	24-25	-1230.53	6 NP	NP	26															
12B	29-30				24		13													
13	33-35				38															
14	38.5-40				24		9													
NF *C	otes: P = Non-Pla orrected as mbols Used	describ	bed on [•]		and	U UU	I - Unco	TEST onfined Com onsolidated - solidated - Ur	Undrai	ned Tria	A xial B al C	/PE OF FAI - Bulge - Single She - Multiple S - Vertical Fi	ear Plane hear Plar	e ne						
	JGRO				Distan	ce Sec	diment	Pipeline				_		MMAR	Y OF T	EST R	ESULT	S - BO		3-19
V	$\equiv \approx$																	LEL	AP Lab ID	#10001
Fugro C	Consultants, In	Je	fferso	n Paris	h, Lou	isiana										Project N 04.55	。 084005			

			ld	entifica	tion Tes	sts		Field She Strength Est		Miniatu Te	re Vane sts			(Compres	sion Tests	S			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	_			Remolded Shear	f Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				264															
2A	2-3	0.81	185	39	158															
2B	3-4				145					0.08										
3	4-5				198															
3B	5-6				357					0.25	0.11									
4B	7-8	0.94	115	34	110	42	99			0.10										
5B	9-10				29															
6B	11-12				49					0.13			-							
7A	12-13	1.01	54	20	54		72													
7B	13-14				73					0.11										
8B	15-16				42					0.20			-							
9B	17-18				77								-							
10A	18-19	0.94	82	25	78															
10B	19-20				70					0.10										
11B	24-25				26	97						UU	26	17	1.82		6.5	97	15.0	A
12	28.5-30				58															
13	33-35				46															
14 15	38.5-40 43.5-45				38 32		96 72													
16A	48-49				52		12	0.50												
16A	49-50				49	73		0.00		0.51		UU	49	34	0.61		0.6	73	7.1	В
17A	53-54				41	70		0.50		0.01					0.01		0.0	10	7.1	
17B	54-55				58			0.00		0.51										
	54.1-				52															
NF *C	otes: P = Non-Pla orrected as mbols Usec	descrit	bed on [·]	Terms a	and	U UL	I - Unco	TEST Defined Componsolidated - solidated - Ur	Undrai	ned Tria	A xial E al C	TYPE OF FA - Bulge - Single Sh - Multiple S - Vertical F	iear Plane Shear Plai	e ne		ı		I	I	
	JGRO				Distan	ce Sec	diment	Pipeline						MMAR	Y OF 1	EST R	ESULT	S - BO	RING E	3-26
V	$\equiv \approx$																	LEL	AP Lab ID	#10001
Fugro C	Consultants, In	Je	fferso	n Paris	h, Lou	isiana										Project N 04.55	o. 084005			

			lde	entificat	tion Tes	sts		Field She Strength Est		Miniatu Te				(Compres	sion Tests	6			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing	-			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
18b	59-60				56	66				0.51		UU	56	41	0.68		0.7	66	3.8	С
*Co	tes: = Non-Plas prrected as mbols Usec	describ	bed on ⁻	Terms a gs.	and	U UU	- Unco	TEST onfined Com onsolidated - solidated - Ur	Undrai	ned Tria	A xial B I C	YPE OF FAI - Bulge - Single She - Multiple S - Vertical Fr	ear Plane hear Plar	e ne						
-fi	IGRO	M	S River	r Long	Distan	ce Sec	diment	Pipeline					SU	MMAR	Y OF T	EST RI	ESULT	S - BO	RING	3-26
V																		LEL	AP Lab ID	#10001
Fugro C	onsultants, In	c Je	ffersor	n Paris	h, Lou	isiana										Project N 04.55	。. 084005			

			ld	entifica	tion Tes	sts		Field She Strength Est		Miniatu Te				(Compres	sion Test	S			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	Penetrometer* (ksf)			Remolded Shear	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0.5-2				182															
2	2-3	1.22	158	36	185															
2B	3-4				208					0.12										
4A	6-7																			
4B	7-8	2.16	44	20	72	60	96			0.11										
5A	8-9	1.05	78	24	81															
5B	9-10				169					0.26										
6A	10-11																			
6B	11-12				83					0.19										
7A	12-13				119		27													
7B	13-14	0.89	86	28	80	53	98			0.09										
8B	15-16				35						0.20									
10	18.5-20				31		87													
11	23.5-25				41															
12	28-30				27		27													
13	33.5-35				22		12													
14	38.5-40																			
15A	43-44	0.63	37	19	31															
15B	44-45				26															
16A	48-49							0.75												
16B	49-50				62	64				0.58		UU	62	34	0.64		0.6	64	3.3	A,C
17A	53-54							0.50												
17B	54-55	0.58	69	23	50	70	100			0.60										
18B	59-60				49	71				0.63		UU	49	41	0.81		0.8	71	4.2	В
NF *C	tes: ? = Non-Pla orrected as mbols Usec	describ	bed on [·]		and	U UU	- Unco	TEST onfined Com onsolidated - solidated - Ur	Undrai	ned Tria	A xial B al C	YPE OF FAI - Bulge - Single She - Multiple S - Vertical Fi	ear Plane hear Plai	e ne						
-fi	JGRO	M	S River	r Long	Distan	ice Sec	diment	Pipeline					SU	MMAR	Y OF 1	EST R	ESULT	S - BO	RING	3-28
$\mathbf{\vee}$																		LEL	AP Lab ID	#10001
Fugro C	Consultants, In	lic Je	ffersoi	n Paris	h, Lou	isiana										Project N 04.55	^{o.} 084005			

			lde	entificat	tion Tes	sts		Field She Strength Est		Miniatu Te				(Compres	sion Tests	6			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	Penetrometer* (ksf)			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				170															
2A	2-3				322															
2B	3-4	0.80	152	41	130	39	98			0.08										
3	4-5				62															
4B	7-8				69					0.12										
5B	9-10				68					0.13										
6A	10-11	1.15	89	30	97															
6B	11-12				103					0.31										
7B	13-14				77					0.12	0.20									
8B	15-16				105					0.23										
9B	17-18				49					0.15										
10B	19-20	0.98	54	21	53	68	100			0.09										
11	23-25	0.95	52	21	50															
12B	29-30				21		16													
14A	38-39				73	59				0.20		UU	73	27	0.38		1.3	59	11.8	A
14B	39-40				32					0.09										
15A	43-44				44															
15B	44-45				64					0.41										
16B	49-50				59	65				0.41		UU	59	34	0.61		0.8	65	6.8	В
17A	53-54				52															
17B	54-55				58					0.44										
18B	59-60				64	63				0.48		UU	64	41	0.57		1.2	63	7.0	С
No	ites:					 TY	PE OF	TEST					ILURE							
NF *Ce	P = Non-Plas orrected as mbols Used	describ	bed on ⁻		and	U UL	- Unco I - Unco	onfined Com onsolidated - solidated - Ur	Undrai	ned Tria	A xial B II C	- Bulge - Single Sh - Multiple S - Vertical Fi	ear Plane hear Plar	e ne						
	JGRO				Distan	ice Se	diment	Pipeline					SU	MMAR	Y OF T	EST R	ESULT	S - BO	RING E	3-38
V																		LEL	AP Lab ID	#10001
Fugro C	Consultants, In	c Je	ffersor	n Paris	h, Lou	isiana										Project N 04.55	。 084005			

			ld	entifica	tion Tes	sts		Field She Strength Est		Miniatu Te				(Compres	sion Tests	6			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing	Penetrometer* (ksf)			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				191															
2	2-4	1.63	232	64	338															
2B	3-4				249															
3B	5-6				55					0.07										
4B	7-8				50					0.14	0.09									
5B	9-10				77					0.13										
6B	11-12				80					0.16										
7B	13-14	1.11	82	26	88	48	99			0.16										
8B	15-16				96					0.11										
9B	17-18				102					0.18										
10A	18-19	0.86	105	28	94															
10B	19-20				67					0.12										
11	23-25				53															
12B	29-30				82	53				0.25		UU	82	20	0.29		1.0	53	9.1	A
13A	33-34				78															
13B	34-35				61					0.23										
14B	39-40				67	60				0.25		UU	67	27	0.35		0.7	60	7.6	А
NF *C	tes: P = Non-Pla orrected as mbols Used	describ	bed on [·]		and	U UU	I - Unco	TEST onfined Com onsolidated - solidated - Ur	Undrai	ned Tria	A xial B I C	YPE OF FA - Bulge - Single Sh - Multiple S - Vertical F	ear Plane hear Plai	e ne						
-fi	JGRO	M	S River	r Long	Distan	ice Sec	diment	Pipeline					SU	MMAR	Y OF 1	EST R	ESULT	S - BO	RING E	3-40
V	=																	LEL	AP Lab ID	#10001
Fugro C	Consultants, In	Je	fferso	n Paris	h, Lou	isiana										Project N 04.55	。 084005			

			ld	entificat	tion Tes	sts		Field She Strength Est		Miniatu Te				(Compres	sion Tests	S			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	Penetrometer* (ksf)			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				378															
2	2-4				221															
3	4-6	1.99	68	20	115															
4B	7-8				277					0.15										
5B	9-10				240					0.12	0.31									
6B	11-12				175					0.13										
7A	12-13	0.79	295	77	250															
7B	13-14				65					0.18										
8B	15-16				97					0.18										
9B	17-18				89					0.13										
10B	19-20				82					0.14										
11B	24-25	2.18	37	17	62	62	99			0.41										
12	28.5-30				65															
13B	34-35				75	56				0.31		UU	75	24	0.36		0.7	56	3.0	А
14A	38-39				36															
14B	39-40				32					0.29										
15B	44-45				34	85				0.31		UU	34	31	0.47		1.1	85	8.1	А
16A	48-49				60															
16B	49-50				51					0.47										
17B	54-55				49	73				0.52		UU	49	38	0.51		0.8	73	4.7	В
18A	58-59				55															
18B	59-60				67					0.63										
NF *Ce	tes: ? = Non-Plas orrected as mbols Usec	describ	bed on [·]		and	U UL	I - Unco	TEST onfined Com onsolidated - solidated - Ur	Undrai	ned Tria	A xial B Il C	YPE OF FA - Bulge - Single Sh - Multiple S - Vertical Fi	ear Plane Shear Plai	e ne						
					Distan		dimont	Pipeline								EST R	E 91 II T	S _ BU		2_/1
J	JGRO			Long	Distail								30						AP Lab ID	
Fugro C	Consultants, In	c Je	fferso	n Paris	h, Lou	isiana										Project N 04.55	。. 084005			

			lde	entificat	tion Tes	sts		Field Shear Strength Estimate			re Vane sts	Compression Tests										
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	Penetrometer* (ksf)			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure		
1	0-1.5				748																	
2B	3-4				215					0.11												
ЗA	4-5	1.19	242	68	276																	
3B	5-6				177					0.14												
4B	7-8				319					0.31	0.15											
5B	9-10				204					0.10												
6B	11-12	1.54	159	40	223	24	83			0.08												
7B	13-14				33					0.15												
8B	15-16				35					0.11												
9B	17-18				98					0.09												
10A	18-19	1.25	66	23	77																	
10B	19-20				72					0.04												
11	23-25				84																	
12B	29-30				80	54				0.21		UU	80	20	0.25		0.8	54	4.3	В		
13A	33-34				73																	
13B	34-35				91					0.21												
14B	39-40				75	57				0.23		UU	75	27	0.28		0.9	57	10.3	А		
Notes: TYPE OF TEST TYPE OF FAILURE NP = Non-Plastic Material U - Unconfined Compression A - Bulge *Corrected as described on Terms and CU - Consolidated - Undrained Triaxial B - Single Shear Plane Symbols Used on Boring Logs. CU - Consolidated - Undrained Triaxial D - Vertical Fracture																						
	JGRO														EST RESULTS - BORING B-42							
U								-									LELAP Lab ID #10					
Fugro Consultants, Inc Jefferson Parish, Louisiana														Project No. 04.55084005								

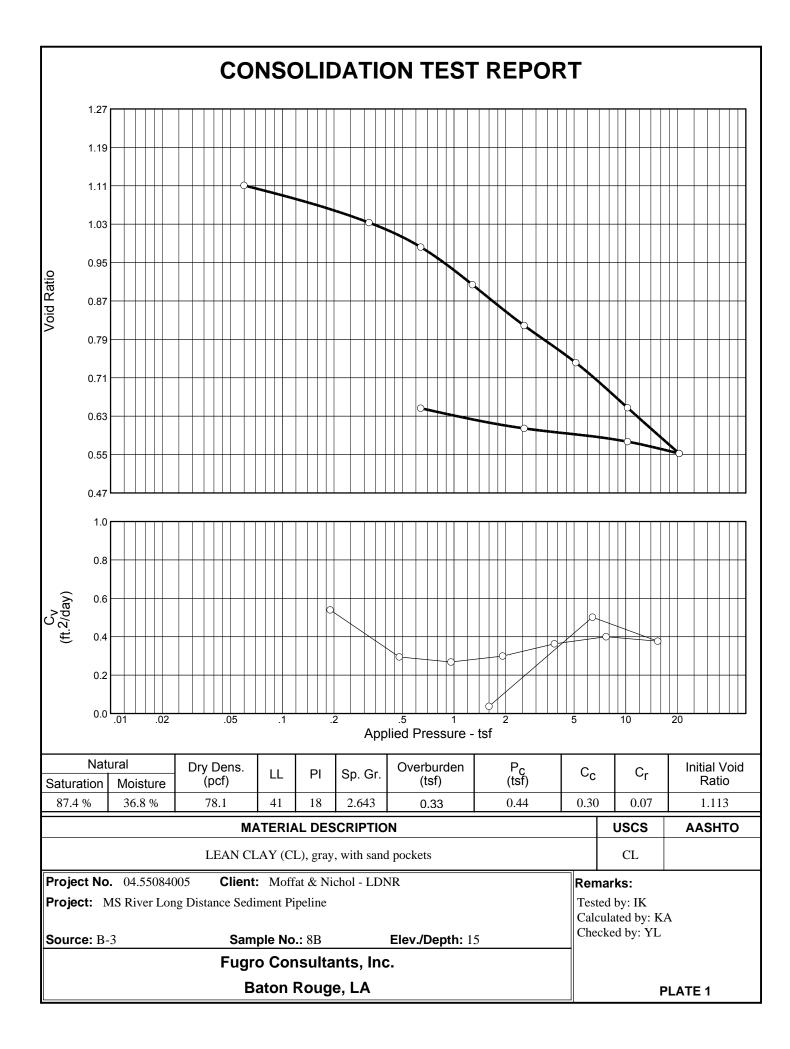
			ld	entifica	tion Tes	sts		Field Shear Miniature Va Strength Estimate Tests				Compression Tests										
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	Penetrometer* (ksf)			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure		
1	0-1.5				379																	
2A	2-3				518																	
2B	3-4	1.23	203	55	236	25	63			0.10												
3B	5-6				61					0.19	0.30											
4B	7-8				40					0.51												
5B	9-10				106			0.75		0.64												
6A	10-11	0.54	88	36	64																	
6B	11-12				78					0.25												
7B	13-14				94																	
8B	15-16				153					0.39												
9B	17-18				171					0.19												
10B	19-20	0.70	200	52	156	31	73			0.11												
11	23-25	1.11	62	22	67																	
12	28-30				78																	
13B	34-35				77	55				0.12		UU	77	24	0.37		0.6	55	3.2	А		
14A	38-39				76																	
14B	39-40				72					0.28												
15B	44-45				74	55				0.33		UU	74	31	0.49		0.9	55	4.1	В		
16A	48-49				61																	
16B	49-50				61					0.33												
17A	53-54				73	58						UU	73	38	0.56		0.7	58	2.5	В		
17B	54-55				72					0.28												
18A	58-59				63																	
18B	59-60				69					0.35												
Notes: TYPE OF TEST TYPE OF FAILURE NP = Non-Plastic Material U - Unconfined Compression A - Bulge *Corrected as described on Terms and CU - Consolidated - Undrained Triaxial B - Single Shear Plane Symbols Used on Boring Logs. CU - Consolidated - Undrained Triaxial D - Vertical Fracture																						
-fi	JGRO	M													UMMARY OF TEST RESULTS - BORING B-43							
I							_									LELAP Lab ID #10001						
Fugro C	consultants, In	lic Je	fferso	n Paris	h, Lou	isiana										Project N 04.55	et No. 55084005					

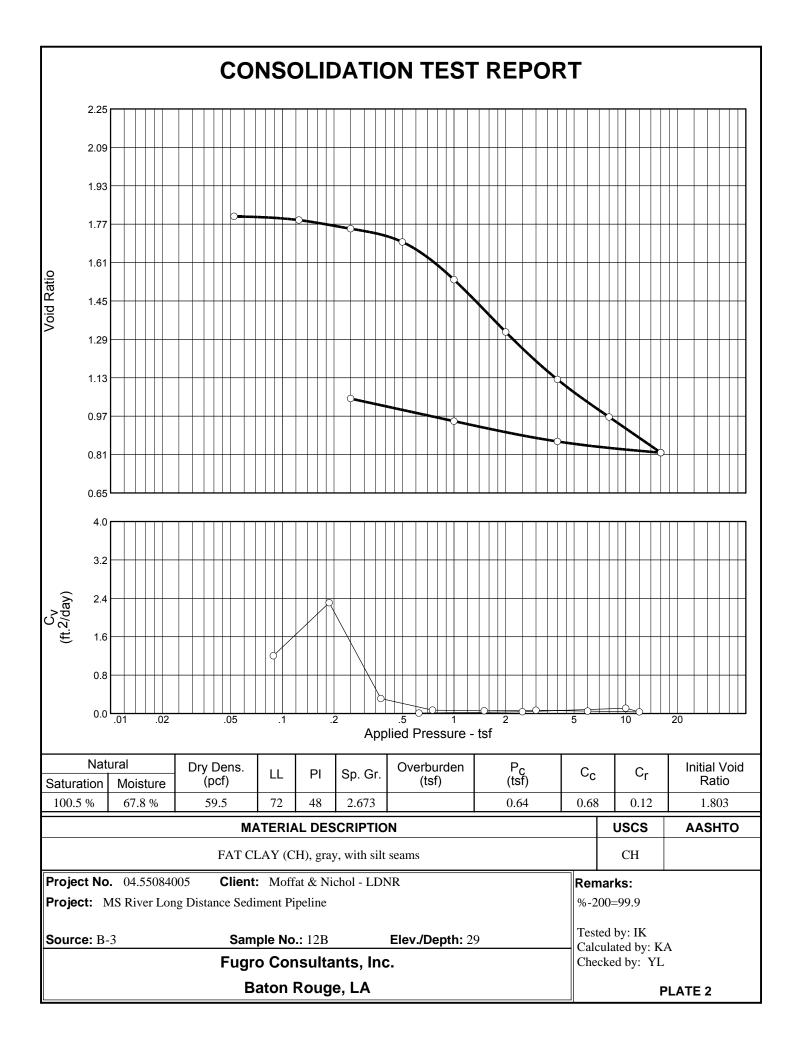
			lde	entificat	tion Tes	sts		Field Shear Miniature Var Strength Estimate Tests				Compression Tests											
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200	_	Torvane (ksf)		Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure			
16A	48-49							0.50															
16B	49-50				60	64				0.50		UU	60	34	0.76		0.8	64	2.5	С			
17A	53-54							0.50															
17B	54-55	0.60	85	27	62		100	0.50		0.65													
18A 18B	58-59 59-60				51	69		0.50		0.61		UU	51	41	0.70		1.0	69	5.3	В			
Тор	59-60				51	09				0.01		00	51	41	0.70		1.0	69	5.5	В			
NP *Co	tes: = Non-Plas prrected as mbols Usec	describ	U - Unconfined Compression UU - Unconsolidated - Undrained Triaxial CU - Consolidated - Undrained Triaxial										TYPE OF FAILURE A - Bulge B - Single Shear Plane C - Multiple Shear Plane D - Vertical Fracture										
-ft	JGRO	M													SUMMARY OF TEST RESULTS - BORING B-17								
																	LELAP Lab ID #1						
Fugro C	onsultants, In	c Je	Jefferson Parish, Louisiana													Project No. 04.55084005							

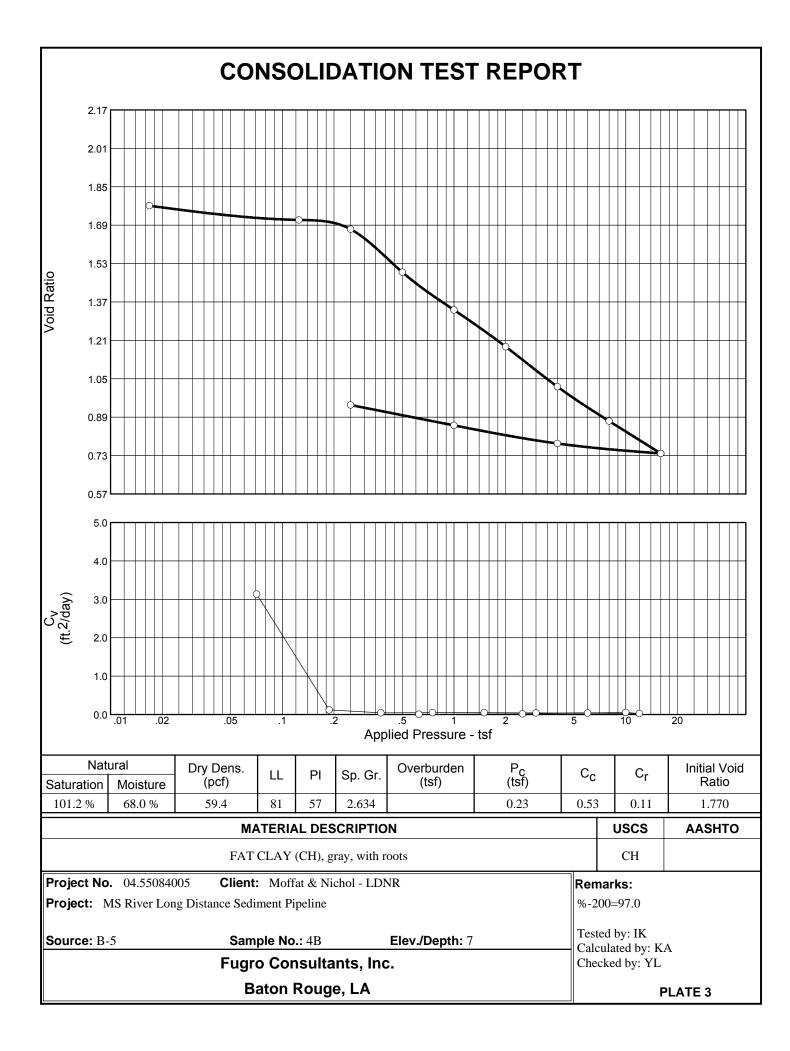


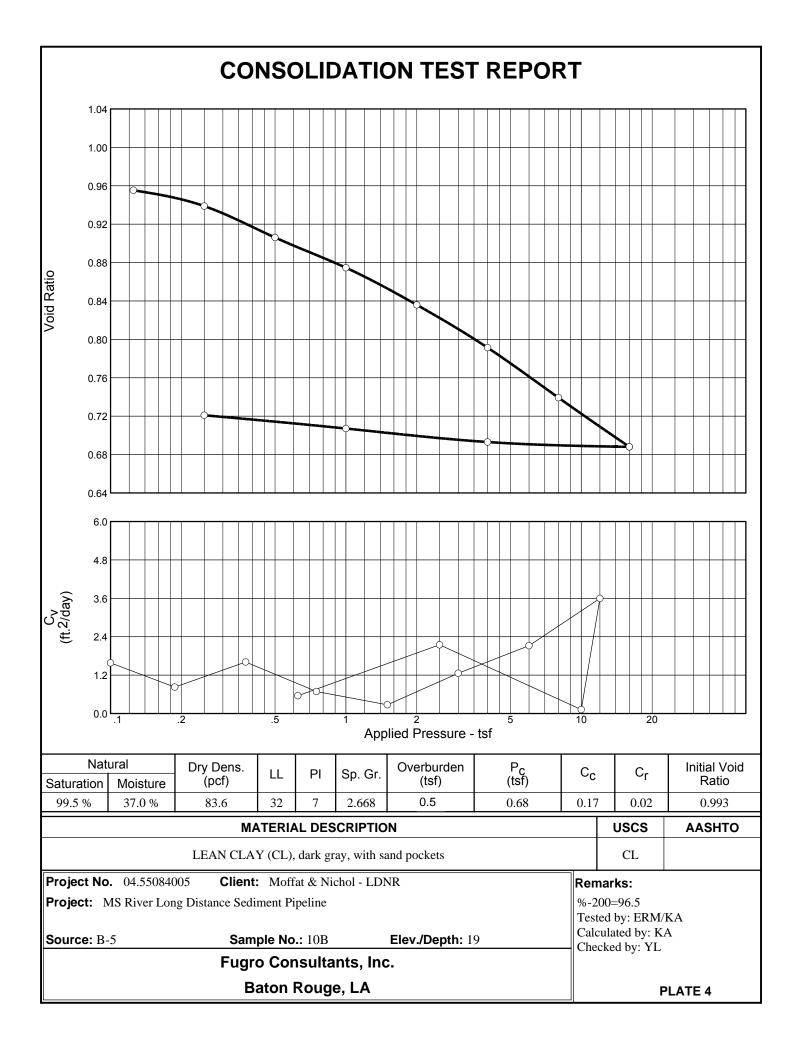
APPENDIX B

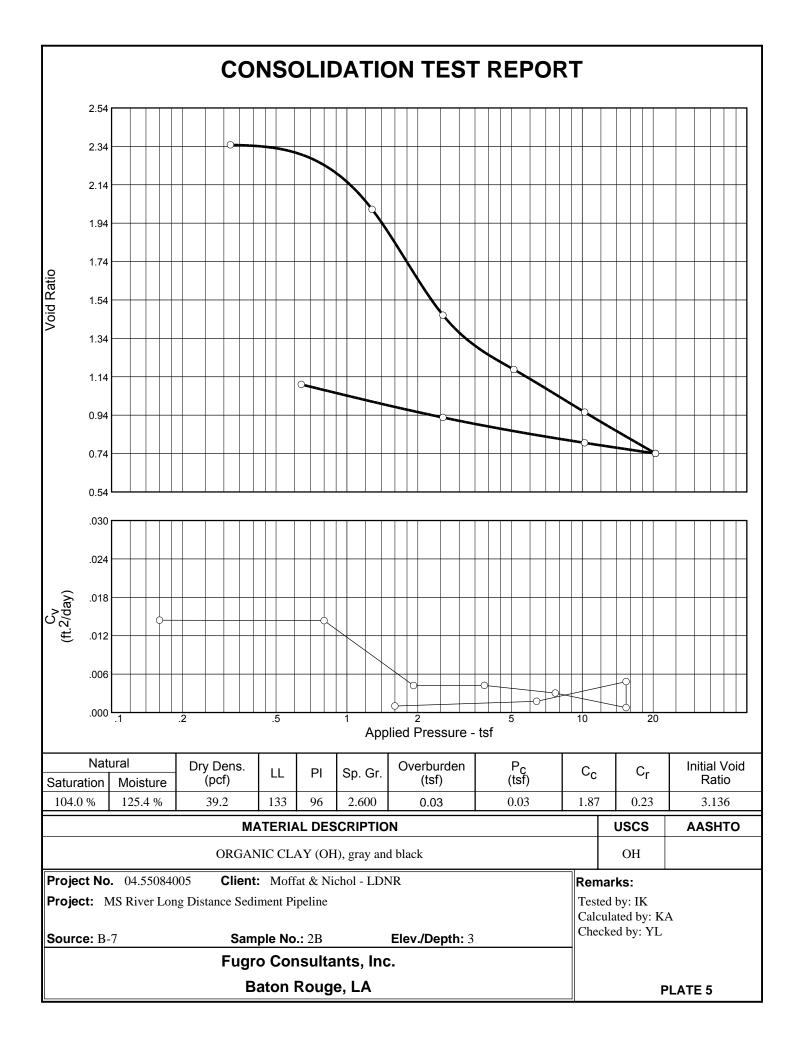
ONE DIMENSIONAL CONSOLIDATION TEST RESULTS

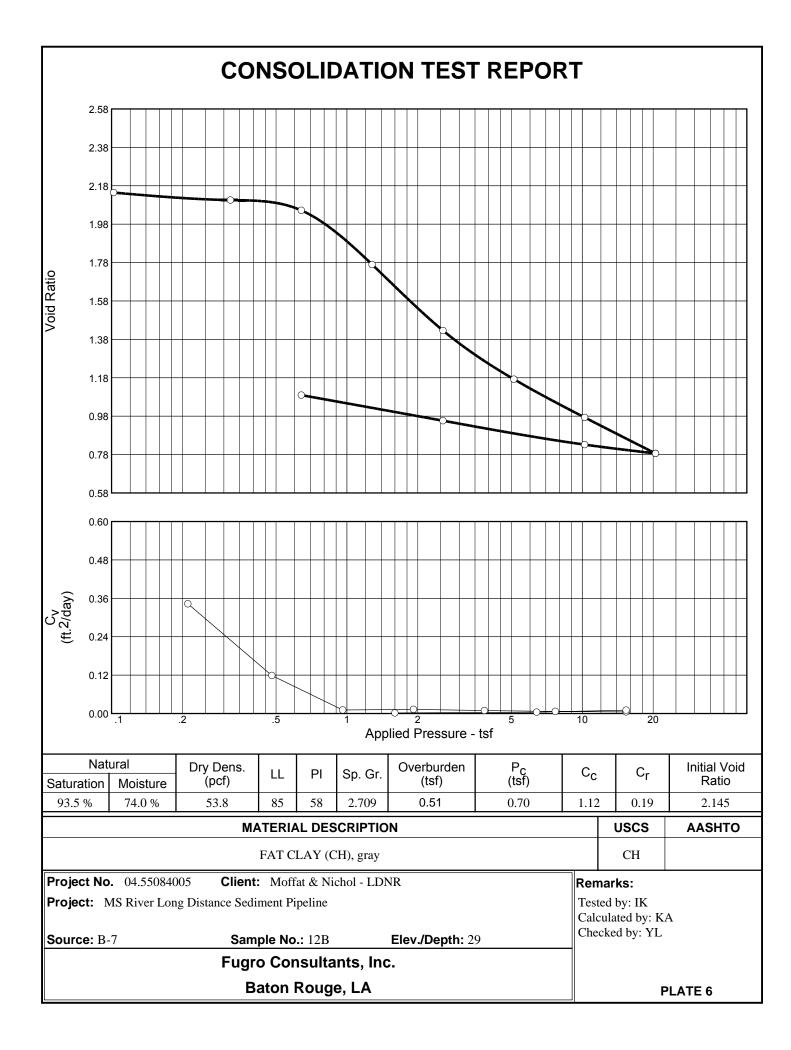


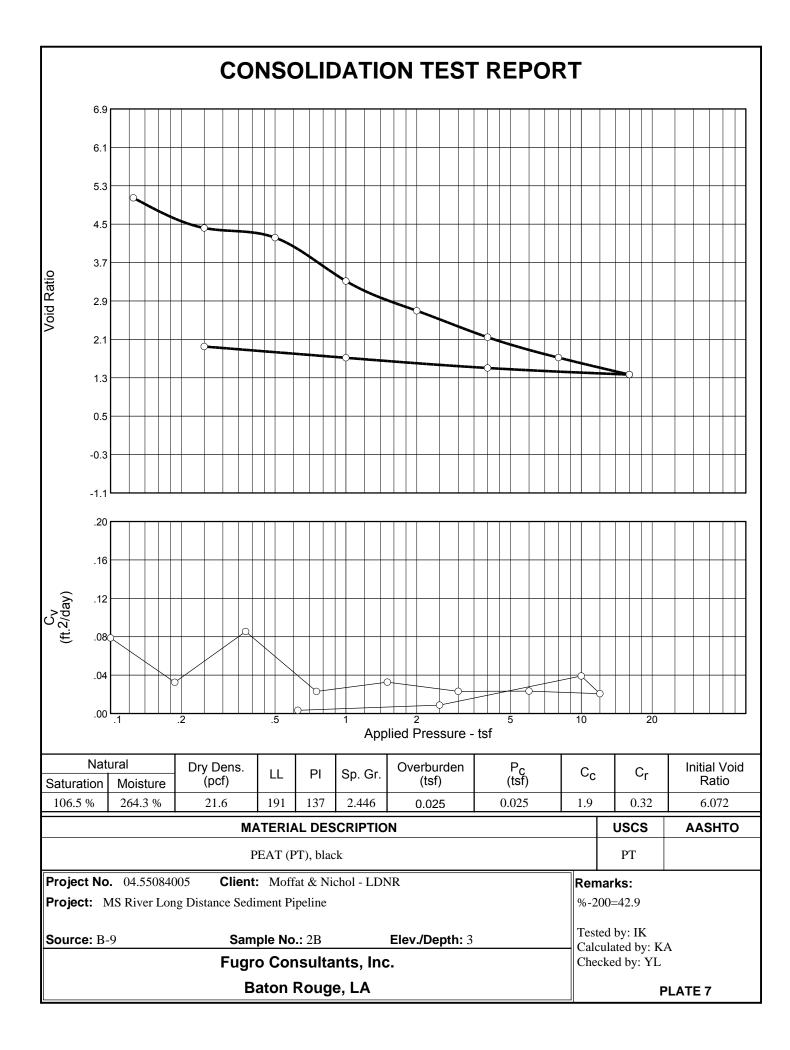


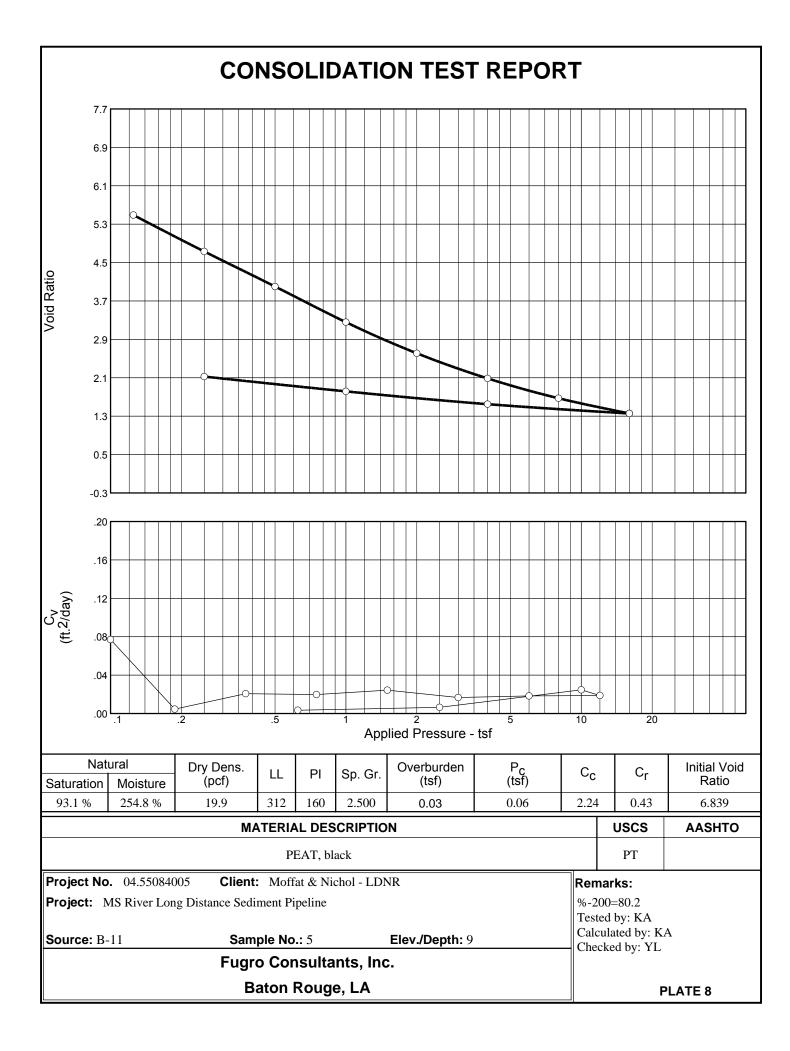


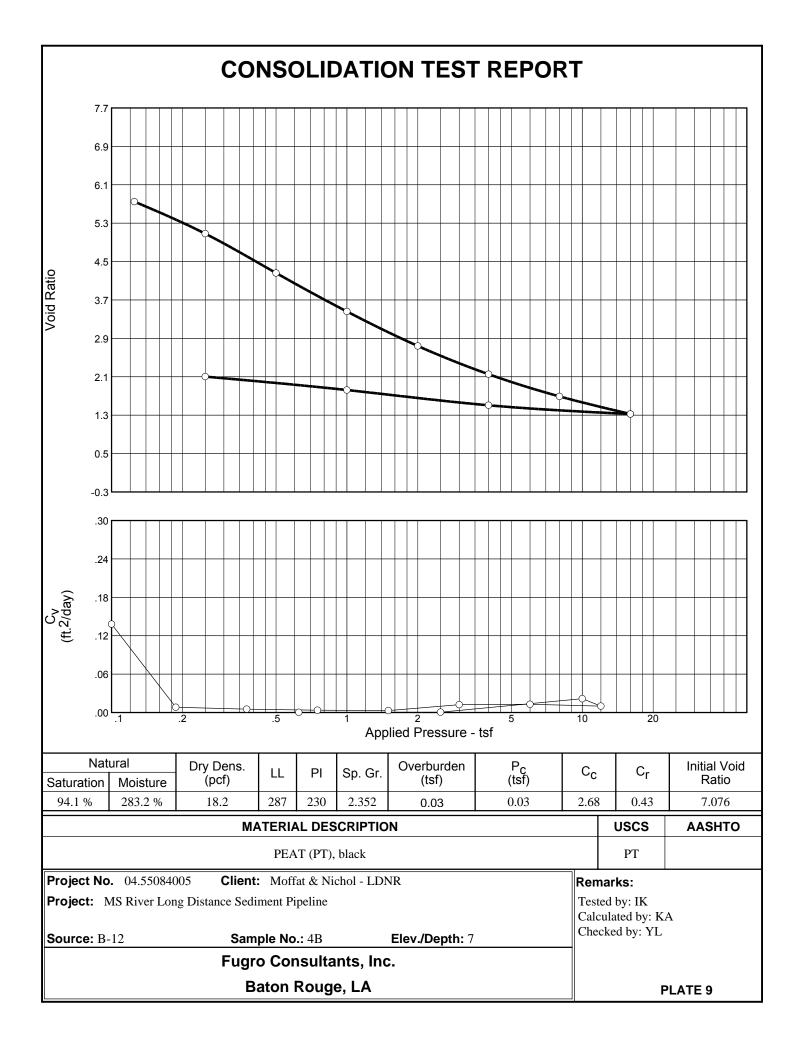


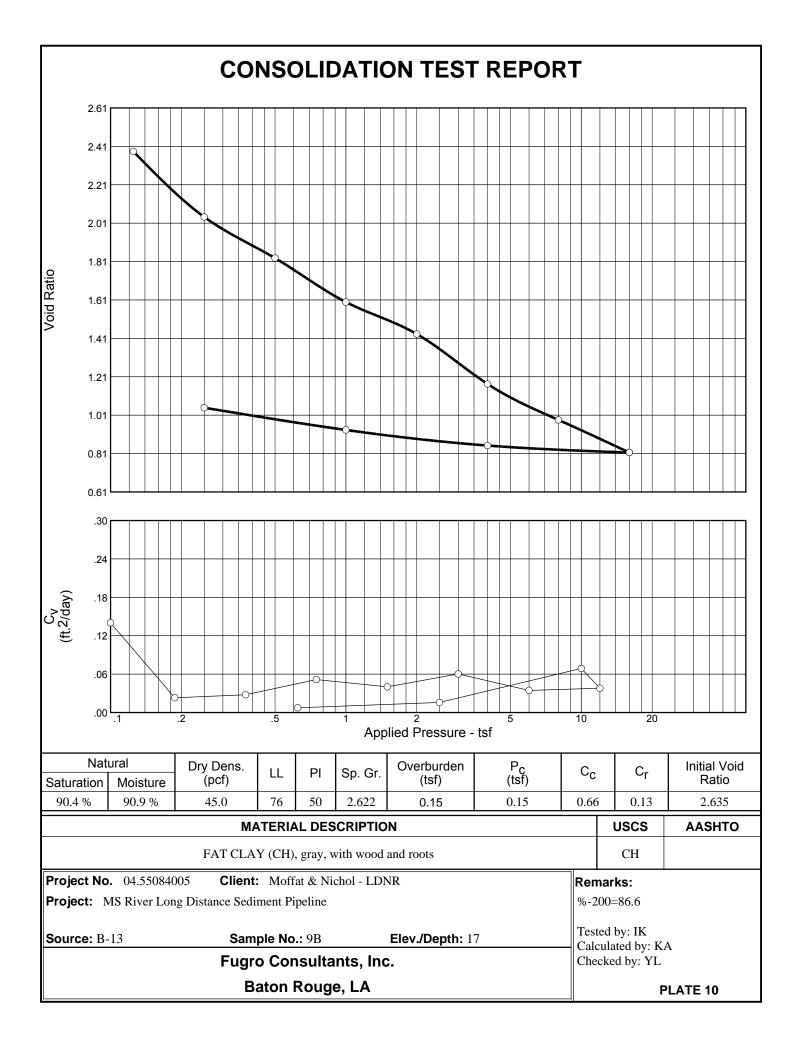


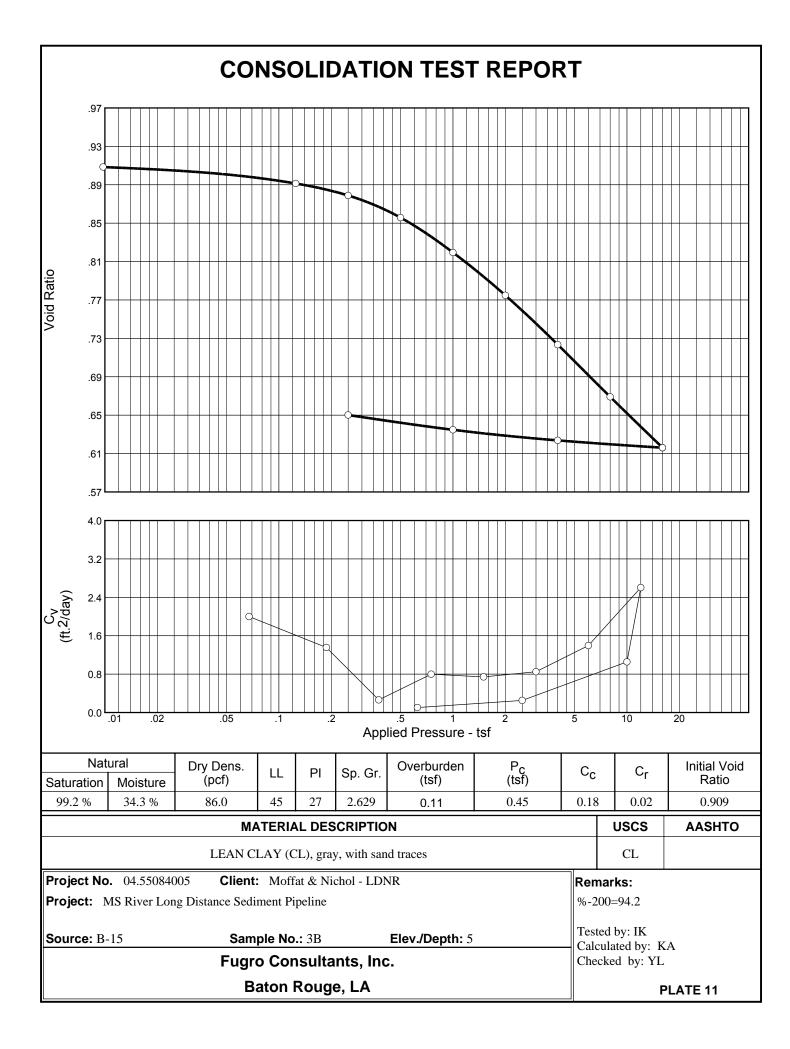


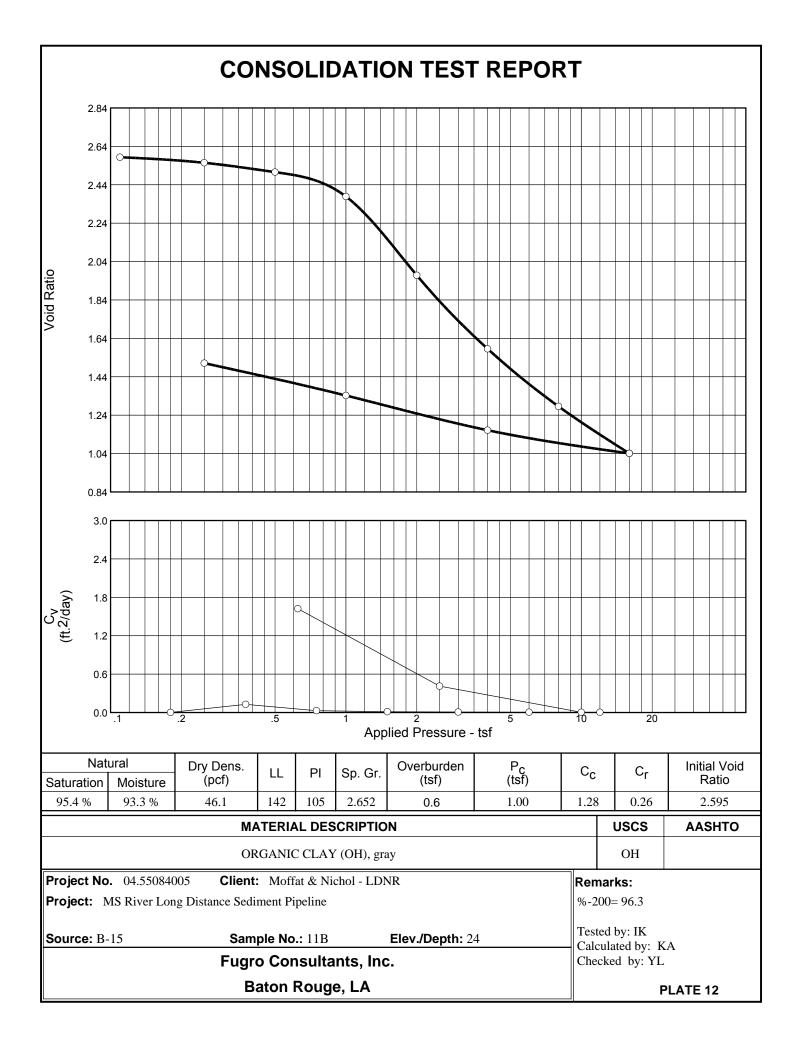


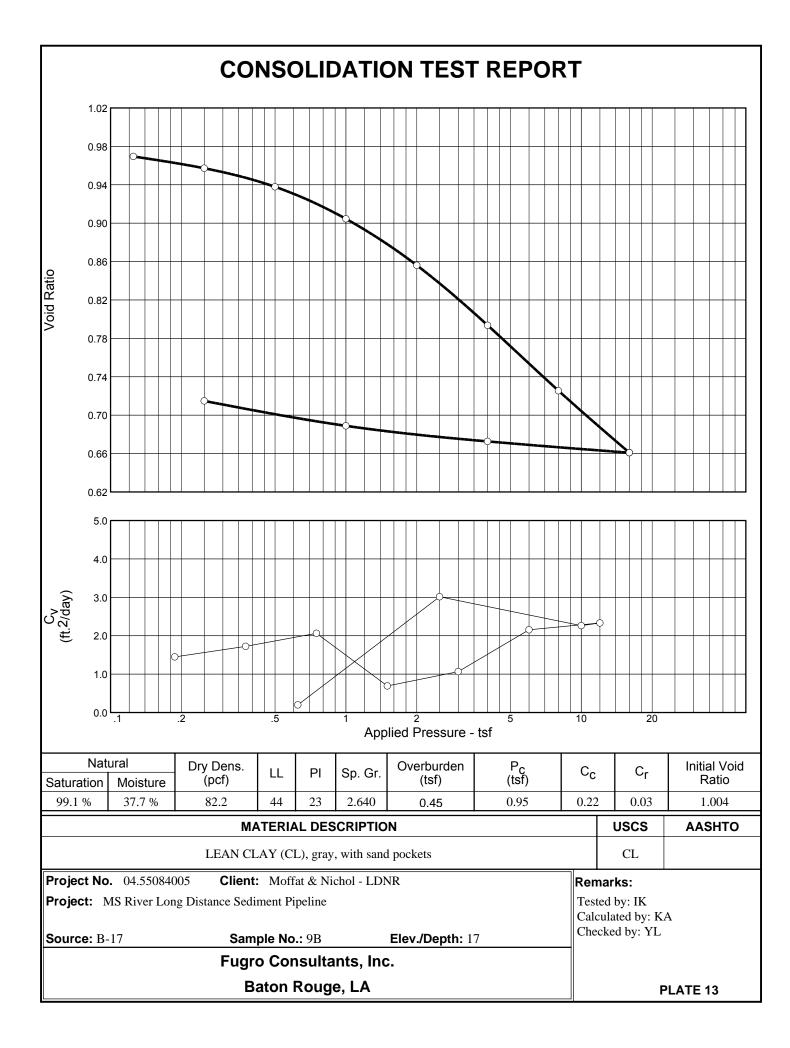


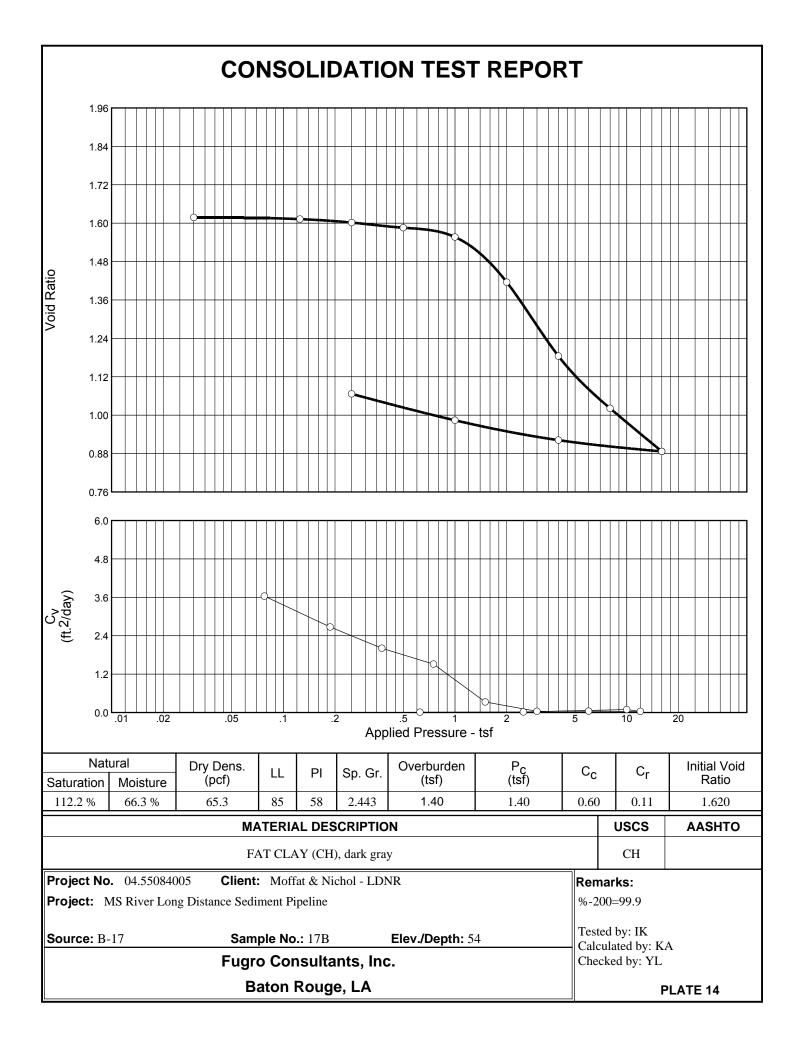


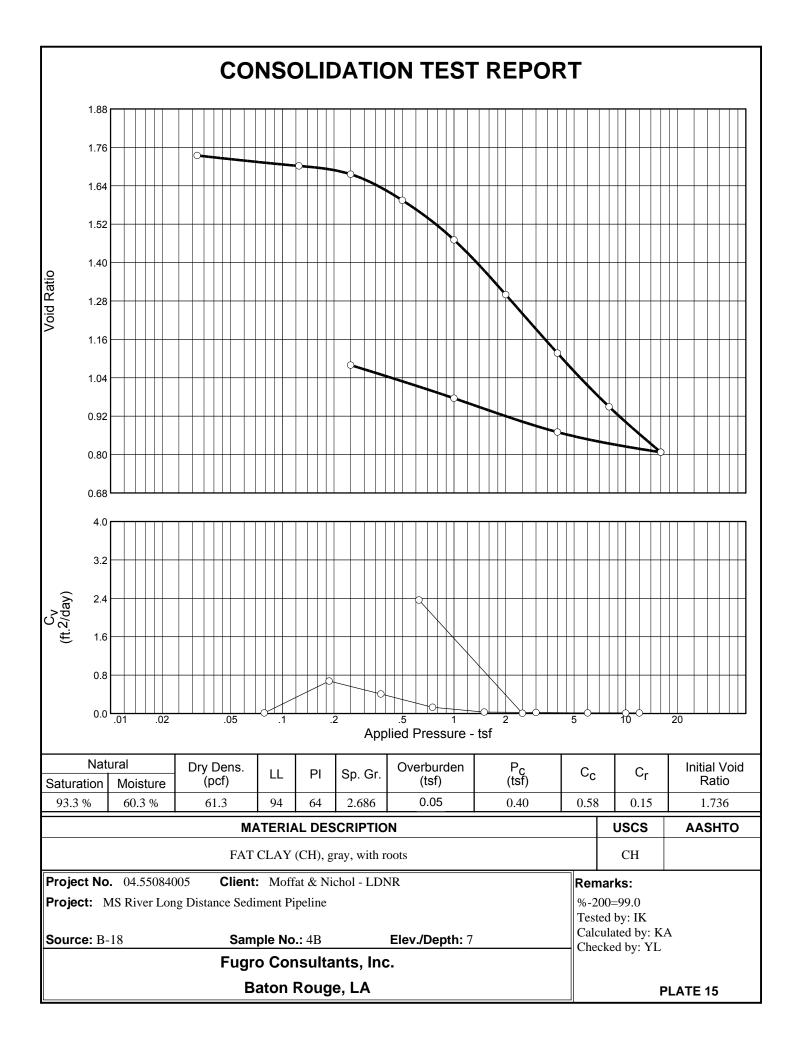


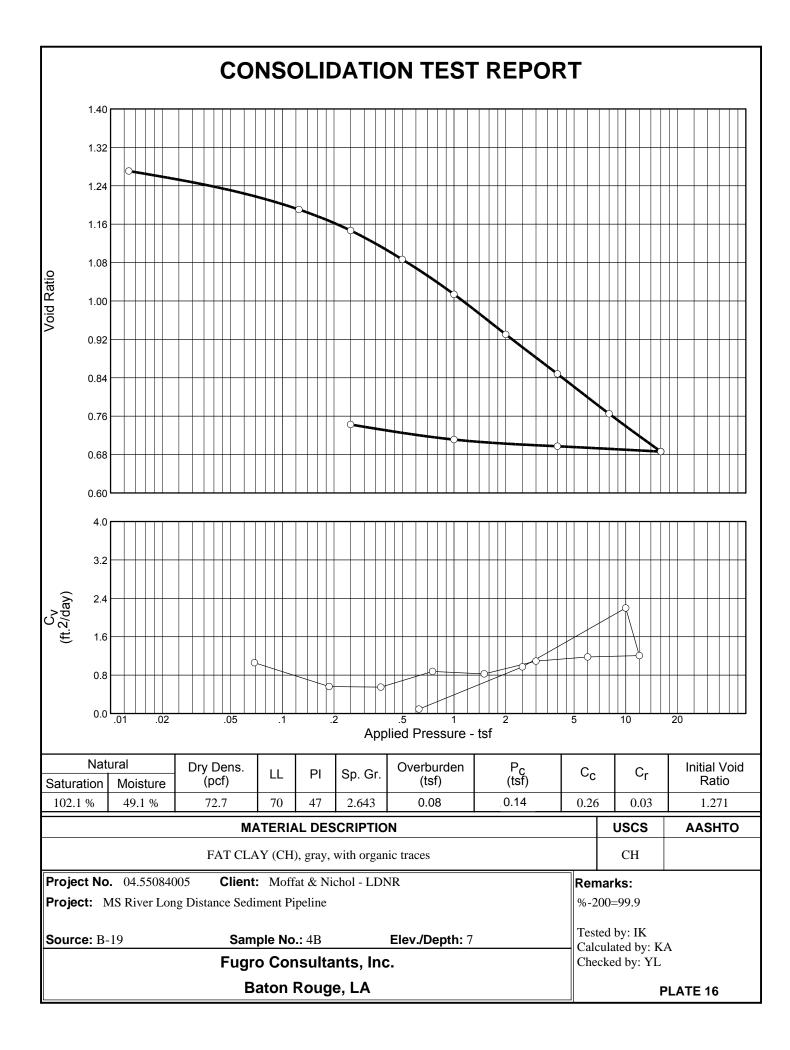


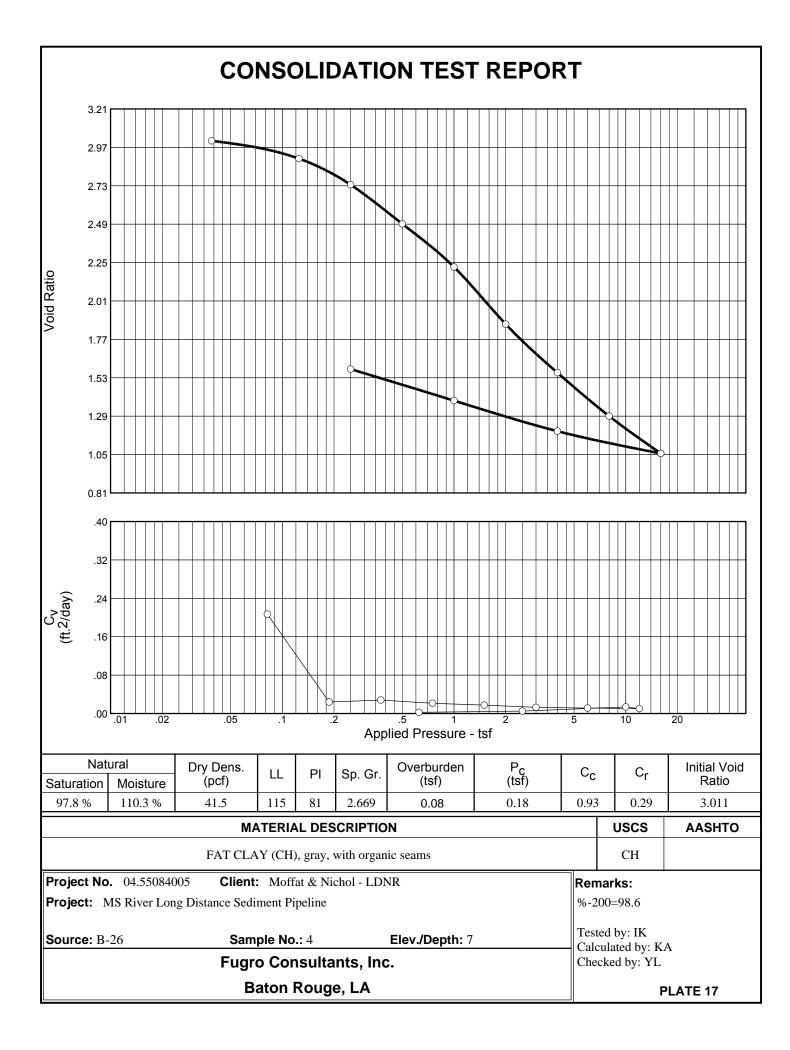


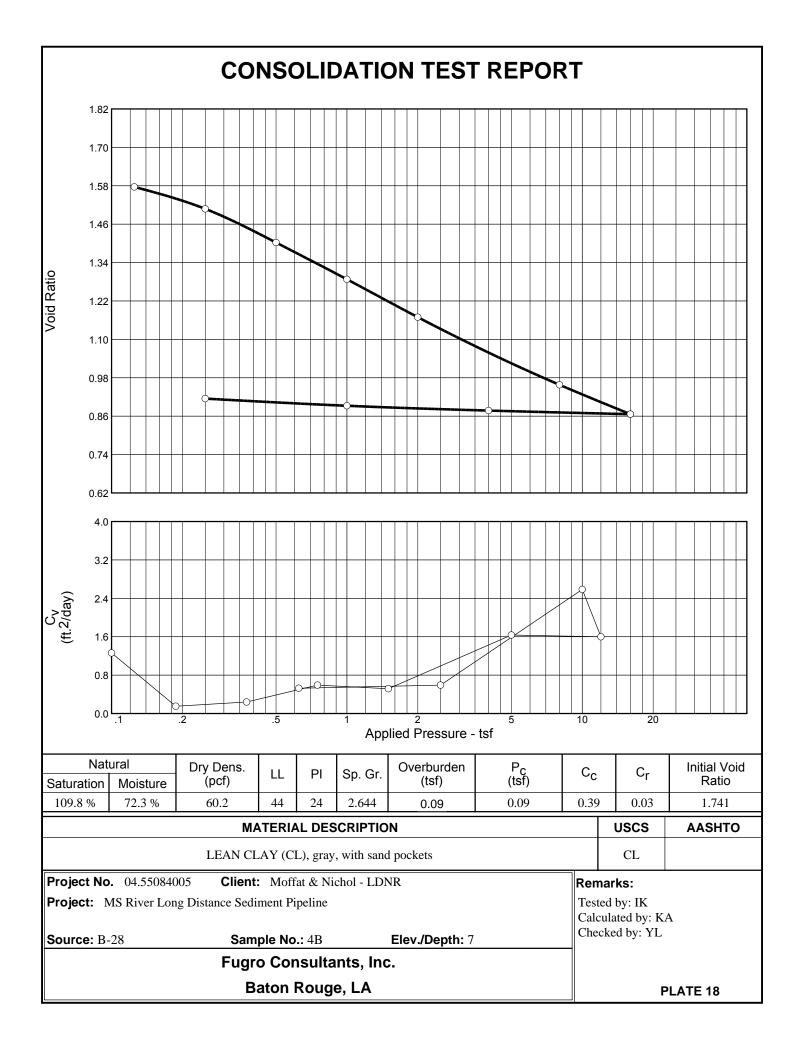


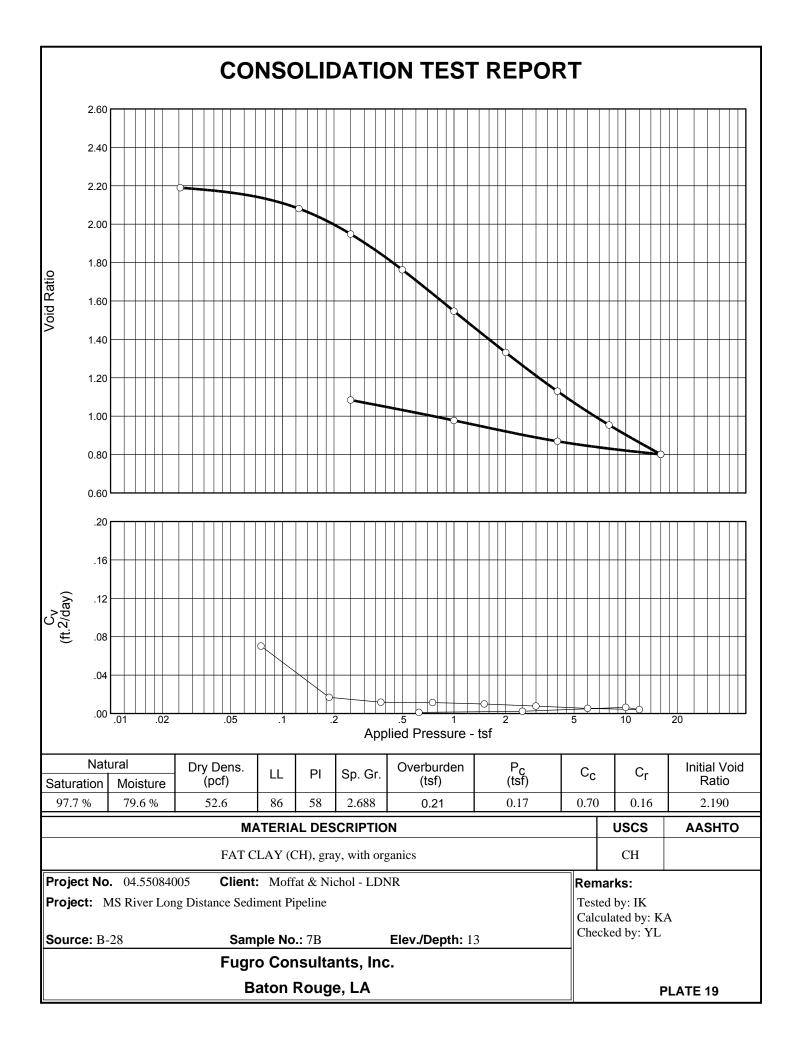


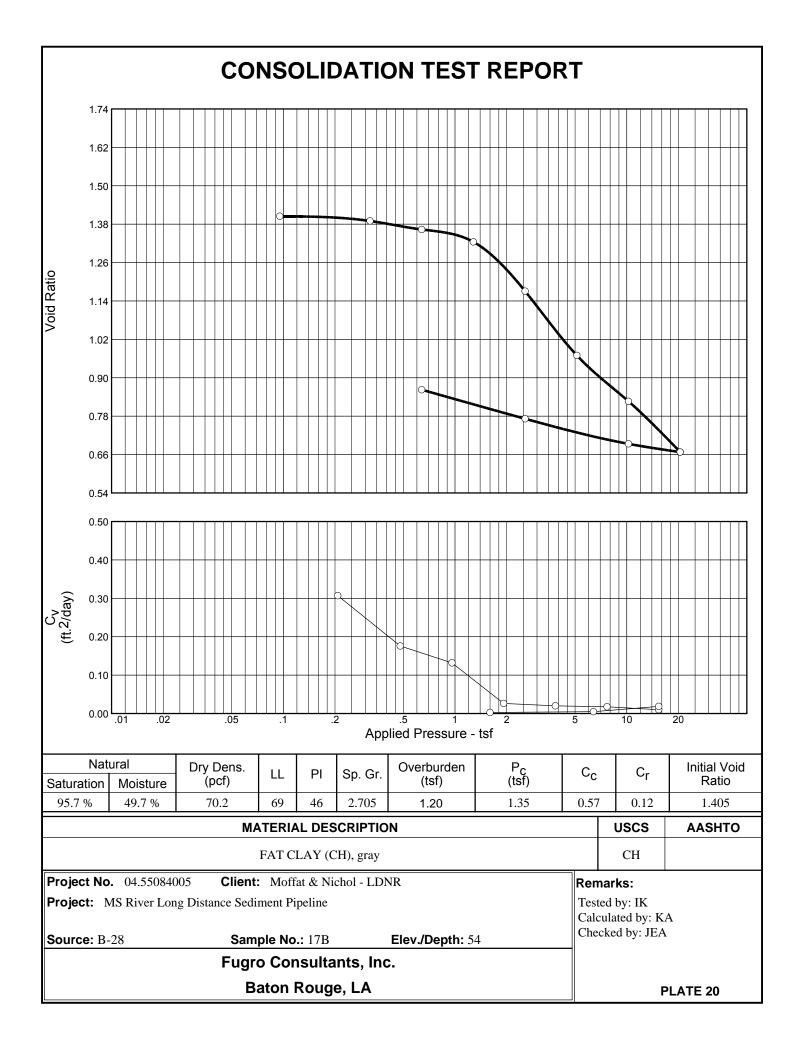


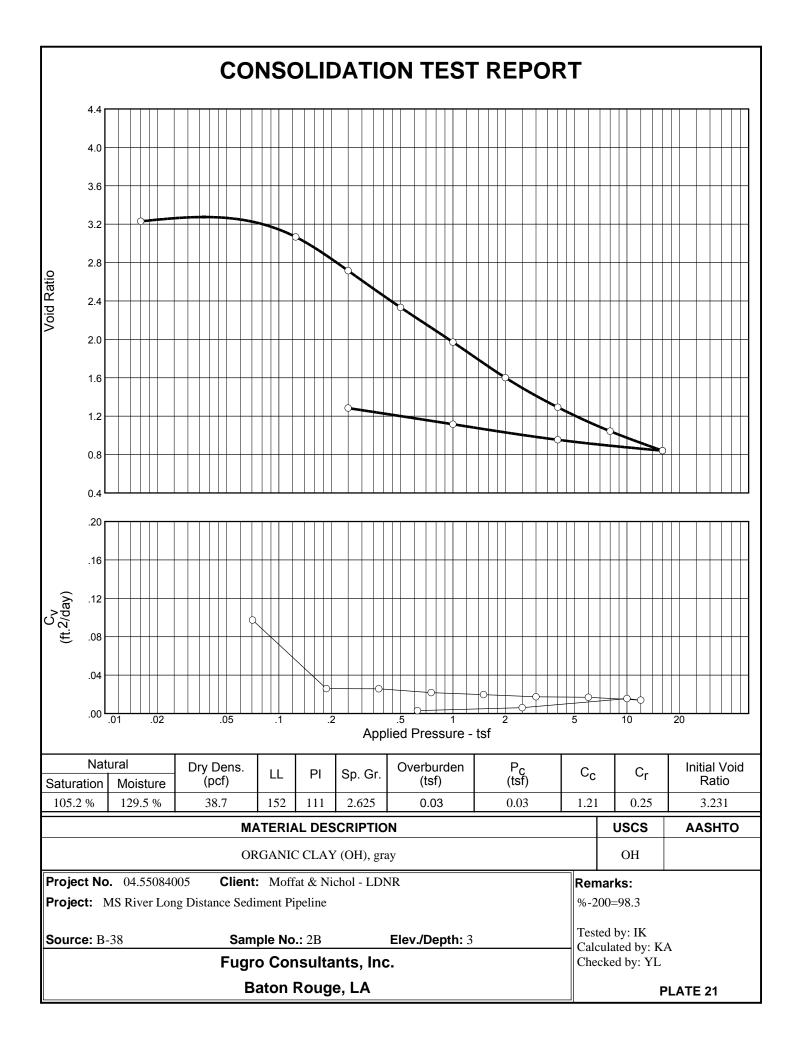


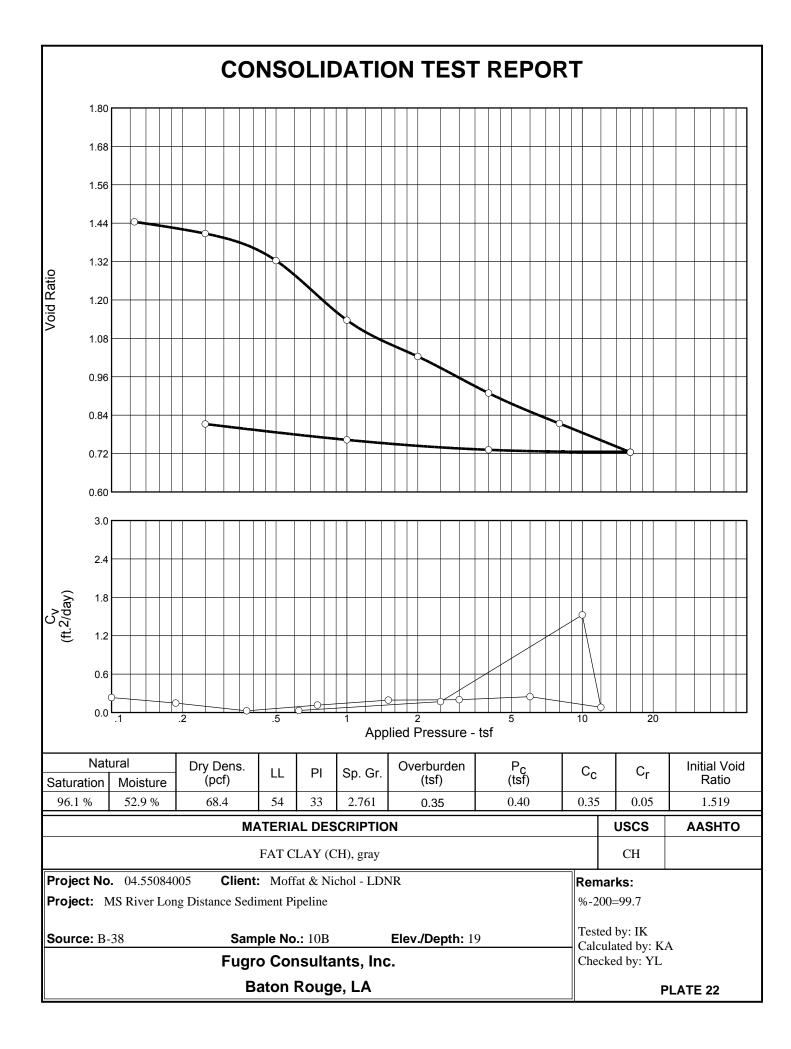


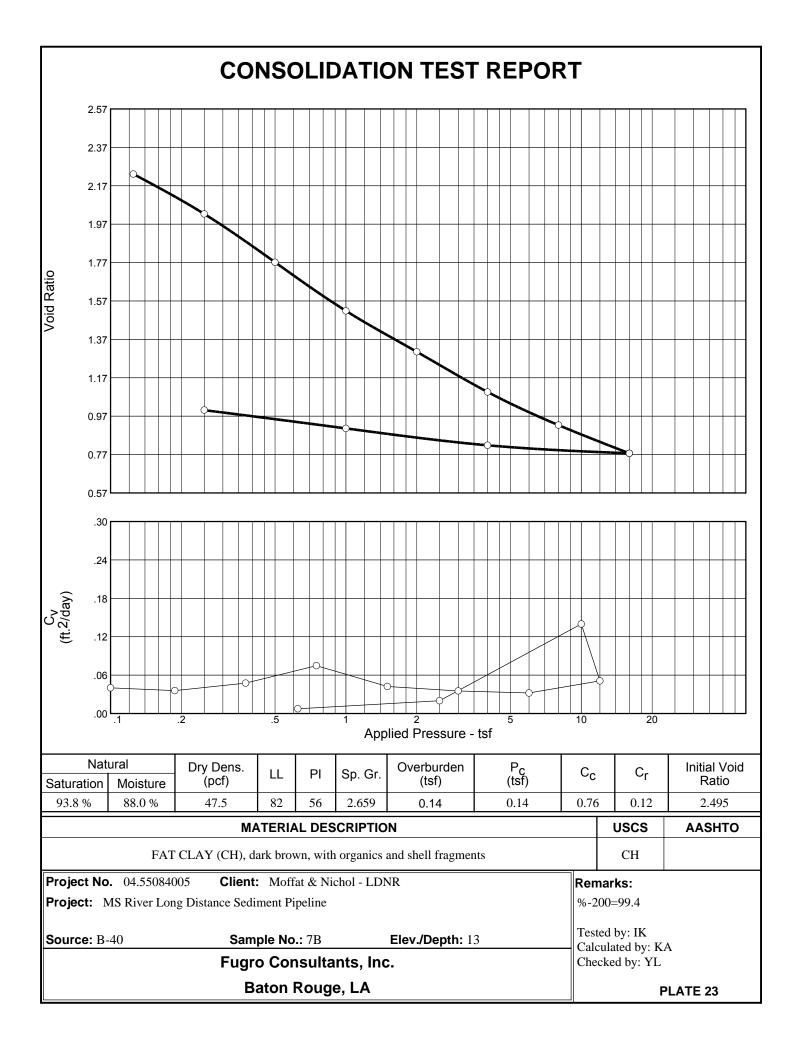


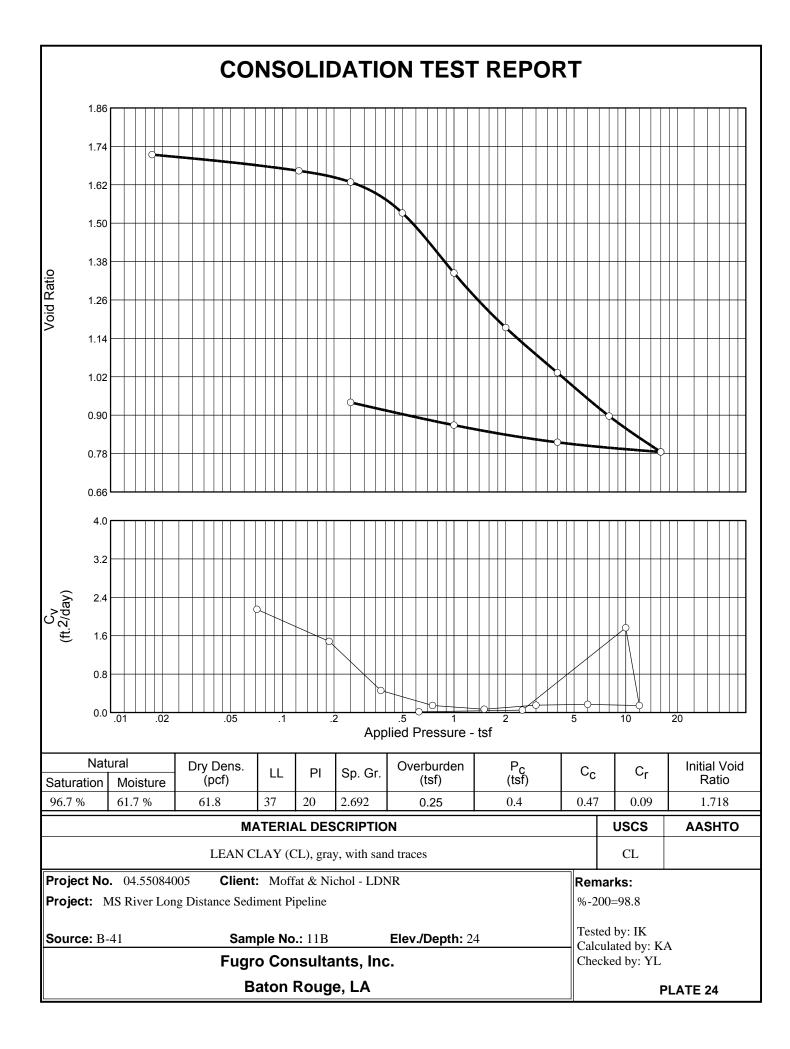


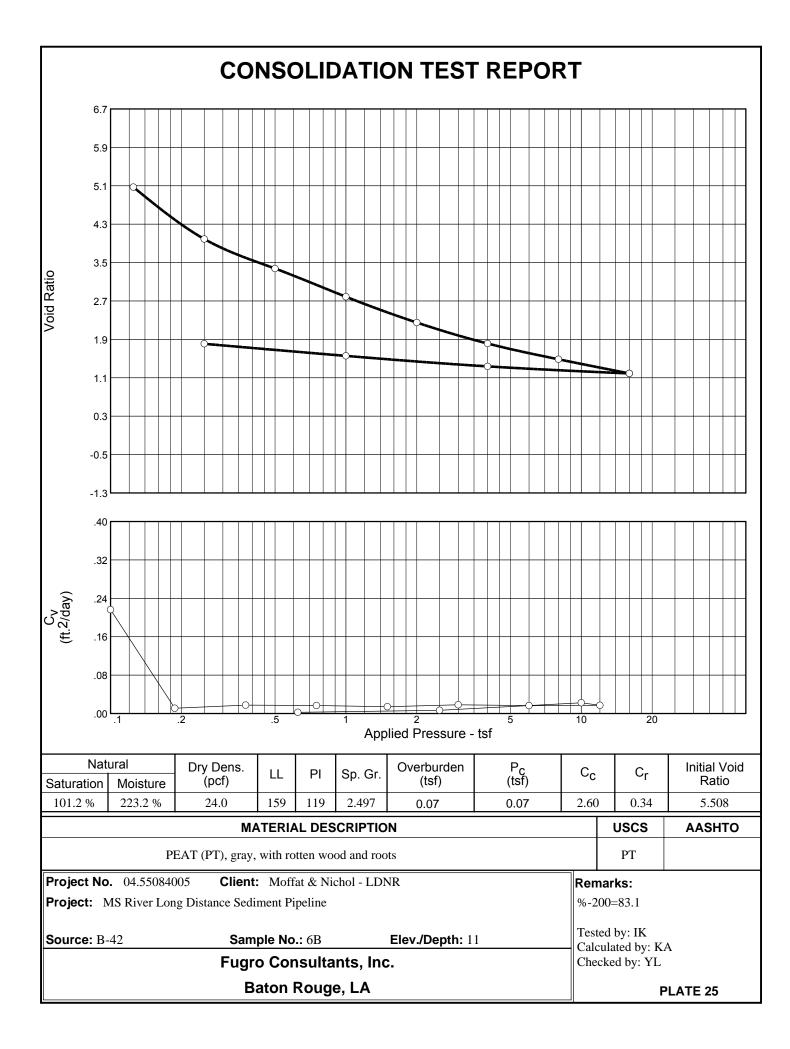


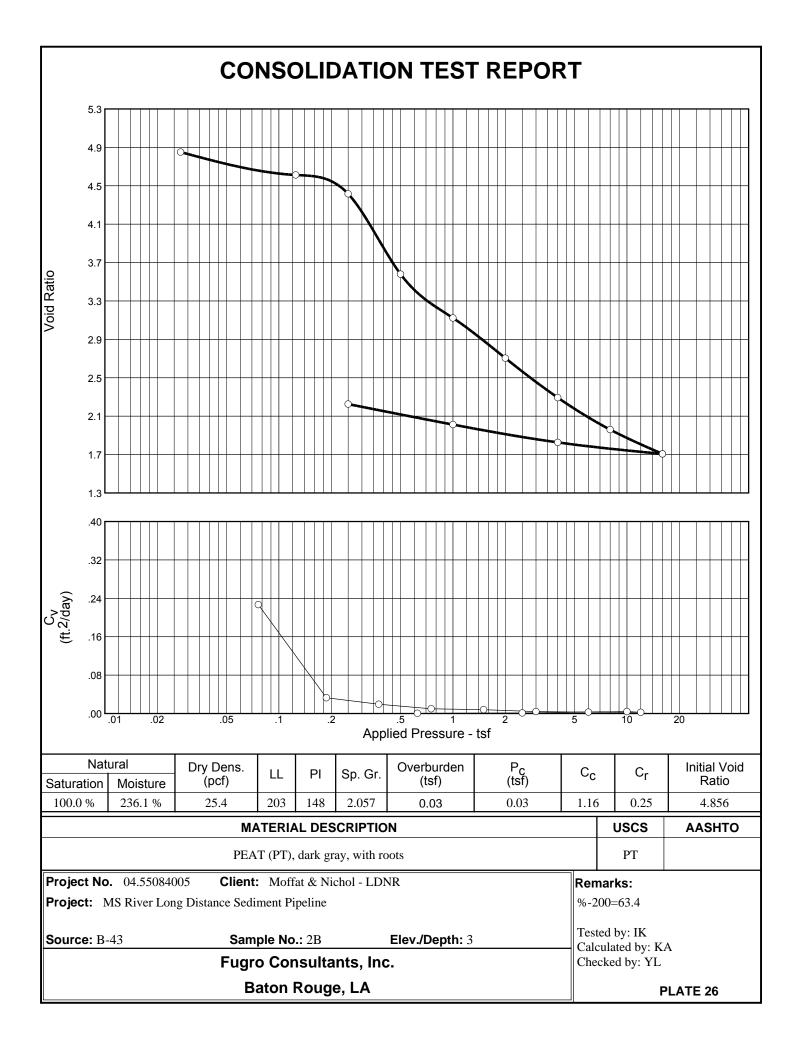


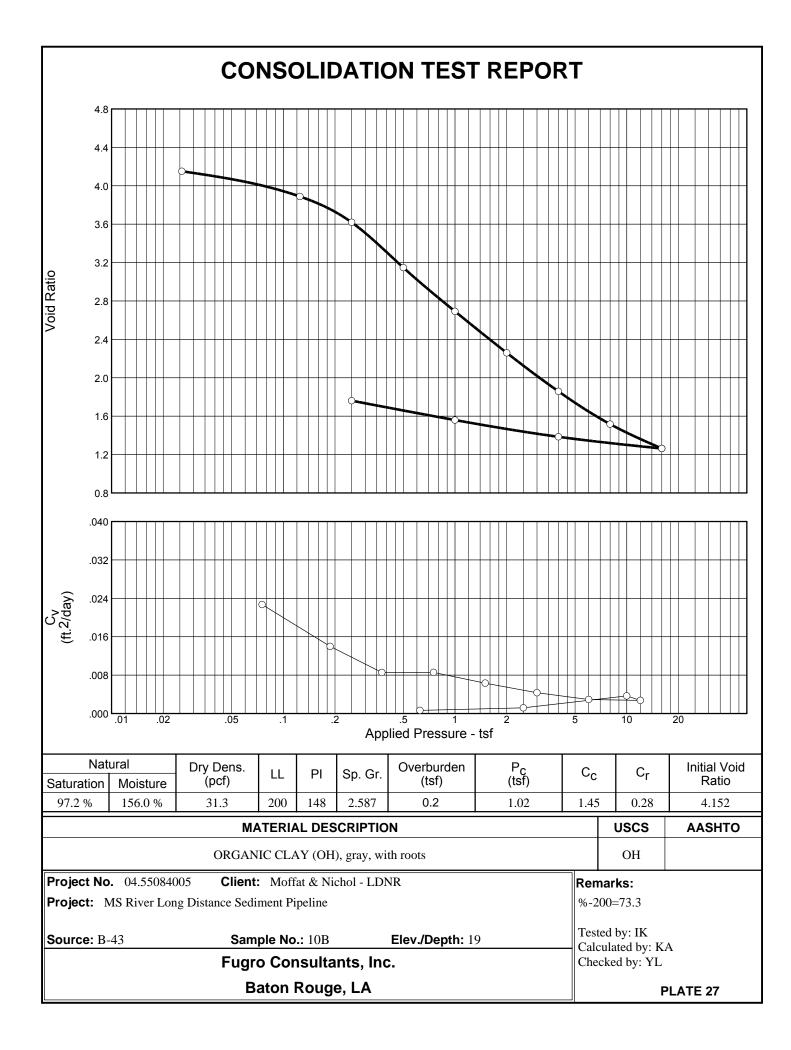












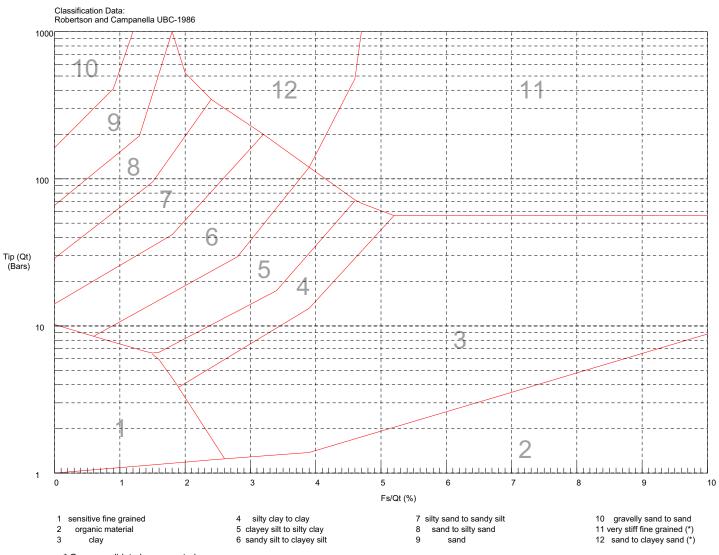


APPENDIX C CONE PENETRATION TEST LOGS





12 Zone Soil Behavior Chart



* Overconsolidated or cemented

Location Baton Rouge-LA



Job Number 04.5508-4005

David Cline

CPT Number CPT-01

Cone Number A15F2.5CKE2H2403

Client Fugro Consultants, Inc.

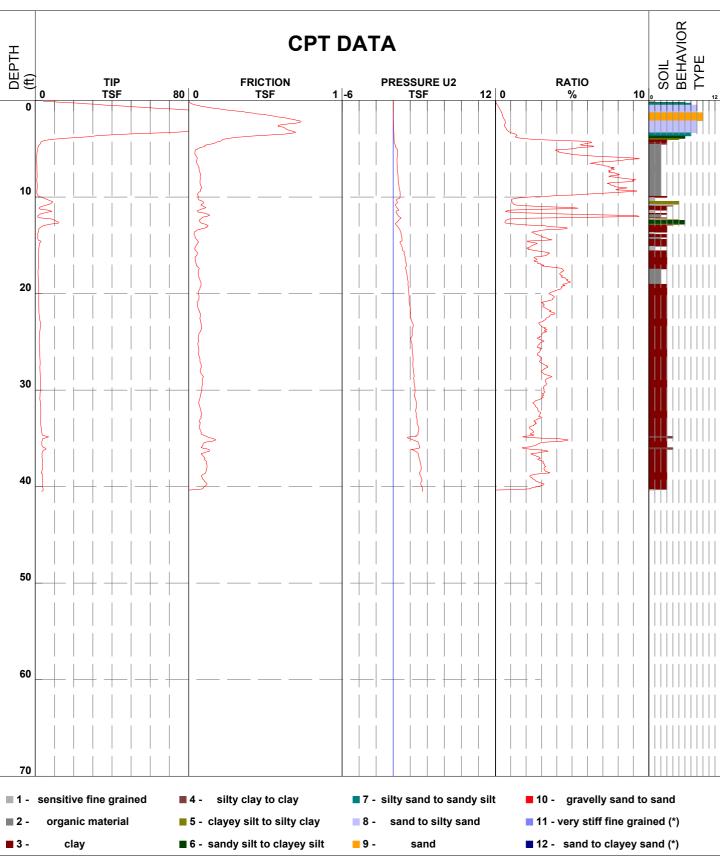
Operator

Date and Tin <u>24-Aug-2011 14:16:29</u>

1.2'

Elevation

Coordinate:N 29 39 18.8 W 90 00 50.3



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA

TUGRO

Job Number 04.5508-4005

David Cline

CPT Number CPT-02

Cone Number A15F2.5CKE2H2403

Client Fugro Consultants, Inc.

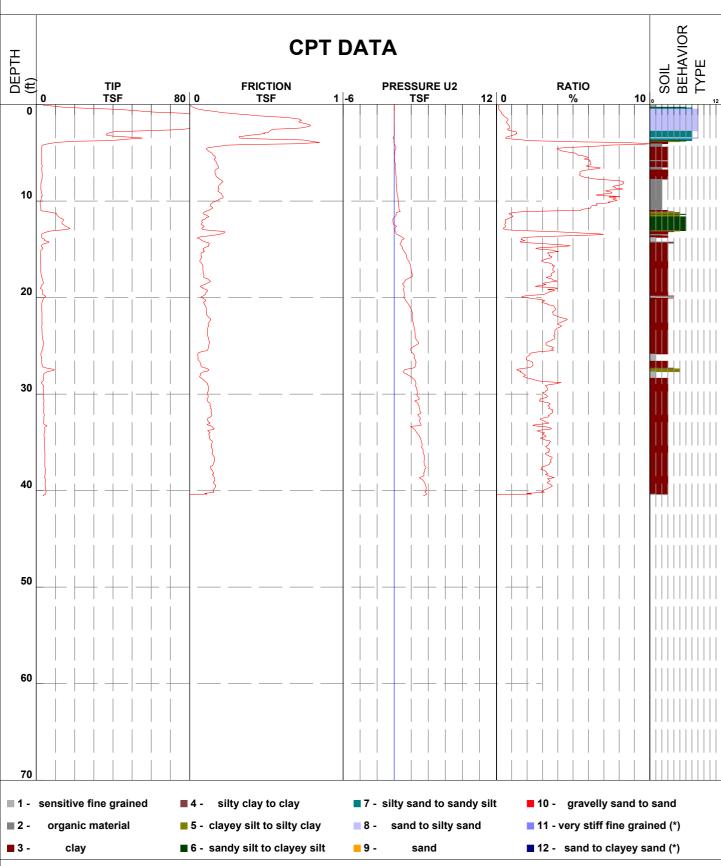
Operator

Date and Tin 25-Aug-2011 07:52:39

2.1'

Elevation

Coordinate:N 29 39 11.4 W 90 01 07.3



Robertson et al. 1986 * Overconsolidated or Cemented

Elevation



Job Number 04.5508-4005

Fugro Consultants, Inc.

CPT Number CPT-03

Location Baton Rouge-LA
Cone Number A15F2.5CKE2H2403

Operator David Cline

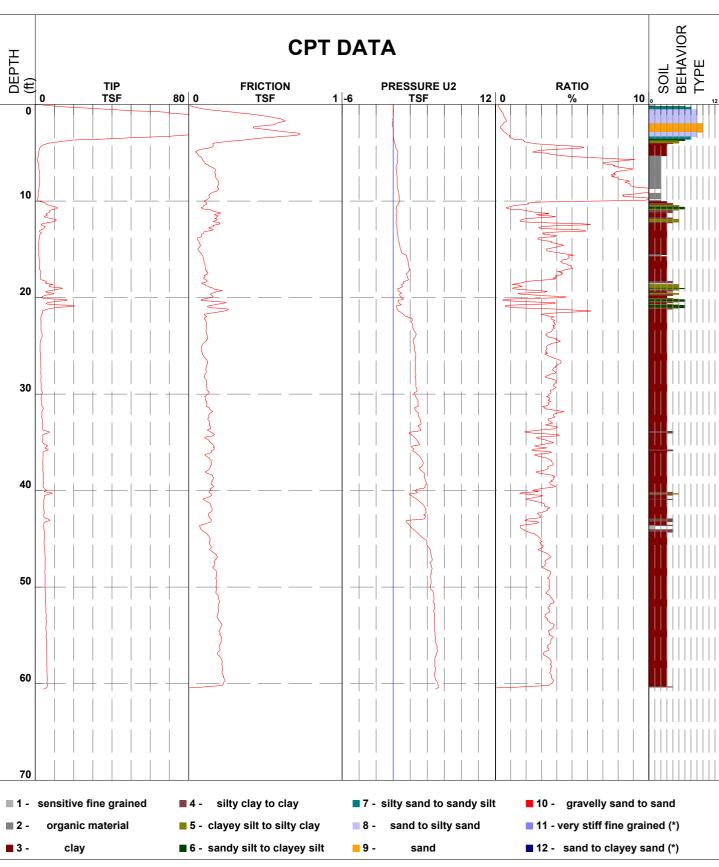
Client

Date and Tir 18-Aug-2011 09:28:47

1.5'

Coordinate

Coordinate N 29 39 09.1 W 90 01 25.4



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA



Job Number 04.5508-4005

Herbert Jackson

CPT Number CPT-04

1.3'

Cone Number A15F2.5CKE2H2403

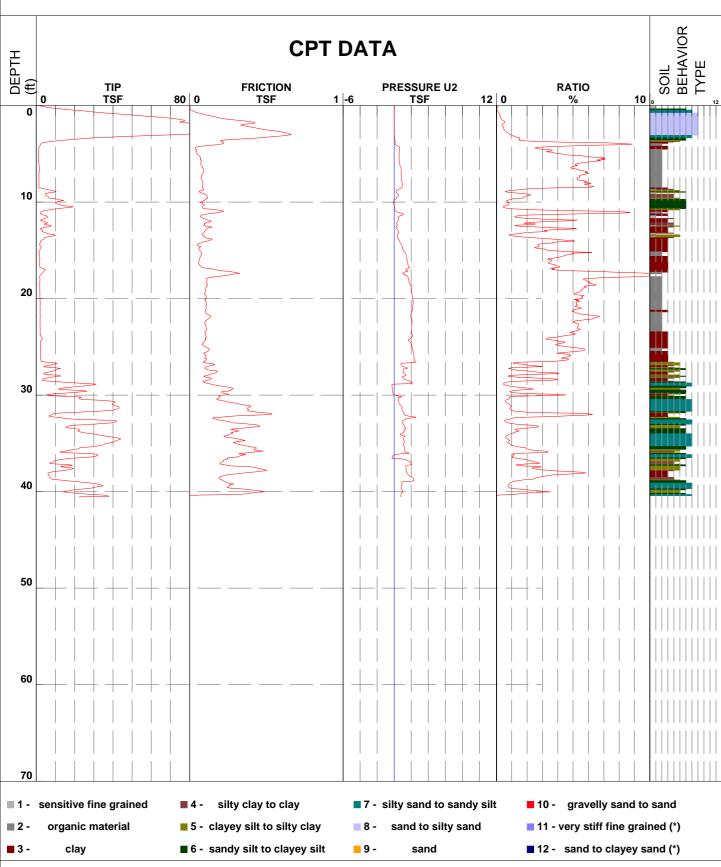
Client Fugro Consultants, Inc.

Operator

Date and Tin <u>13-Sep-2011 15:22:16</u>

Elevation

Coordinate:N 29 38 56.3 W 90 01 44.4



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA

JUGRO

Job Number 04.5508-4005

CPT Number CPT-06

Cone Number A15F2.5CKE2H2403

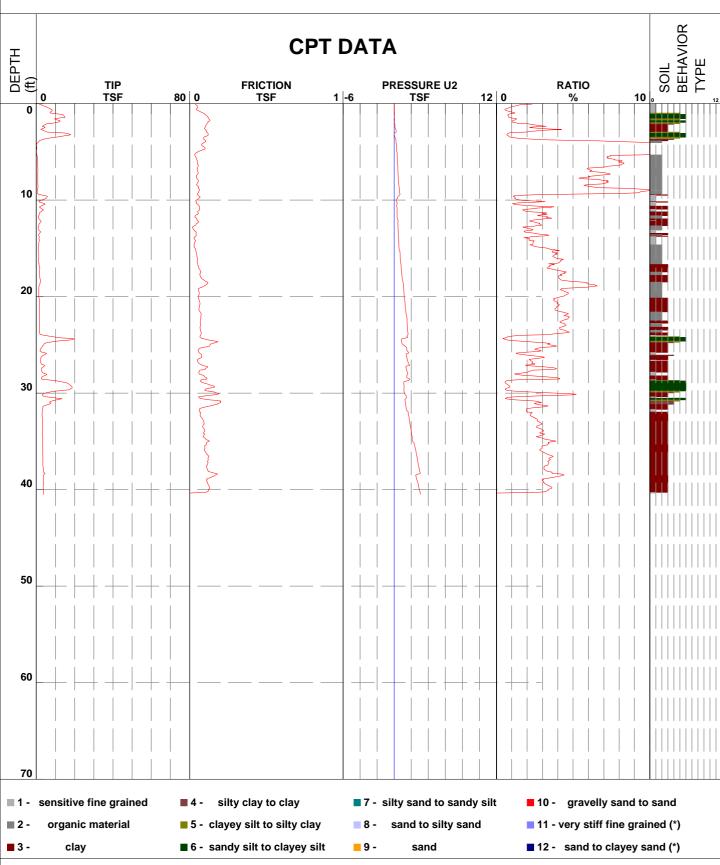
Client Fugro Consultants, Inc.

Operator

Herbert Jackson Date and Tin <u>13-Sep-2011 12:47:17</u>

Elevation 0.7'

Coordinate:N 29 38 40.5 W 90 02 18.2



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA

TUGRO

Job Number 04.5508-4005

David Cline

CPT Number CPT-7

-0.80'

Cone Number A15F2.5CKE2H2403

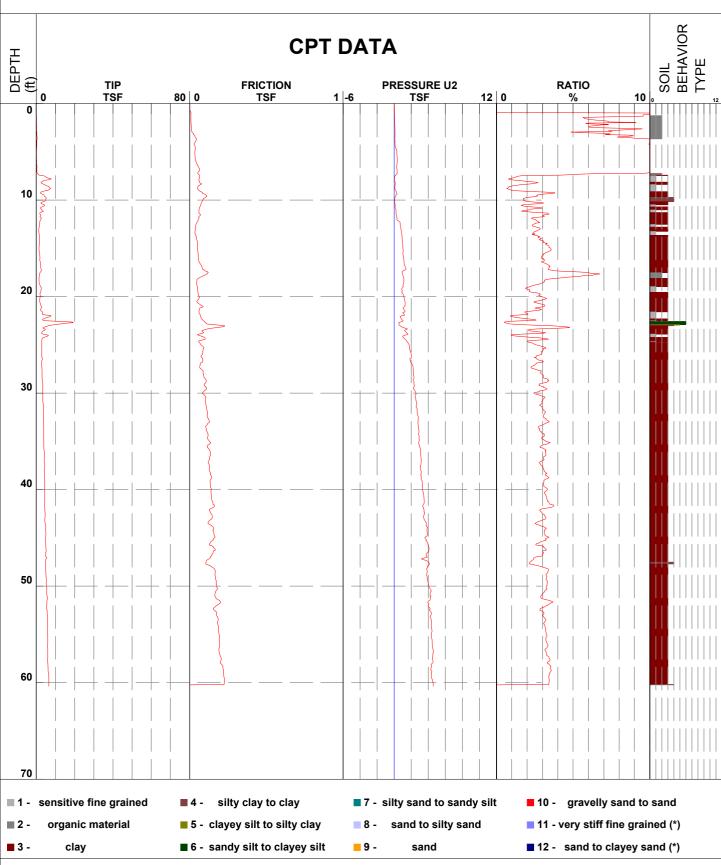
Client Fugro Consultants, Inc.

Operator

Date and Tin <u>17-Aug-2011 14:16:21</u>

Elevation

Coordinate:N 29 38 27.9 W 90 02 38.7



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA

Job Number 04.5508-4005

CPT Number CPT-08

Cone Number A15F2.5CKE2H2403

Client Fugro Consultants, Inc.

Operator

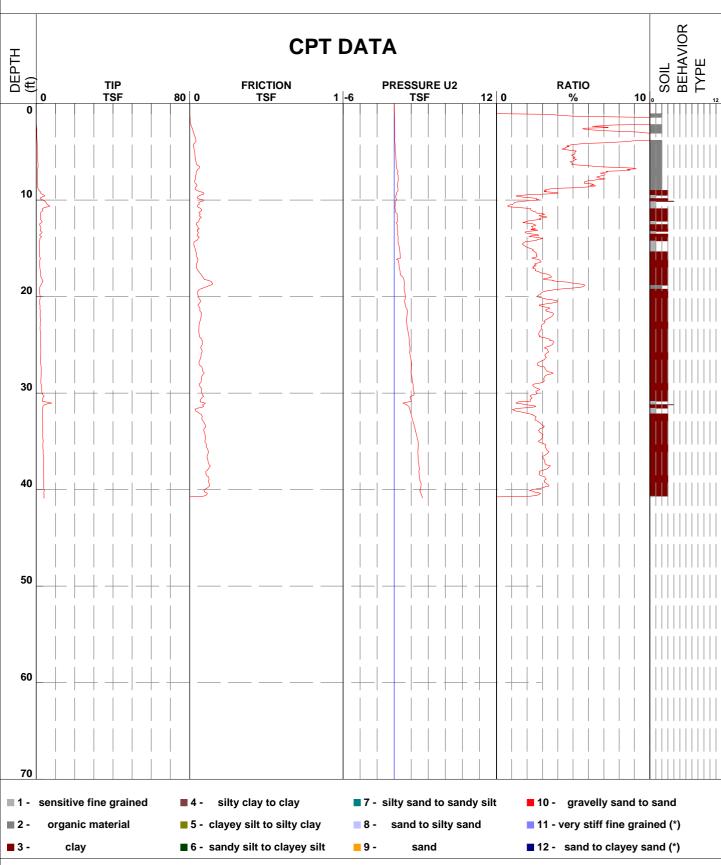
Herbert Jackson Date and Tir

Date and Tin 13-Sep-2011 10:55:19

-2.2'

Elevation

Coordinate:N 29 38 17.6 W 90 02 48.4



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA



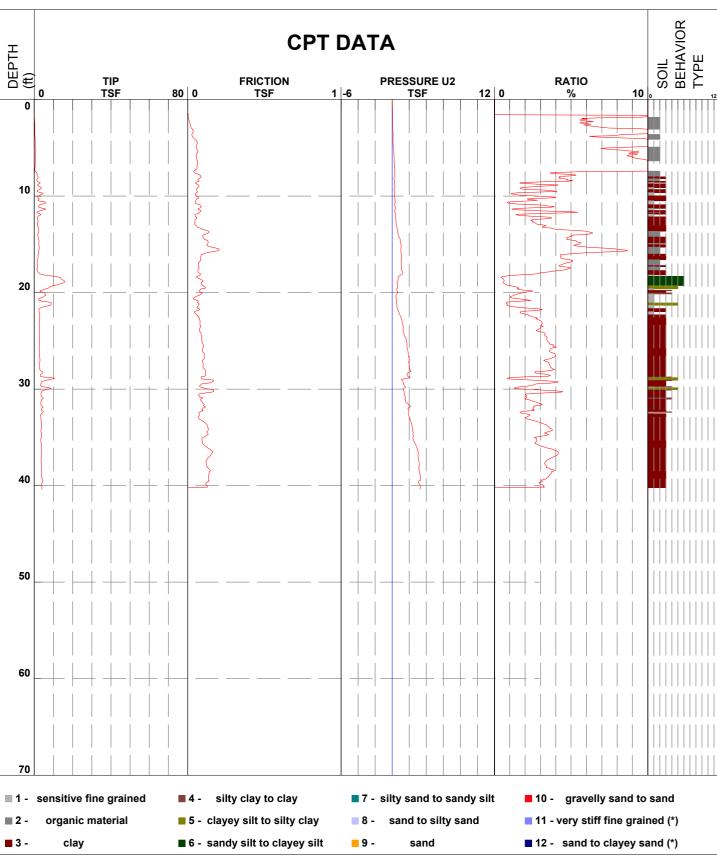
Job Number 04.5508-4005 Operator David Cline CPT Number CPT-10

Cone Number A15F2.5CKE2H2403

Client Fugro Consultants, Inc.

Date and Tin <u>17-Aug-2011 11:54:25</u> Elevation -1.7'

Coordinate:N 29 37 26.1 W 90 03 03.5



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA



Job Number 04.5508-4005

CPT Number CPT-14

Cone Number A15F2.5CKE2H2403

Client Fugro Consultants, Inc.

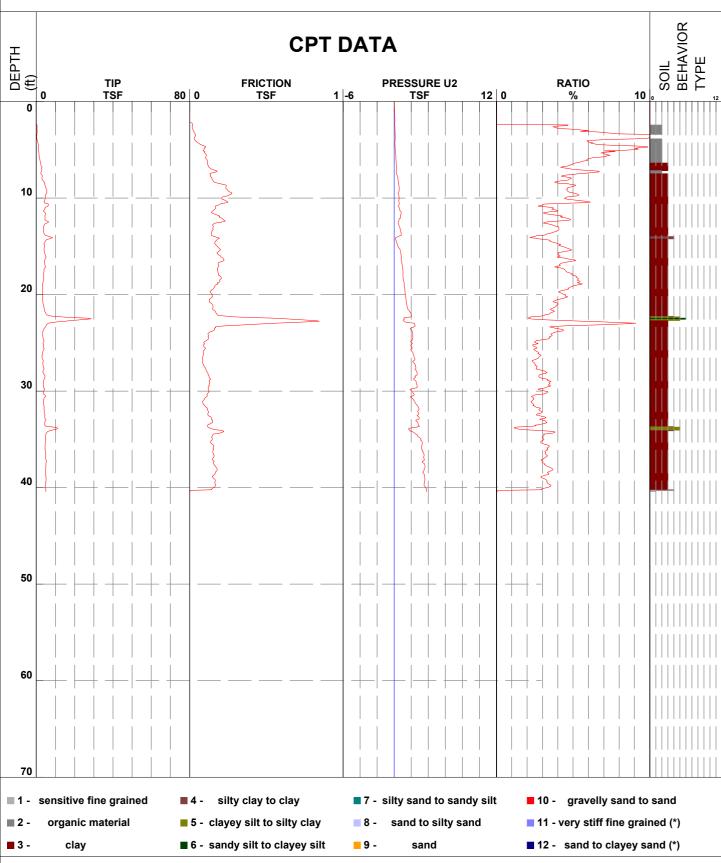
Operator David Cline

Date and Tin 17-Aug-2011 08:02:21

-1.5'

Elevation

Coordinate:N 29 36 19.3 W 90 03 17.1



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA

JUGRO

Job Number 04.5508-4005

CPT Number CPT-16

Cone Number A15F2.5CKE2H2053

Client Fugro Consultants, Inc.

Operator

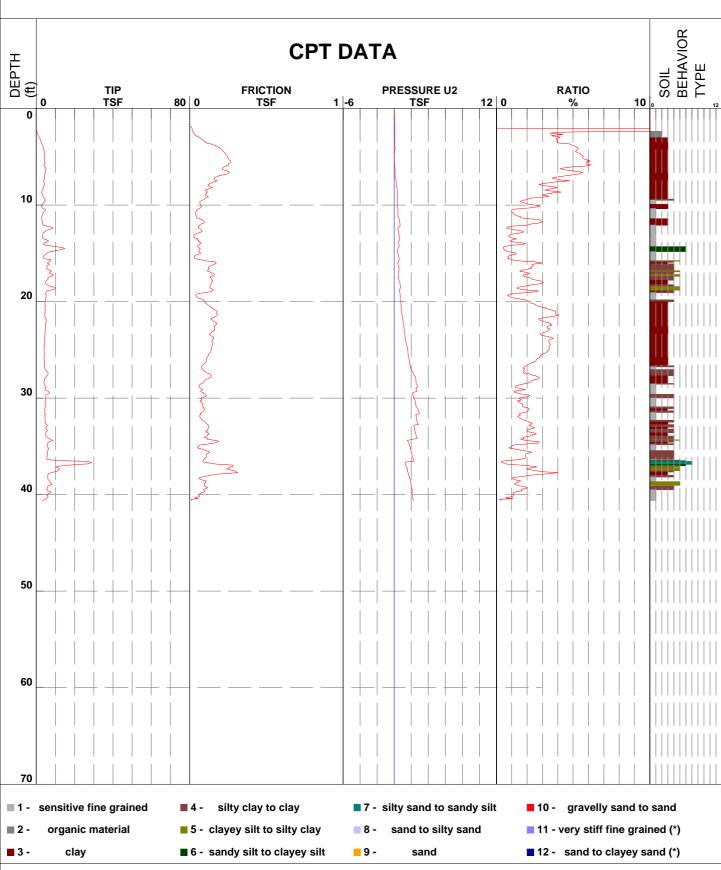
Herbert Jackson

Date and Tin 12-Sep-2011 09:56:21

-2.0'

Elevation

Coordinate: N 29 36 14.2 W 90 03 56.8



Robertson et al. 1986 * Overconsolidated or Cemented

Location **Baton Rouge-LA**



Job Number 04.5508-4005

David Cline

CPT Number CPT-17

Cone Number A15F2.5CKE2H2403

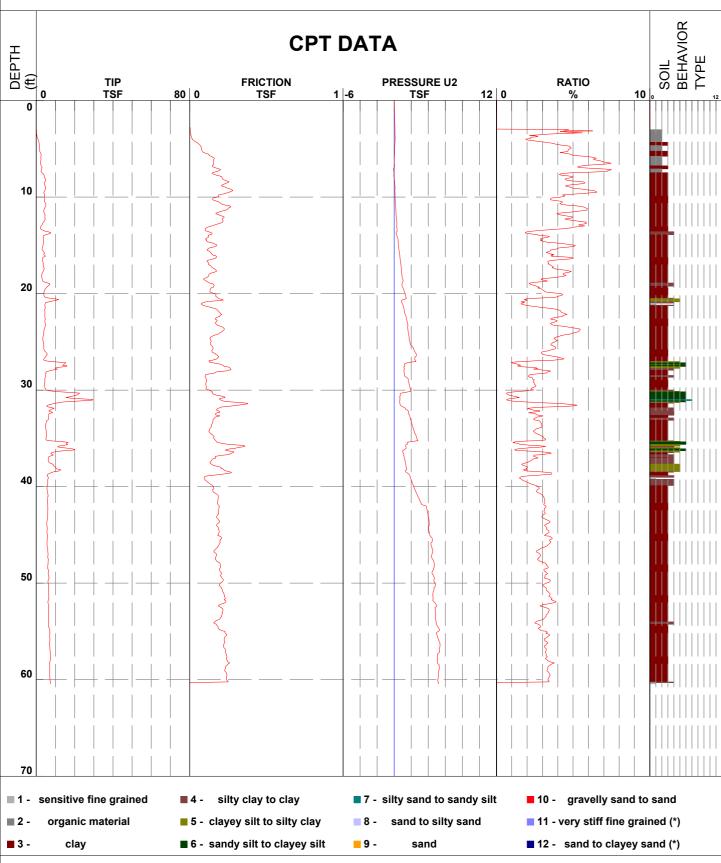
Client Fugro Consultants, Inc.

Operator

Date and Tin 19-Aug-2011 08:42:08 Elevation

-2.30'

Coordinate:N 29 36 10.4 W 90 04 16.3



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA



Job Number 04.5508-4005

CPT Number CPT-26

Cone Number A15F2.5CKE2H2403

Client Fugr

Operator

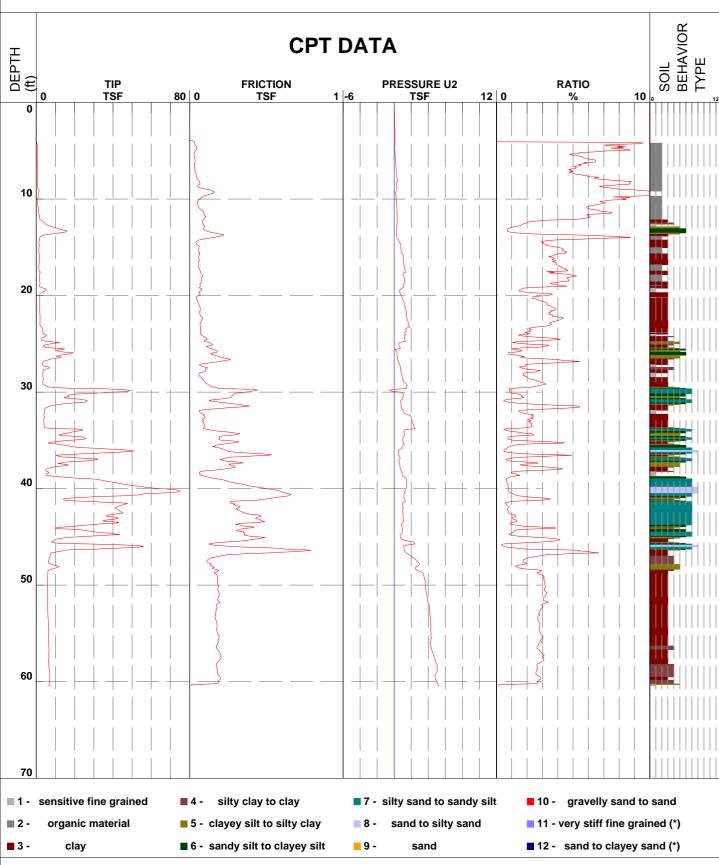
Herbert Jackson_____ Fugro Consultants, Inc.

Date and Tin 13-Sep-2011 08:02:27

-3.5'

Elevation

Coordinate:N 29 37 06.9 W 90 01 46.7



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA

TUGRO

Job Number 04.5508-4005

CPT Number CPT-27

Cone Number A15F2.5CKE2H2403

Client Fugro Consultants, Inc.

Operator

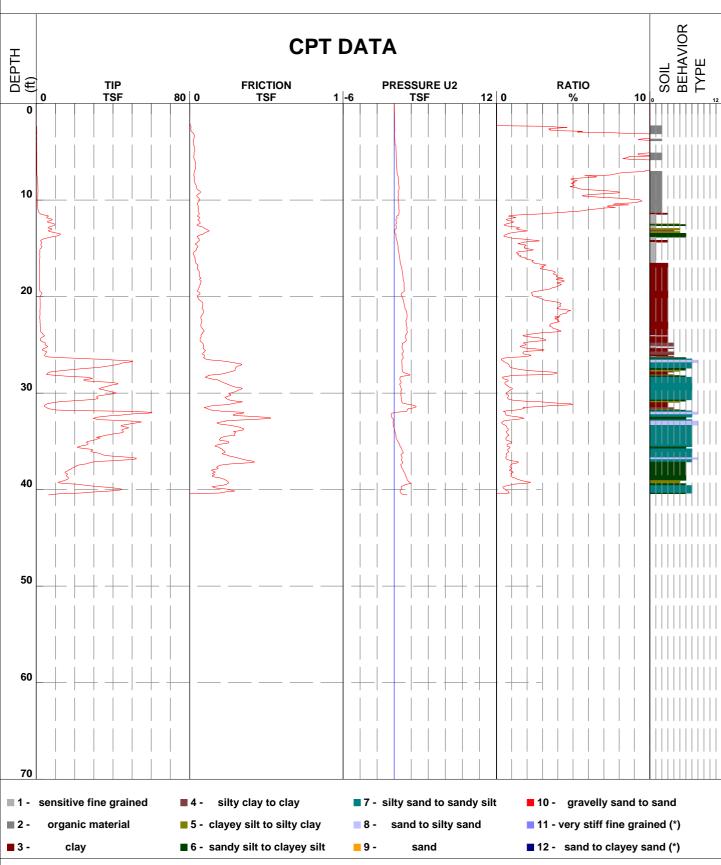
Herbert Jackson Date and

Date and Tin 12-Sep-2011 15:03:18

-1.7'

Elevation

Coordinate:N 29 37 05.4 W 90 02 14.5



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA



Job Number 04.5508-4005

David Cline

CPT Number CPT-28

Cone Number A15F2.5CKE2H2403

Client Fugro Consultants, Inc.

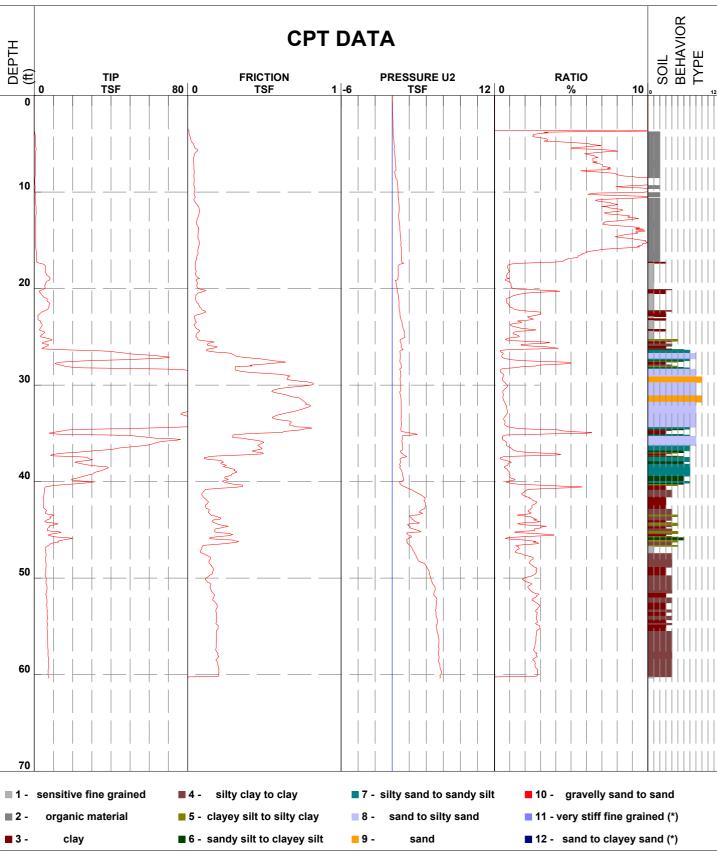
Operator

Date and Tin 17-Aug-2011 10:27:31

2.9'

Elevation

Coordinate:N 29 37 04.9 W 90 02 32.1



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA

JUGRO

Job Number 04.5508-4005

Herbert Jackson

CPT Number CPT-29

Cone Number A15F2.5CKE2H2403

Client Fugro Consultants, Inc.

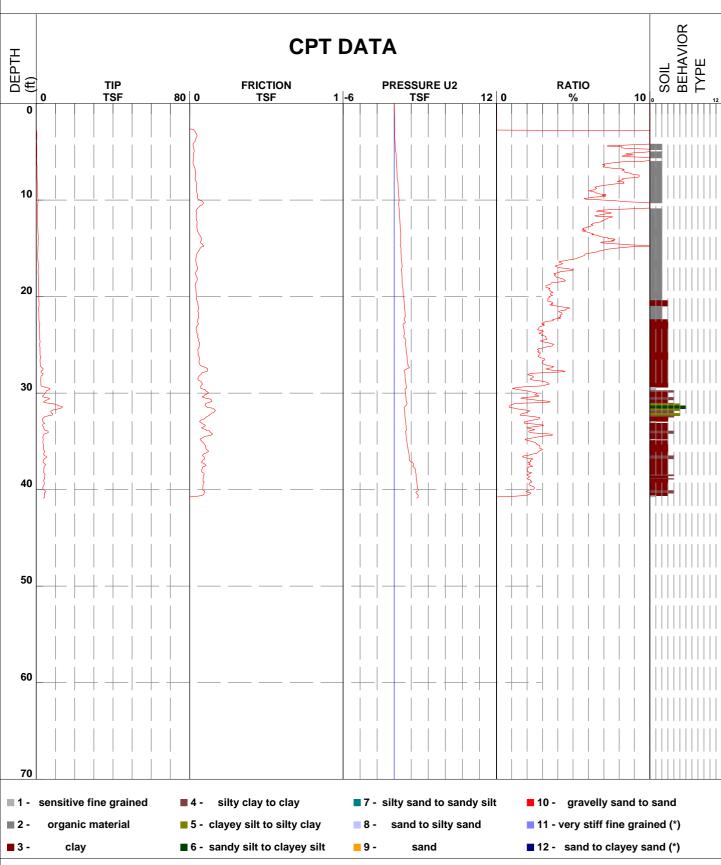
Operator

Date and Tin 12-Sep-2011 13:02:30

-1.8'

Elevation

Coordinate N 29 36 50.3 W 90 02 49.0



Robertson et al. 1986 * Overconsolidated or Cemented





Job Number 04.5508-4005

CPT Number CPT-30

Cone Number A15F2.5CKE2H2403

Client

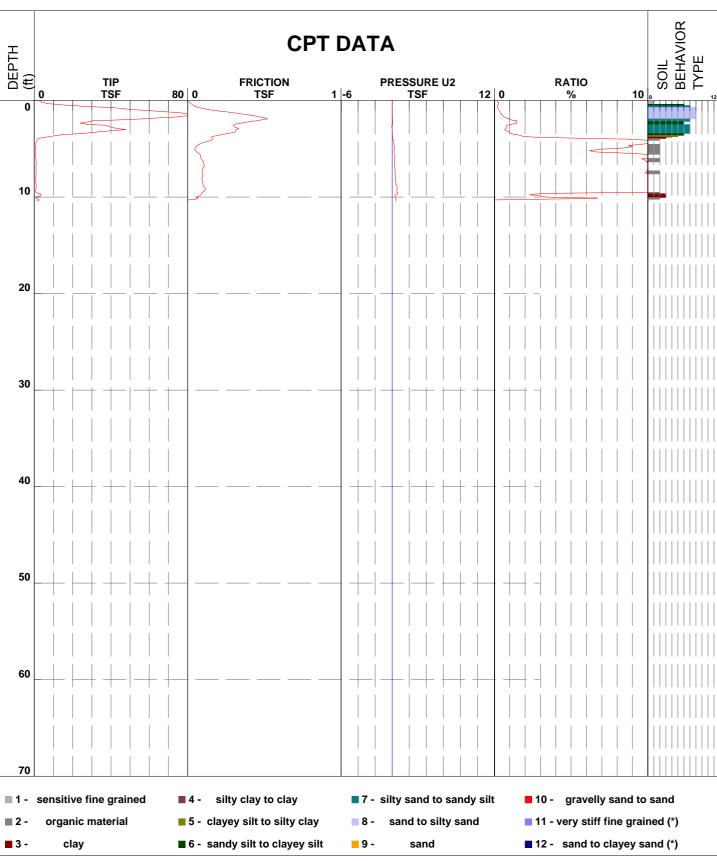
Operator David Cline

Date and Tin 18-Aug-2011 11:47:12

Fugro Consultants, Inc. Elevation

1.40'

Coordinate:N 29 39 25.1 W 90 00 42.3



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA

TUGRO

Job Number 04.5508-4005

Herbert Jackson

CPT Number CPT-32

Cone Number A15F2.5CKE2H2403

Client Fugro Consultants, Inc.

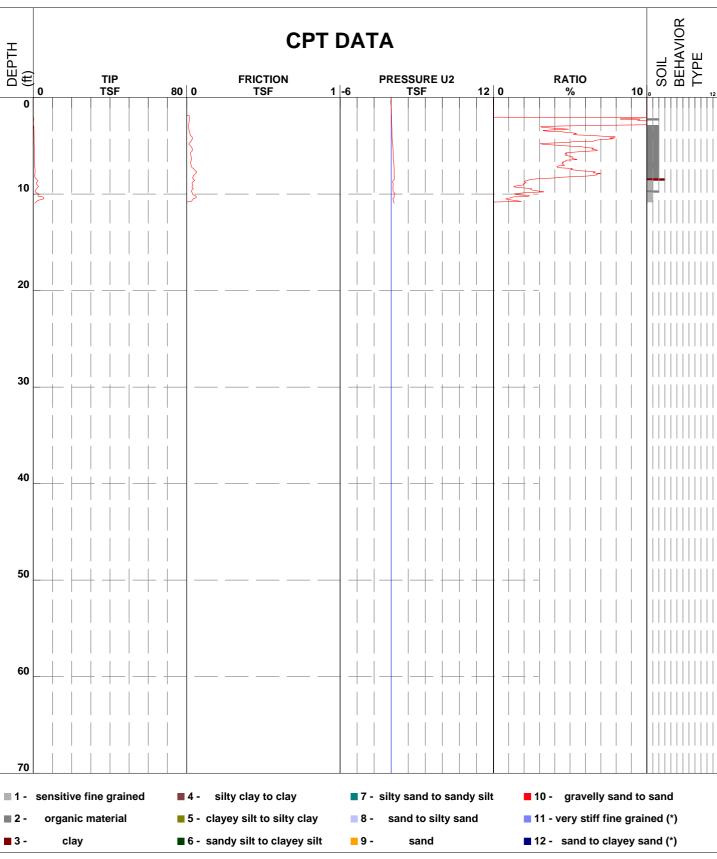
Operator

Date and Tin 14-Sep-2011 10:00:13

0.6'

Elevation

CoordinatesN29 39 15.4 W 90 00 49.2







Job Number 04.5508-4005

CPT Number CPT-34

Cone Number A15F2.5CKE2H2403

Client Fugro Consultants, Inc.

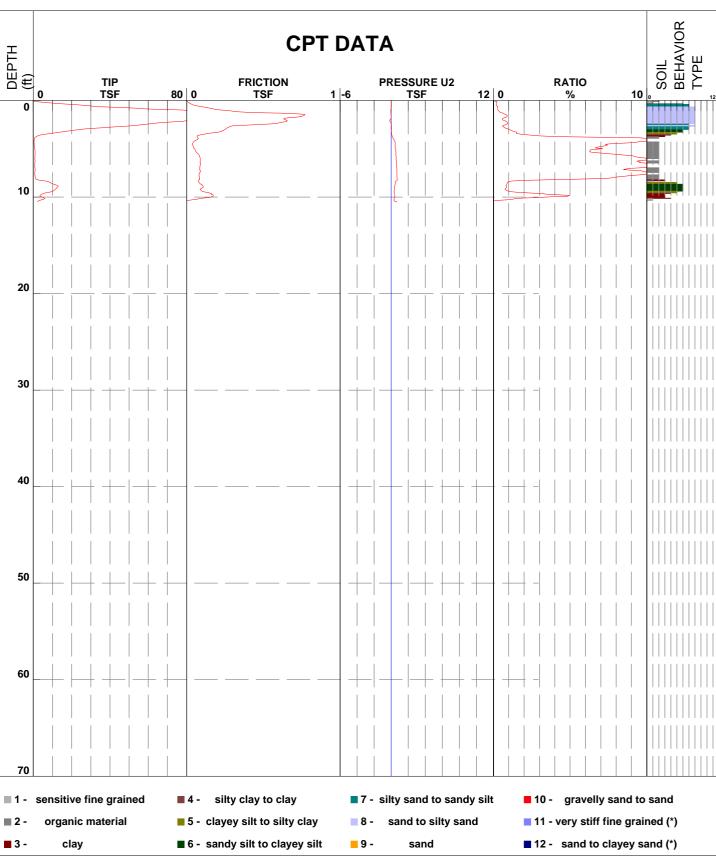
Operator David Cline

Date and Tin 25-Aug-2011 10:14:22

1.4'

Elevation

CoordinatesN 29 39 081 W 90 01 06.7



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA



Job Number 04.5508-4005

David Cline

CPT Number CPT-35A

Cone Number A15F2.5CKE2H2403

Client Fugro Consultants, Inc.

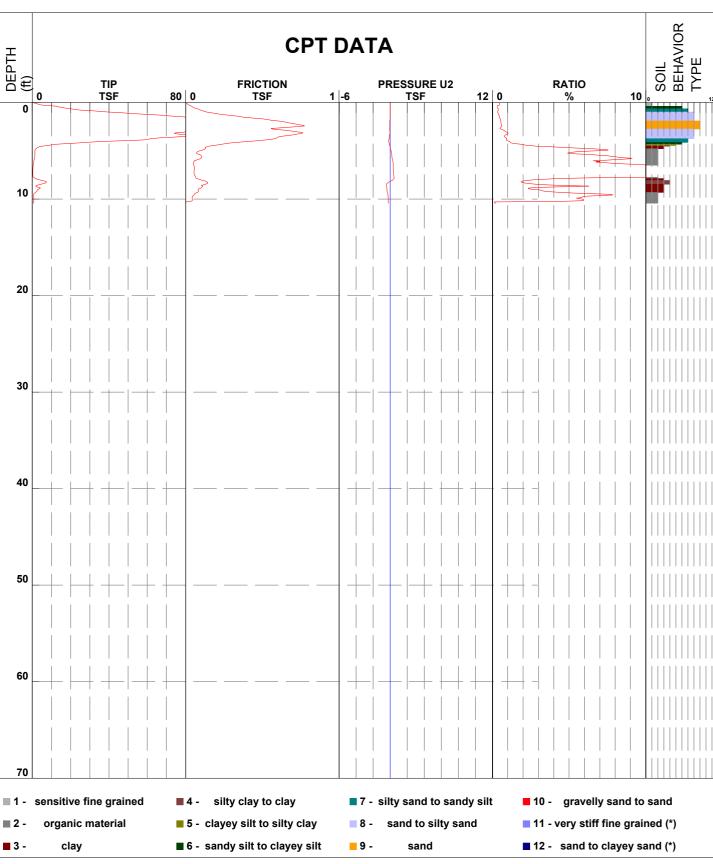
Operator

Date and Tin 25-Aug-2011 11:31:38

1.4'

Elevation

Coordinate:N 29 38 53.1 W 90 00 48.0



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA



Job Number 04.5508-4005

David Cline

CPT Number CPT-36

1.3'

Cone Number A15F2.5CKE2H2403

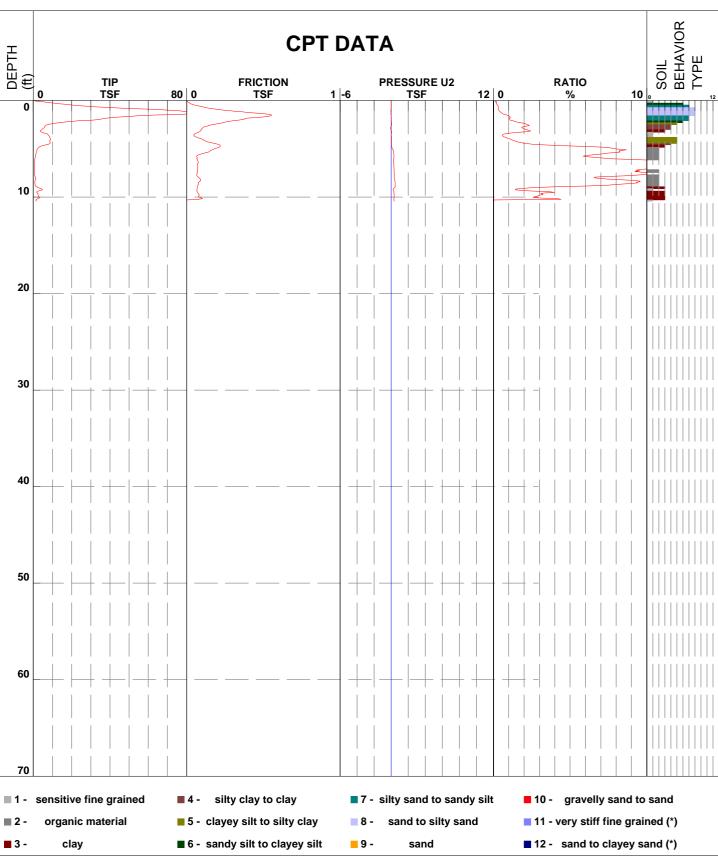
Client Fugro Consultants, Inc.

Operator

Date and Tin 25-Aug-2011 08:51:51

Elevation

Coordinate:N 29 39 05.0 W 90 01 22.5



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA

TUGRO

Job Number 04.5508-4005

David Cline

CPT Number CPT-37

Cone Number A15F2.5CKE2H2403

Client Fugro Consultants, Inc.

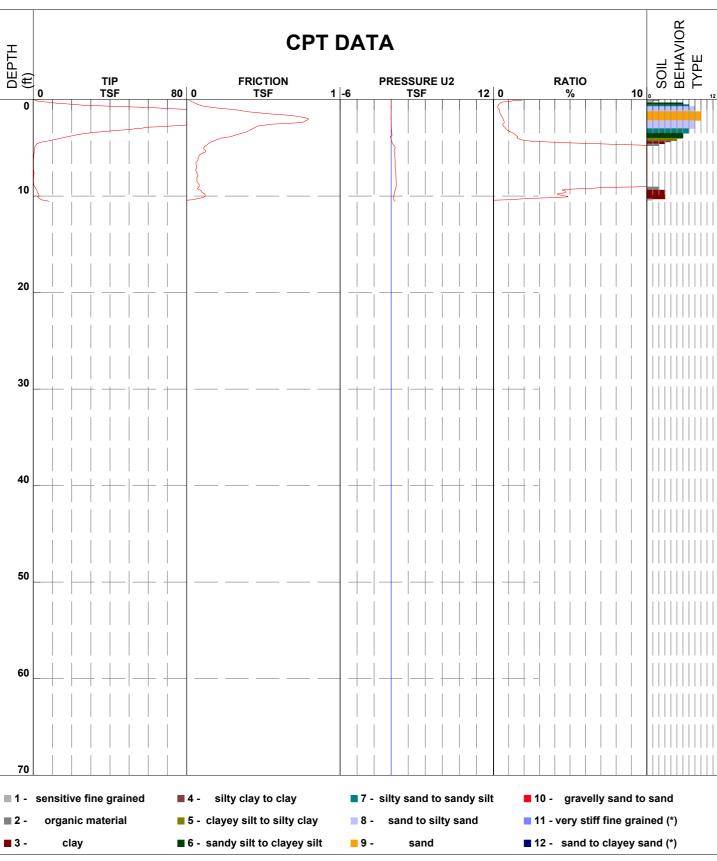
Operator

Date and Tin 25-Aug-2011 12:24:30

1.0'

Elevation

CoordinatesN 29 38 516 W 90 01 10.8



Robertson et al. 1986 * Overconsolidated or Cemented

Location Baton Rouge-LA



Job Number 04.5508-4005

Herbert Jackson

CPT Number CPT-39

Cone Number A15F2.5CKE2H2403

Client Fugro Consultants, Inc.

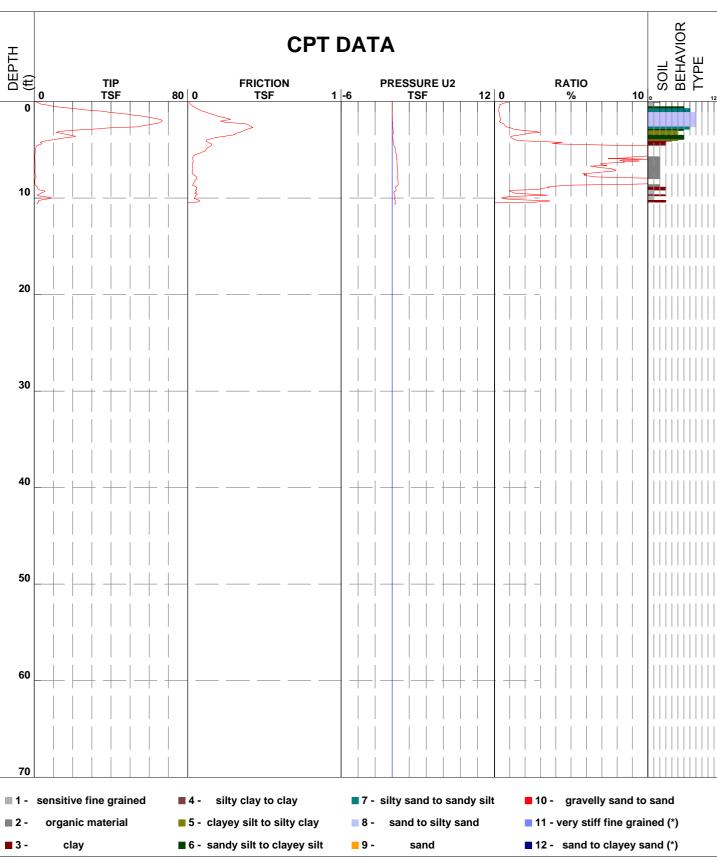
Operator

Date and Tin 13-Sep-2011 14:28:20

0.6'

Elevation

Coordinate:N 29 38 50.0 W 90 01 55.2



Robertson et al. 1986 * Overconsolidated or Cemented



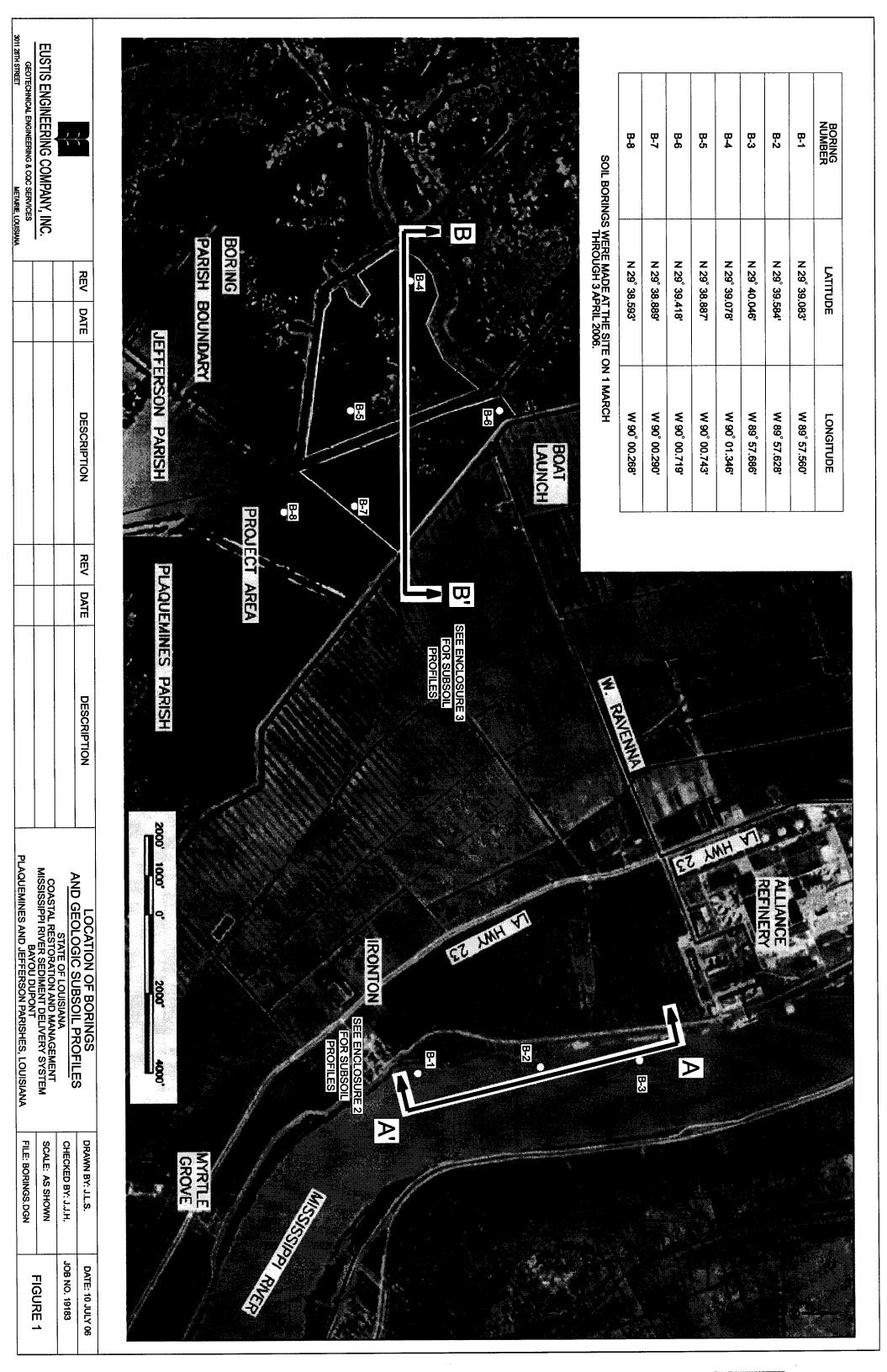
APPENDIX D

SUBSURFACE INFORMATION OBTAINED BY OTHERS



APPENDIX I

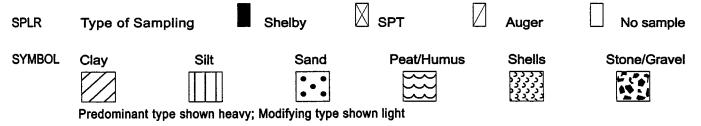
LOGS OF SOIL BORINGS AND LABORATORY TEST RESULTS





PP Pocket penetrometer: Resistance in tons per square foot

SPT Standard Penetration Test: Number of blows of a 140-lb hammer dropped 30 inches required to drive 2-in. O.D., 1.4-in. I.D. sampler a distance of 1 foot into the soil after first seating it 6 inches



USC Unified Soil Classification

DENSITY Unit weight in pounds per cubic foot

SHEAR TESTS

TYPE

- UC Unconfined compression shear
- OB Unconsolidated undrained triaxial compression shear on one specimen confined at the approximate overburden pressure
- UU Unconsolidated undrained triaxial compression shear
- CU Consolidated undrained triaxial compression shear
- DS Direct shear
- Ø Angle of internal friction in degrees
- c Cohesion in pounds per square foot

ATTERBERG LIMITS

- LL Liquid Limit
- PL Plastic Limit
- Pl Plasticity Index

OTHER TESTS

- CON Consolidation
- PD Particle size distribution (sieve and/or hydrometer)
- k Coefficient of permeability in centimeters per second
- SP Swelling pressure in pounds per square foot

Other laboratory test results reported on separate figures

GENERAL NOTES

- (1) If a ground water depth is shown on the boring log, these observations were made at the time of drilling and were measured below the existing ground surface. These observations are shown on the boring logs. However, ground water levels may vary due to seasonal fluctuations and other factors. If important to construction, the depth to ground water should be determined by those persons responsible for construction immediately prior to beginning work.
- (2) While the individual logs of borings are considered to be representative of subsurface conditions at their respective locations on the dates shown, it is not warranted that they are representative of subsurface conditions at other locations and times.

Ground Elev.: Scale PP In PP		m ⊢	Datum:	Datum: NAVD 88 Gr. V Symbol Visual Cla Loose gray clayey silt	/ater D Issificatio	STATE OF LOUI: COASTAL RESTORATION AN MISSISSIPPI RIVER SEDIMENT BAYOU DUPONT, LO BAYOU DUPONT, LO	ML R	STATE C RESTORA YOU DUF YOU DUF Job No.: Sample Number	STATE OF LOUISIANA L RESTORATION AND MANAGEMENT PI RIVER SEDIMENT DELIVERY SYSTEM BAYOU DUPONT, LOUISIANA Job No.: 19183 Date Drilled: 3/01/ Job No.: 19183 Date Drilled: 3/01/ C Number In Feet Percent Dry Wet	STATE OF LOUISIANA ESTORATION AND MAI ESTORATION AND MAI IVER SEDIMENT DELIV OU DUPONT, LOUISIA OU DUPONT, LOUISIA I 19183 Date Sample Depth Content Number In Feet Percent	VERY S VERY S ANA Be Drille	SIANA VD MANAGEMENT DELIVERY SYSTEM DUISIANA Date Drilled: 3/01/06 Water Density 5 Dontent Dry Wet Type	06 Typ	Shear Tests	Bori	` [#]	S S Cimits	(Sheet 1 of 1) Refer to "L PI	egends & Ott Tee	Notes"
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Comments: Estimated water surface at el 2.7. N 29° 39.083'; W 89° 57.560'

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Comments: Estimated water surface at el 2.7. N 29° 39.584'; W 89° 57.628'

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Comments: Estimated water surface at el 2.7. N 29° 40.046', W 89° 57.686'

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	0.00			Very soft gray clay w/sandy silt lenses & pockets	ਤ	5	9-10	76	55	98	OB	0 58					
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Comments: Estimated water surface at el 0.2. N 29° 39.078'; 90° 01.346'

EUSTIS ENGINEERING COMPANY, INC.

LOG OF BORING AND TEST RESULTS

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101	0.00					5	9-10										
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t t				Soft gray clay w/sand lenses	.												
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50	0.75					16	49-50										
	I	•															

Comments: Estimated water surface at el 0.2. N 29° 38.887'; W 90° 00.743'

EUSTIS ENGINEERING COMPANY, INC.

LOG OF BORING AND TEST RESULTS

		Refer to "Legends & Notes"	Other	Tests							<u> </u>							
2)	ī	o "Legends						,		<u> </u>								
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RESI	SYS1	Date Drilled: 3/30/06	Density	y Wet														
EST F	MANAG LIVER SIANA	ate Dri		ent Dry														
		33 D	Water		2		<u> </u>					<u></u>						
NA C		.: 1918	Depth	In Feet		00-+0	59-60										***==	
RINC		Job No.: 19183	Samole	Number	į	2	18										-	
F BO	STAL R SIPPI F BA	ì		DSU DSU	ъ	сн												
LOG OF BORING AND TEST RESULTS	COASTAL RESTORATION AND MANAGEMENT MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM BAYOU DUPONT, LOUISIANA	Gr. Water Depth: N/A		Visual Classification		Ą												
Υ, INC				Visual C	lay	ff gray cla												
EUSTIS ENGINEERING COMPANY, INC.		Datum: NAVD 88			Soft gray clay	Medium stiff gray clay												
NG CO		tum: N		L Symbol R														
EERII				SPT L											<u> </u>			
NIÐN		Ground Elev.: -1.8					75		<u> </u>									
STIS E		ind Ele	e	а Б Б Б Б Б Б Б	}	- 0.50	0.75	1 1				1			- <u> </u>	11	-11	
EUS		Grou	Scal	Feet In	50		60 -			- 02			08		- 06			100

Comments: Estimated water surface at el 0.2. N 29° 38.887'; W 90° 00.743'

a trans

GINEERING COMPANY, IN -0.3 Datum: NAVD 88 C -0.3 Datum: NAVD 88 C Nery soft gray very soft gray very soft gray	VC. LOG OF BORING AND TEST RESULTS STATE OF LOUISIANA COASTAL RESTORATION AND MANAGEMENT MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM	ם	Sample Depth Water Density Shear Tests Atterberg Limits	sual Classification USC Number In Feet Content Dry Wet Type ø C LL PL PI Tests	brown humus Pt 1 1-2	Clay w/sitt pockets CH 2 3-4 63 61 100 UC - 145 88 27 61 CON	3 5-6	4 7-8 63 62 100 UC - 215 81 23 58	ML 5 9-10	7 13-11 00 00	° CH	9 17-18	10 19-20	Jy silt pockets 11 24-25 11		13 34-35	14 39-40		
EUSTIS ENG Ground Elev.: Scale In Feet 10- 0.50 0.50 0.50 0.50 0.50 0.75	EUSTIS ENGINEERING COMPANY, INC. LOG OF BORING AND TEST RES STATE OF LOUISIANA COASTAL RESTORATION AND MANAGEME MISSISSIPPI RIVER SEDIMENT DELIVERY SYS	-0.3 Datum: NAVD 88 Gr. Water Depth: N/A Job No.: 19183 Date Drilled:	S Sample Depth	SPI L Symbol Visual Classification USC Number In Feet Content		2 3.4 63		7-8 63	Medium compact gray clayey silt w/clay ML 6 41.1.2 20	enses 0 11-12 30	Very soft gray clay w/silt lenses & layers CH 8 15-16 57 8 15-16								

$\rightarrow \rightarrow \rightarrow$	& Notes"	Other	Tests															NCC				 	12
of 1)	Refer to "Legends & Notes"																						
(Sheet 1 of 1)	Refer	its	Ы				ъ			55								ŝ	2				
(Sh		Atterberg Limits	Ч				31			25								ş	1				
	2 :1	Attert	L				36			80								2	ţ				
	Boring: 7	sts	v	64			616			100			95					ġ				 	
		Shear Tests	e Ø	0			•			0			1						1				
(0		ي م	Type	OB			8			B			о Л					-	ງ 			 	
	03/06	Density	Wet	64			120			97			66					ç	0				
	d: 4/	Ď	Dry	8			63			54			21	_				Ĺ	8			 	
ORING AND TEST RESULTS STATE OF LOUISIANA RESTORATION AND MANAGEMENT I RIVER SEDIMENT DELIVERY SYSTEM AYOU DUPONT. LOUISIANA	Job No.: 19183 Date Drilled: 4/03/06	Water	Percent	002			29			79			74					ç	80				
LOUISIA LOUISIA ON AND I MENT DE	19183 D	Depth	In Feet	1-2	3-4	5-6	7-8	9-10	11-12	13-14	15-16	17-18	19-20		24-25		29-30		00-40	39-40			
30RING AND TEST I STATE OF LOUISIANA AL RESTORATION AND MANAC PI RIVER SEDIMENT DELIVER BAYOU DUPONT. LOUISIANA	Job No.:	Sample	Number	-	7	e	4	5	9	7	8	6	10		11		12	ç	5	14			1
		0	ראכ חאכ	đ		ML				Ъ									ਲ				
EUSTIS ENGINEERING COMPANY, INC. LOG OF BC COASTAL MISSISSIPPI B	NAVD 88 Gr. Water Depth: N/A		Visual Classification	Very soft black humus		Medium compact gray clayey silt				Very soft gray clay w/sand lenses & pockets		w/sand pockets					w/sand lenses & pockets		Medium stiff gray clay				
CO	n: N⊿		symbol																				
IEERING	7 Datum:	sσ	- Las					- · · · S														 	
ENGIN	Elev.: -2.7		ት 	0.00	0.00	1.50	0.75	0.50	0.00	0.00	0.50	0.00	0.50	1	0.25	T T	0.50		0.75	1.00		 	
EUSTIS	Ground Elev.:	Scale	Feet	0	1			 9	2	I	I	1	20 –				30 –		1	' Ş	?	 '	20

Comments: Estimated water surface at el 0.2. N 29° 38.889'; W 90° 00.290'

	Notes"	Other	Tests				CON												
	Refer to "Legends & Notes"												 						_
1 of 1	fer to "I																		_
(Sheet 1 of 1)	Re	_imits	Ы				157												
		Atterberg Limits	Ы				67												
	Boring: 8	At	LL				224					<u></u>	 						
	Bori	Tests	ø C	- 13			0 57		0 221			- 155		- 130					
		Shear Tests	Type	Ŋ			OB		BO			nc		n					
ST. 2	90	ity	Wet	65			76		115			93		100					\neg
SUL IENT YSTEN	: 3/31	Density	Dry	10			25		83			52		64					
ORING AND TEST RESULTS STATE OF LOUISIANA RESTORATION AND MANAGEMENT RIVER SEDIMENT DELIVERY SYSTEM AYOU DUPONT, LOUISIANA	Job No.: 19183 Date Drilled: 3/31/06	Water	Percent	528			208		38			81		57					
ND TE LOUISIAN DN AND M AENT DEI VT, LOUIS	19183 Da	Depth	In Feet	1-2	34	5-6	7-8	9-10 11-12	13-14	15-16	17-18	19-20	 24-25	29-30	34-35	39-40 39-40	2		
SORING AND TEST I STATE OF LOUISIANA L RESTORATION AND MANAG PI RIVER SEDIMENT DELIVER BAYOU DUPONT, LOUISIANA	Job No.:	Sample	Number	1	5	ო	4	<u>م</u> م	7	8	o	10	11	12	13	14	:		
		US I	200	ъ		đ	Ĺ	ML		сн									
Y, INC. LOG	88 Gr. Water Depth: N/A	Vieual Classification		Very soft black humus		and dark was build in a dark	very solituain gray riuritus wroous ariu day layers	Very loose gray clayey silt		Very soft gray clay	w/sand lenses & pockets								
/dWC	NAVD		5	<u>به</u>	3333	333		<pre> </pre>		Ver Ver								 	
Ŭ P	Datum: NAVD 88	P S	L ayrinuu R															 	
EERIN		LO S											 						
S ENGIN	Elev.: -1.8	ç	<u>L</u> L	0.00	0.00	0.00	0.00	0.50	0.00	0.00	0.00	0.00	 0.00	0.25	0.50		1 - 1- 5	 	
EUSTIS	Ground Elev.:	Scale	Feet	0	I		'	6 1		. 1		20	. •	30			40 1		50

Comments: Estimated water surface at el 0.2. N 29° 38.593'; W 90° 00.268'

EUSTIS ENC Ground Elev.: Scale PP Feet PP	ИGINEEF :: -18.3 П spт	RING C Datum:	EUSTIS ENGINEERING COMPANY, INC. LOG OF BORING AND STATE OF LOUI: COASTAL RESTORATION AN MISSISSIPPI RIVER SEDIMENT BAYOU DUPONT, LC BAYOU DUP	F B(STAL B, B, B,	JKING STATE O STATE O STATE O STATE O STATE O VOU DUF Job No.:	CCKING AND IES I KESUL STATE OF LOUISIANA L RESTORATION AND MANAGEMENT PI RIVER SEDIMENT DELIVERY SYSTEM BAYOU DUPONT, LOUISIANA Job No.: 19183 Date Drilled: 3/01/ Job No.: 19183 Date Drilled: 3/01/ C Number In Feet Depth Content Dry Wet			TEST RESOLUS SIANA ND MANAGEMENT DELIVERY SYSTEM DUISIANA Date Drilled: 3/01/06 Water Density strems Content Dry Wet Type	2 <u>8</u>	Shear Tests	Bori	(S ng: 1 Atterberg Limits LL PL PI	(S)	(Sheet 1 of 1) Refer to "L PI	et 1 of 1)
)		Loose gray sandy silt Very soft gray clay	GH MI	۱ co 4 co Co 1	5-6 5-6 6-7 7-8 11-12	25 56	98 67	122 104	8 N		4	65 23	42		
20			Loose to medutin dense gray sirty sand w/clay layers Very soft gray clay w/silty sand lenses & layers Loose brown & gray sandy silt w/clay		- 86 - <u>1</u> 2 - 88 -	15-16 16-17 16-20 20-21 23-24	47	44	109	BO	0	75	72 24	48		6 6
- 0.25 30 - 0.25 30 - 0.25			Very soft to soft brown & gray clay w/silt lenses & pockets Medium compact gray sandy silt		15 15 15 15	25-26 27-28 29-30 31-32 32-34	43	4	11	2	ł	139	70 27	£ 3		Q
40 - 0.25			Soft brown & gray clay w/silt lenses & pockets	Б	20	35-36 37-38 39-40	Ω.	ő	102	2	1	203	64 22	4		
20																

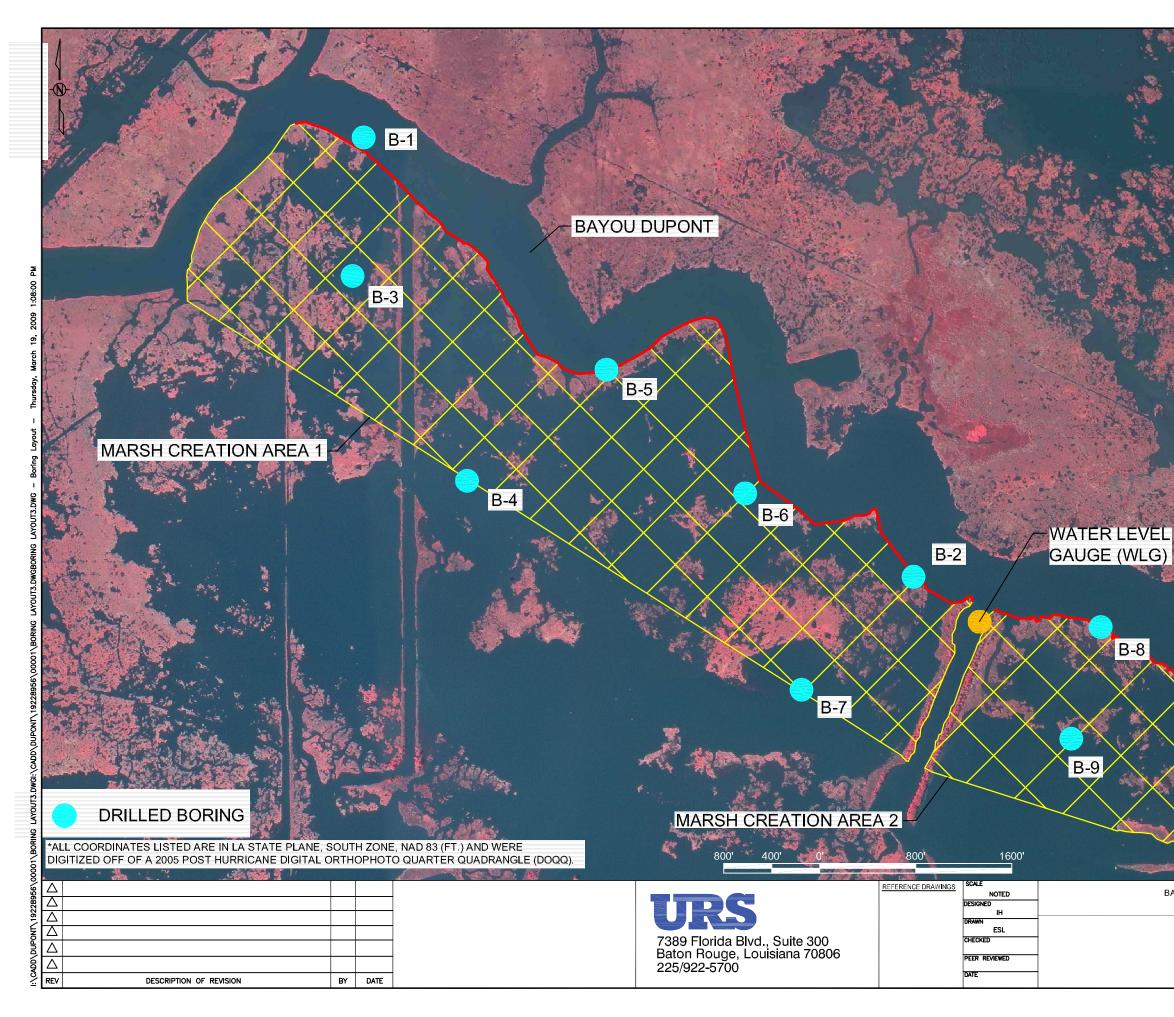
Comments: Estimated water surface at el 2.7. N 29° 39.083'; W 89° 57.560'

Constra RESTORMACEINT INSISTENT RELACTIONATIONAL INSISTENT RELACTIONAL INSISTENT RELA	EUSTIS	ENGI	VEERIN	Ú U U U	EUSTIS ENGINEERING COMPANY, INC.	LOG OF BORING	BOR	ING AI		AND TEST RESULTS	SUI	.TS				Ç		ŝ		
						COAST/ MISSISSIP	AL RES PI RIV BAVO	TALE UP L STORATIC ER SEDIN	-CUUSIAF NN AND N AENT DE	VA AANAGEA LIVERY S	AENT YSTE	Σ				Ŋ	neet 1	of 1)	$\left\{ +\right\} $	
PF Struct B Struct B	Ground E			tum:		ter Depth: N/A		Job No.:	19183 Di	ate Drillec		1/06		Boril			Ref	er to "Legen	ds & Not	tes"
	Scale	2		л В С			US T	Sample	Depth	Water	Den	sity	Shear	Tests	Att	erberg L	imits		Oth	her
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Feet			L oyiii		Silication	S	Number	In Feet	Percent	Dry	Wet	Type		Е	Ы	₫		Tes	sts
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$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		_						5	3-4	37	85	116	Ŋ			17	23			
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1	0.25			Very soft gray clay w/sit	It lenses & pockets	Ь	ю	5-6											
0.25 0.26 0.26 0.26 0.26 0.26 0.26 0.26 0.26 0.26 0.25 0.26 0.25 0.26 0.25 0.26 0.25 0.26 0.25 0.26 0.25 0.26 0.26 0.26 0.25 0.26 0.25 0.26 0.25 0.26 0.25 0.26 0.25 0.26 <th< td=""><td></td><td>0.25</td><td></td><td></td><td></td><td></td><td></td><td>4</td><td>7-8</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>		0.25						4	7-8											
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1 13-14 70 1 13-14 70 1 13-14 70 1 13-14 70 1 13-14 70 1 13-14 70 1 13-14 70 1 13-12 13-14 1 13-12 13-14 1 13-12 13-14 1 13-12 13-14 1 13-12 13-14 1 13-12 13-14 1 13-14 14 1 13-14 14 1 14 12 1 14 25-26 1 14 26-30 1 14 26-30 1 14 26-30 1 14 26-30 1 14 26-30 1 14 26-30 1 14 26-30 16 34-36 16	2				Loose gray clayey silt			9	11-12	56										
Loose gray sity fire sand wicky layers SM B 15-16 15-16 Very soft gray clay with pockets & lenses CH 11 21-22 43 76 109 UC - 81 Very soft gray clay with pockets & lenses CH 11 21-22 43 76 109 UC - 81 Very soft gray clay with pockets & lenses CH 11 21-22 43 76 109 UC - 81 Very soft gray sity sand wickay layers SM 12 22-24 43 76 109 UC - 81 Modum sitil gray sity clay wist 1 22-24 23 22 101 122 28-30 0.50 Modum sitil gray sity clay wist lenses CL 20 38-40 0 101 122 08 0 107				•	Loose gray sandy silt		NS	7	13-14	20										
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15 28-30 16 30-32 17 32-34 18 34-36 19 36-38 19 36-38 19 36-38 19 36-38 19 36-38 19 36-38 19 36-38 19 36-38 19 36-38 101 122 12 38-40								14	26-28										ī.	
0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50	30							15	28-30											
0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50	3							16	30-32											
0.50 0.50 0.50 0.50 19 19 19 19 19 19 19 19 19 19 19 19 19				•				17	32-34	22	101	122	OB	0 110	~					
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I	1	0.50			Medium stiff gray silty c	slay w/silt lenses	5	20	38-40											
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Comments: Estimated water surface at el 2.7. N 29° 39.584'; W 89° 57.628'

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	Refer to "Legends & Notes"	Other	ests							0							D									
	egends		-																							
(Sheet 1 of 1)	r to "L																									
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hS)		imits	Ч																							
	с	Atterberg Limits	Ъ																							
	Boring:	Atte	LL							_																
	BC	sts	υ		28			204																		
		Shear Tests	8		ł			0																		
TS.	90/9	s	Type		3			80																		
	Date Drilled: 3/05/06	ity	Wet		109			117																		
RE: GEMI	rilled:	Density	Dry		74			06																		
	ate Di	- 1																								-
	ä	Water	Percent		48			30																		
BORING AND TEST I STATE OF LOUISIANA AL RESTORATION AND MANAG PI RIVER SEDIMENT DELIVER BANCH DI POLIVER	Job No.: 19183	Depth	Feet	0-2	2-4	4-6	6-8	8-10	10-12	12-14	14-16	16-18	18-19 19-20.5		22-23	25-26	28-29	31-32	34-35	37-38	39-40	2				
	lo.: 1								-	<u>+</u>	-				~~~~	й 	5	'n	М	ۍ بې						_
STA STA RIVER	Job N	Sample	Mumb	-	2	e	4	5	9	7	80	6	2 2		12	13	14	15	16	17	÷	2				
LOG OF BORING AND TEST RESULTS STATE OF LOUISIANA COASTAL RESTORATION AND MANAGEMENT MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM BANOLI PULEDANT TO UISTANA		Uol I	255	ษ			W	Į	SM				NS													
OF COAS	N/A			7									+-													
0	Gr. Water Depth: N/A			Extremely soft to very soft gray silty clay			2	Ĩ																		
	ter De	Viend Cleanification	וורפווסוו	ft gray			e andv	, fri inc	day				sand													
<u> </u>	. Wat		Class	very so			A Grav	c Alay	and w/c				av siltv													
ZI ≻	_	View	PUSIA	soft to			to loce		/ silty s				inse ar)												
IPAN	/D 88			remely			Very loose to loose gray sandy sit	y 10000	Loose gray silty sand w/clay				Medium dense grav siltv sand													
NOC	NA/		5	EX	m	m			Lo Lo				Me					• • • • •				<u> </u>			-	
- NG	Datum: NAVD 88																									
EER		s P												يل م	<u>시</u>	<u>م</u>		K _	L K	¥	<u>مل</u> ا	لە				-
GINI	-27.3		5										80		2	13	25	24	16	18	20					
EUSTIS ENGINEERING COMPANY, INC.	Ground Elev.:	8	L. L	0.25	0.25	0.25																				
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Е	5 D	Ň	ш																							

Comments: Estimated water surface at el 2.7. N 29° 40.046', W 89° 57.686'



	COORDI	NATES*
BORING	NORTHING	EASTING
B-1	414828.530	3689295.369
B-2	411170.779	3693876.928
B-3	413674.665	3689203.468
B-4	411968.841	3690156.752
B-5	412894.741	3691318.762
B-6	411864.051	3692474.243
B-7	410229.205	3692943.938
B-8	410752.088	3695435.524
B-9	409821.951	3695191.911
WLG	410795.322	3694472.572

BAYOU DUPONT MARSH CREATION AND RIDGE RESTORATION

TEST LOCATION PLAN



2

Log of Boring B-1

Date(s)						Logged		<u>.</u>			Check	od				\equiv
Drilled	2/2	0/09 - 2/2					By Drill Bit		apatnam			By Total E	I.	Harrou			
Drilling Method	, ROI	ary Was	sh				Size/Type	Bottom	Discharge 4(5/8)	•		Drilled	(feet)	31.8			- 11
Drill Ri Type	° ma	rsh Bug	gy				Drilling Contractor	SESI				Sampl Type(s	s) T	Piston Tube	Sampl	er/ Sn	elby
Ground and Da	dwater I ate Mea	Level -0 sured -0).2' 2/2	0/2009			Hammer Data	140 LB	S Safety			Approx Surfac	e Eleva	ation	0.2'		
Locatio	on N4 1	14828.53	84 E36	89295.3	69							Boreho Backfil		ement	Grout		
		SA	MPL	ES								(tsf)					%
Elevation feet	D epth, feet	Type Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	I	MATERI	AL DE	SCRIPTION		Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
	-				-	WATER				-							
	_	T			Z	-	NE El2.03										
	_	ST-1	20			ORGAN	NICS with C	lay (OH)		_			607				
5	5	ST-2	15			Very So – (OH)	oft, Brown to)*) Black Hl	IMUS with Clay	_		0.10	305	21	0.08	618	395
	-	ST-3	15			Very So	oft, CLAY wi	ith Organi	cs (CH - OH)	-			230	24	0.06	202	150
10	- 10-	ST-4	22			Very So	oft, Gray Lea	an CLAY (CL)*	-		0.75	64	72	0.15	46	20
	-	ST-5	22			Very So trace	oft, Gray SIL e Fine Sand	T with Cla (CL-ML)*	ay, Organics and	-		0.25	54	74	0.17	43	18
15	- 15 -	ST-6	22			- Very So	oft, Gray CL	AY with S	ilt (CH)			0.25	88	55	0.12		
20	- 20- - -	ST-7	15			- Very So	oft, Gray fat	CLAY (Cł	+)*	-		0.25	87	47	0.20	85	54
25	25–	ST-8	15			- Very So (CH)	oft, Gray CL)*	AY with tr	ace Organic Pocke	ets –		0.25	79	56	0.08		

Log of Boring B-1

Sheet 2 of 2

\square	S	AMPLI					(tsf)			(.0	%
Elevation feet	Depth, feet Type Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
30	30 - T ST-	9 20			Soft, Gray fat CLAY (CH)*	-	0.50	75	61	0.26	92	60
35	- - 35- -				Bottom of hole @ 30 feet below MUDLINE * - Look at Table: Boring B - 1 for additional Laboratory Results	-						
40	- - 40 -				· · · · · · · · · · · · · · · · · · ·							
45	- - 45 -					-						
50	- - 50 -				· · · · · · · · · · · · · · · · · · ·	-						
55	- 55 -					-						
Templ	ate: 19228956_BAY	OUDUPO	NT Proj II	D: 192289	756.00001.GPJ URS						Printed:	4/7/09

Log of Boring B-2

Date(s Drilled) 2/1	9/09 - 2/1	9/09				Logged By	A. Bukkapa	itnam		Check By	^{ed} I.	Harrou	ıch		
Drilling Method	j Ro	tary Was	h				Drill Bit Size/Type	Bottom Dis	charge 4(5/8)"		Total [Drilled		31.5			
Drill Ri Type	^g Ma	rsh Bugg	ау				Drilling Contractor	SESI			Sampl Type(s	er F S) T	Piston Tube	Sampl	er/ Sh	elby
Ground and Da	dwater I ate Mea	Level 0.	2' 2/19	9/2009			Hammer Data	140 LBS Sa	afety		Appro: Surfac	ximate e Eleva	ation ().2'		
Locatio	on N4 ′	11170.77	9 E36	93876.9	82						Boreh Backfi		ement	Grout		
		SA	MPL								(tsf)			6	%	%
 Elevation feet 	− Depth, feet	Type Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	ſ	MATERI	AL DESC	RIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, 9	Plastic Index,
Ů	-				-	WATER MUDLIN	₹ NE EI1.3'			-						
	-	ST-1	20			ORGAN	NCS with CI	ay (OH)		-		915				
5	- 5	ST-2	20			Very Sc (OH)		RGANICS wi	th Clay and Peat	-	0.25	475	12	0.12	400	254
	-	ST-3	20			Very Sc and S	oft, Gray and Silt traces (C	l Black CLAY CH)*	with Organics	-	0.25	204	27	0.13		
	-	ST-4	22			Very Sc	oft, Gray CLA	AY with Orga	nic pockets (CH)	-	0.25	95	50	0.06	123	90
10	10— -	ST-5	18			Very Sc	oft, Gray CLA	AY with Orga	nics (CH)*	_	0.25	88	52	0.07	97	70
15	- - 15 - -	ST-6	18			- - - - -	oft, Gray CL/	AY with Orga	nic pockets (CH)	-	0.25	141	36	0.07	144	104
20	- 20 - -	ST-7	20			- Very Sc -	oft, Gray CL/	AY with Silt ((CH)	-	0.50	50	75	0.14	58	36
25	- 25–	ST-8	16			- Very Sc Orga	oft, Gray CL/ inics (CH)*	AY with Silt p	ockets and	-	0.25	98	51	0.11		



Log of Boring B-2

Sheet 2 of 2

SAMPLES MATERIAL DESCRIPTION State of the second s				SA	MPL	ES				(tsf)					%
35 35- - - 1.00 42 69 0.12 78 53 35 35- - <th>Elevation feet</th> <th>Depth, feet</th> <th>Type</th> <th>Number</th> <th>Recovery, in.</th> <th>Sampling Resistance, blows / ft</th> <th>Graphic Log</th> <th>MATERIAL DESCRIPTION</th> <th>Torvane (tsf)</th> <th>Hand Penetrometer</th> <th>Water Content, %</th> <th>Dry Unit Weight, pcf</th> <th>Cohesion (ksf)</th> <th>Liquid Limit, %</th> <th>Plastic Index,</th>	Elevation feet	Depth, feet	Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index,
	30	- - - - - - -		ST-9	20			Bottom of hole @ 30 feet below MUDLINE	-	1.00	42	69	0.12	78	53
	35	- 35- -	-					Laboratory Results							
	40	- 40 - -	-												
	45	- 45 - -	-				-		-						
	50	- 50 - -	-					·	-						
	55	- 55-					-		-						

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Log of Boring B-3

Sheet 1 of 2

Date(s) Drilled	2/20/09 - 2/20/09	Logged By	A. Bukkapatnam	Checked By I. Harrouch
Drilling Method	Rotary Wash	Drill Bit Size/Type	Bottom Discharge 4(5/8)"	Total Depth Drilled (feet) 40.7
Drill Rig Type	Marsh Buggy	Drilling Contractor	SESI	Sampler Type(s) Piston Sampler/ Shelby Tube
	ater Level Measured -0.2' 2/20/2009	Hammer Data	140 LBS Safety	Approximate Surface Elevation -0.2'
Location	N413674.665 E3689203.468			Borehole Backfill Cement Grout

			SA	MPL	ES				(tsf)				_	~
Elevation feet	D epth, feet	Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
	U		ST-1	14			WATER 	-		1171			996	644
	-		ST-2	12			Very Soft, Black PEAT with Clay (PT)*	-	0.25	383		0.12		
5	5— -		ST-3	18			Very Soft, Gray CLAY with Organic pockets (CL)*	-		171		0.06	141	102
	-		ST-4	18			Very Soft, Gray Lean CLAY with trace Organics (CL)*	-	0.25	43		0.14		
10	- 10		ST-5	16			Very Soft, Gray Lean Clay (CL - ML)*	-	0.50	46		0.07	45	15
15	- - 15 -		ST-6	12					0.50	90		0.08	126	104
20	- 20 -		ST-7	18			- Very Soft, Gray Clay becoming Organic Peat and – Clay (CH) – 	-	0.50	230		0.11		
25	- 25– -		ST-8	18			Very Soft, Gray CLAY with Organics (CH)*	-		100		0.13	108	81

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Log of Boring B-3

Sheet 2 of 2

		S	AMPL	ES				tsf)					<u>`</u> 0
Elevation feet	Depth, feet		Recovery, in.	aî.	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
30	- - 30 - -	ST-6	9 20						33		0.38		
35	- 35 -	ST-1	0 18			Gray Sandy Silt with Clay pockets (ML)*	-		26		5.12	NP	NP
40	- - 40 -	ST-1	1 20			 Loose, Gray Sandy Silt with trace Clay (ML) Bottom of hole @ 40 feet below MUDLINE * - Look at Table: Boring B - 3 for additional Laboratory Results 	-		27		0.26	NP	NP
45	- - 45 -					- · ·	-						
50	- - 50 -					- · ·	-						
55	- - 55 -						-						

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Log of Boring B-4

<u> </u>																	
Date(s Drilled	⁾ 2/1	7/09 - 2/1	17/09				Logged By	A	. Bukkapatnam			Check By	^{ed} I.	Harrou	ıch		
Drilling Method	d Rot	ary Was	sh				Drill Bit Size/Type	В	ottom Discharge 4(5/8)"			Total Drilled	Depth (feet)	40.7			
Drill Ri Type	^g Ma	rsh Bug	gy				Drilling Contractor	S	ESI			Sample Type(s	er F s) T	Piston Tube	Sampl	er/ Sh	elby
Ground and Da	dwater I ate Mea	_evel 0. sured 0.	2' 2/17	7/2009			Hammer Data	14	40 LBS Safety			Approx Surfac	kimate e Eleva	ation	0.2'		
Locatio	on N4 ′	1968.84	1 E36	90156.7	52							Boreho Backfil	le Co	ement	Grout		
		SA	MPL	FS								sf)					
Elevation feet	Depth, feet		Recovery, in.	ů.	Graphic Log	I	MATERI	IAL	DESCRIPTION		Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
-0	0-					WATER							20				
	-	ST-1				·	NE El0.47 vith Clay *	<u>/</u>		/-			860			958	427
	-	ST-2				- Very So (OH)	oft, Dark Gra)*	ay C	CLAY with Organic pockets	\$ - _			333	17	0.11	482	386
_	5	╂┤														102	
5	- -	ST-3				Very Sc	oft, Gray CL	AY	with Organic pockets (CH) _			80	56	0.07	122	83
	-	ST-4				- Very Sc trace	oft, Gray CL e Shells (CH	_AY ⊣)*	with Organic pockets and	-			72	49	0.06	64	41
10	- 10— -	ST-5				- Very Sc Shell	oft CLAY wit Is (CH)*	ith S	ilt, Organic pockets and				90	50	0.07		
15	- - 15 -	ST-6				- Very Sc - (CH) -	oft, Gray CL	_AY	with Organic and Silty Cla	- - - - - -			114	45	0.10	91	58
20	- 20— -	ST-7				- Very Sc - pock	oft, Gray CL ets (CH)*	_AY	with Silt and Organic	-			91	50	0.09		
25	- - 25-	ST-8				- Very Sc Sanc	oft, Gray CL dy Silt and S	_AY Silty	with Organic pockets, Sand layers (CH)*	-		0.25	97	57	0.10	101	62



Log of Boring B-4

Sheet 2 of 2

		S	AMPL	ES				tsf)					,o
Elevation feet	Depth, feet		Recovery, in.	di	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
30	- - 30	ST-9				Firm, Gray Clayey SILT (ML)		0.25	30	92	0.87		
35	- 35- -	ST-10	D		-	Firm, Gray Sandy SILT with Clay (ML)*	-	0.25	28	99	1.08	NP	NP
40	- - 40 - -	ST-1	1			Soft, Gray CLAY (CH) Bottom of hole @ 40 feet below MUDLINE * - Look at Table: Boring B - 4 for additional Laboratory Results	-	0.30	63	66	0.38	63	39
45	- 45 -				-	·							
50	- 50 -				-	· · · · · · · · · · · · · · · · · · ·							
55	- 55 -				-	·	-						



Log of Boring B-5

Date(s Drilled	⁾ 2/1	6/09 - 2/1	7/09				Logged By	А. В	sukkapatnam		Check By	^{ed} I.	Harrou	ıch		
Drilling Method	d Rot	ary Was	h				Drill Bit Size/Type	Bott	tom Discharge 4(5/8)"		Total I Drilled	Depth (feet)	60.4			
Drill Ri Type	^g Ma	rsh Bugg	ау				Drilling Contractor	SES	il		Samp Type(s	er F s) T	Piston Tube	Sampl	er/ Sh	elby
Ground and Da	dwater I ate Mea	Level 0.	2' 2/17	7/2009			Hammer Data	140	LBS Safety		Appro Surfac	ximate e Eleva	ation ().2'		
Locatio	on N4 ′	12894.74	1 E36	91318.7	62						Boreh Backfi	ole C	ement	Grout		
		SA	MPL	ES							tsf)					
Elevation feet		Type Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	I	MATERI	AL	DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
-0	0-						R NE El0.22	,		7						
	-	ST-1	17				oft PEAT (PT			/ _ _		428	11	0.05		
	-	ST-2	24			PEAT v	with Clay and	d Orga	anics (PT-OH)*	-		223			223	165
5	5	ST-3	13			Very So	oft, PEAT wi	th Cla	y and Organics (PT-OH)*	-		334	17	0.07		
	-	ST-4	23			Very So	oft Gray CLA	AY wit	h Organic pockets (CH)	-		84	55	0.05	68	42
10	- 10-	ST-5	22			Very So trace	oft Gray CLA e Silt pockets	λΥ wit s (CH)	h Organic pockets and)	-		62	64			
15	- - - 15	ST-6	20			Very So Fine	oft, Gray Lea Sand (CH)*	an CL/	AY with Organics and	-		117	39	0.08	78	42
20	- - 20 -	ST-7	22			Very So -	oft Gray CLA	Y wit	h Organic pockets (CH)*	-		138	40	0.07		
25	25–	ST-8	23			Very So	oft, Gray SIL	.TY CI	LAY (CL)*	-		168	40	0.09	47	23



Log of Boring B-5

Sheet 2 of 3

		S	AMPL				(tsf)				.0	%
Elevation feet	Depth, feet	Type Number	Recovery, in.	Sampling Resistance, blows / ft Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
30	- - - 30-	ST-9	23		Very Soft, Gray CLAYEY Silt with Clay and Sand (CL-ML)			33	81	0.09	34	6
35	- - 35	ST-1	0 17		Alternating layers of Very Soft, Gray SILTY CLAY with Sand (CL)			47	72			
40	- - 40	ST-1	1 24		Loose Gray SILT with CLAY layers (ML)*			38	89	0.46	NP	NP
45	- - 45	ST-12	2 19		Medium, Gray CLAYEY Silt with Clay (CL-ML)*			32	95	0.60		
50	- - 50 -	ST-1	3 18		Very Soft to Soft Gray CLAY (CH)*	•		68	62	0.24	79	44
55	- - 55	ST-14	4 22		Very Soft to Soft, Gray CLAY with Silt pockets and trace Organics (CH)*			56	69	0.22		

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Log of Boring B-5

Sheet 3 of 3

SAMPLES MATERIAL DESCRIPTION Image: second			SA	MPL					r (tsf)			f)	%	%
60 60 St.15 15 Soft Gray CLAY with trace Organics (CH)* 53 74 0.38 67 42 60 60 St.15 15 Bottom of hole @ 00 feet below MUDLINE 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 65 65 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 65 65 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 70 70 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 70 70 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 75 75 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 75 75 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 100 kal Table Boring B - 5 for additional 75 75	Elevation feet	Depth, feet	Type Number	Recovery, in.	Sampling Resistance blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometei	Water Content, %	Dry Unit Weight, pcf	Cohesion (ks	Liquid Limit, ⁹	Plastic Index,
	60	- - - 60- - -	ST-1	5 15			Bottom of hole @ 60 feet below MUDLINE			53	74	0.38	67	42
	65	- 65 - -												
	70	- 70 -												
	75	- 75 -												
	80	- - -												
	85	- 85 -												

Log of Boring B-6

Date(s Drilled	⁾ 2/1	7/09 - 2/ [,]	17/09				Logged	A. Bukk	apatnam			Check By	^{ed} I.	Harrou	ıch		
Drilling	Det	tary Was					By Drill Bit Size/Type		Discharge 4(5/8	3)"		Total Drilled	Depth	62.2			
Drill Ri Type		rsh Bug	ду				Drilling Contractor	SESI				Sampl Type(s	er F	Piston ube	Sampl	er/ Sh	elby
Ground	dwater ate Mea	Level		7/2009			Hammer Data	140 LBS	Safety			Approx).2'		
		11864.05	51 E36	92474.2	43		Dulu					Boreho Backfil	ole 👝	ement	Grout		
-		64	MPL	ES													\square
 ☐ Elevation feet 	Depth, feet	Type Number 5	Recovery, in.	aî.	Graphic Log	I	MATERI	AL DE	SCRIPTION	I	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
_0	-					WATEF	۲			_							
	-					MUDLI	NE El1.97			_							
	-	ST-1	22			- Very So	oft, PEAT wi	th Clay (P	T)*	-			194	23		289	145
5	5	ST-2	23			– Very So (PT/	oft, Brown O OH/CH)*	rganic CL	AY with Peat	_			374	18	0.08		
	-	ST-3	18			Very So	oft, Gray CL/	AY with O	rganic pockets ((CH)* - -			123	43	0.07	120	76
10	- 10-	ST-4	19			Very So	oft, Gray CL/	AY with O	rganic pockets ((CH) - -							
	-	ST-5	22			Very So	oft, Gray CL/	AY with O	rganic pockets ((CH)* - - -			99	52	0.10	67	33
15	- 15 - -	ST-6	22			- Very So	oft, Gray CL/	AY with O	rganic pockets ((- CH) - _ -			124	44			
20	- 20— -	ST-7	12			- Very So SILT	oft, Gray CL/ `with Clay (0	AY becom CH becom	ing Gray SAND ing ML)*	- - - -			104	47	0.10		
25	- 25	T				-				- - -							



Log of Boring B-6

Sheet 2 of 3

		SA	MPL	ES				(tsf)			-		%
Elevation feet	Depth, feet		Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
	-	ST-8	22			Very Soft, Gray CLAY becoming Gray SILT with Clay (CH) -			83	63	0.16	130	90
30	30 - - -	ST-9	22			Very Soft, Gray CLAY with Silt (CH)*			71	61	0.18		
35	35— - - -	ST-10	21			Soft, Gray CLAY becoming Gray SILT with Clay - (CH)* -			46	84	0.36	83	52
40	40 - - -	TST-11	10			Soft, Gray CLAY with trace Silt and Organics - (CH)* -			62	68			
45	45 - - -	TST-12	23			Loose, Gray SILT with trace Organics, trace silt and silt lenses, with Clay (MH)* - -			50	76	0.33	55	22
50	50 - - -	ST-13	22			Medium, Gray CLAY with Silt pockets (CH) -			50	81	0.34		
55	55— -												

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Log of Boring B-6

Sheet 3 of 3

	SAMPLES				(tsf)					%
Elevation feet Depth, feet	Type Type Number 61 Recovery, Sampling Resistance	blows / ft Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
- 60 60-	TST-14 19		Soft, Gray CLAY with trace Silt (CH)*			63	66	0.60		
65 65- -			Bottom of hole @ 60 feet below MUDLINE * - Look at Table: Boring B - 6 for additional Laboratory Results							
75 75- -			 							
<u>85</u> 85-										

Log of Boring B-7

Date(s)	7/09 - 2/					Logged	A Bu	kkapatnam			Check	ed I	Harrou	ich		
Drilled Drilling	D -4	ary Was					By Drill Bit		m Discharge 4(5/	/8)"		By Total D	Depth	41.8			
Methoo Drill Ri	~	rsh Bug					Size/Type Drilling	0501		.0)		Drilled Sample	er F	Piston		er/ Sh	elby
Type Ground				7/0000			Contractor Hammer					Type(s Approx	kimate	Tube			
	dwater I ate Mea			7/2009	<u></u>		Data	140 L	BS Safety			Surfac Boreho	e Eleva		0.2'		
Localic	n N4 1	10229.20	5 E30	92943.9	38							Backfil		ement	Grout		
		SA	MPL									r (tsf)			f)	%	%
Elevation feet	Depth, feet	Type Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	I	MATERI	AL D	ESCRIPTION	N	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, 9	Plastic Index,
-0	0					_ WATEF	R NE El -1.63	'		-							
	_	ST-1	20			_			pockets (PT)			<0.25	955	6	0.04	925	595
5	5-	ST-2	15			- Very Sc - (PT)	oft, PEAT be	ecoming	Clay with Organic			<0.25	309	18		384	284
	-	ST-3	22			- Very So	oft, Gray CL	AY with	Organics (CH)	-		<0.25	112	45	0.05		
	-	ST-4	18			Very So (CL)		LTY CLA	Y with trace Orga	anics		<0.25	90	52	0.06		
10	10	ST-5	15			Very So and	oft, Gray CL pockets (Ol	.AY with H)*	Humus, Organic I	layers		<0.25	334	18	0.10	240	178
15	- - 15 - -	ST-6	16			- Very Sc - SAN -	oft, Intermix DY SILT (C	ed Gray L to ML	CLAY, SILT and	-		<0.25	55	70	0.08		
20	- 20— - -	ST-7	18			- Soft, Gr - -	ray SILTY (CLAY wit	h trace Organics (- (CL)* - -		0.25	48	83	0.29	43	22
25	_ 25—	ST-8	18			- Firm, C	LAYEY SIL	T with tr	ace Sand (ML)*	-		0.25	29	99	1.06		



Log of Boring B-7

Sheet 2 of 2

	Depth,	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	r ent, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
30	-						Torv	Hanc Pene	Water Content, ⁶	Dry U Weigh	Cohes	Liquid	Plastic
	30	ST-9	16			- Very Soft, Gray CLAY with Silt streaks and trace Organics (CH)*		0.30	56	71	0.17	90	60
35	35	ST-10) 20			- Soft, Gray CLAY becoming Gray SILT with Clay (CH) -		0.35	25	99	0.24		
40	40	ST-11	20			Soft, Gray SILTY CLAY with Sandy Silt (CL) Bottom of hole @ 40 feet below MUDLINE * - Look at Table: Boring B - 7 for additional	- - -	0.40	47	77	0.34	35	12
45	- 45- - -					* - Look at Table: Boring B - 7 for additional Laboratory Results							
50	- 50 - -												
55	- 55 -				-								

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Log of Boring B-8

Date(s) 2/10	9/09 - 2/ [,]	19/09				Logged	A B	ukkapatnam		Check	ed I	Harrou	ich		
Drilled Drilling Method		ary Was					By Drill Bit		om Discharge 4(5/8)"		By Total D Drilled	Depth	41.8			
Drill Ri		rsh Bug					Size/Type Drilling Contractor	SES			Sampl	er F	Piston		er/ Sh	elby
Type Ground and Da		-		9/2009			Hammer		LBS Safety		Type(s Approx	kimate e Eleva	ube).2'		
		10752.08			24		Data		-		Boreho Backfil	ole 👝	ement			
\square				50						1						
Elevation feet	Depth, feet	Type Number 6	Recovery, in.		Graphic Log	I	MATERI	AL [DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
-0	0-					WATEF	2									
	-	ST-1	20			-	NE El1.63 oft, PEAT (F			-		766	8	0.07		
5	5	ST-2	20			Very Sc	oft, PEAT wi	ith Clay	y pockets (PT)*	-	0.25	383	15	0.13		
	-	ST-3	22			Very Sc - (CH-	oft, Gray CL OH)*	AY wit	h Organic pockets		0.25	140	36	0.09	185	137
	-	ST-4	18			Very Sc	oft, Gray CL	AY wit	h Organic pockets (CH)	-	0.25	117	44	0.06	96	63
10	10— - -	ST-5	18			– Very Lo – Orga –	oose, Gray S anic pockets	SILTY (s (MH)*	CLAY with Clay and	-	0.25	130	40	0.05	87	36
15	- 15 - -	ST-6	16				Gray SILT v iets (ML)*	with tra	ce Sand and Silty Clay	-	0.25	50	75	0.82	NP	NP
20	- 20 - -	ST-7	22			- Loose, - and (Gray SILT v Organic poo	with tra ckets (N	ce Fine Sand and Clay ML)*	-	0.75	29	96	0.98	NP	NP
25	_ 25–	ST-8	18			- Very Sc	oft, Gray CL	AY wit	h Silt and Organics (CH)	-	0.50	107	46	0.13	107	71



Log of Boring B-8

Sheet 2 of 2

SAMPLES MATERIAL DESCRIPTION Image: State of the sta			SA	MPL					(tsf)			(%	%
30 30 ST-9 22 Very Soft Ciray CLAY with Silt pockets becoming Ciray Silt with Clay (CL-ML)* 35 35 ST-10 18 Ciray Silt with Clay (CL-ML)* 40 40 ST-11 18 Ciray CLAY and Silt with Clay (CL-ML)* 40 40 ST-11 18 Ciray CLAY and Silt with trace Sand 40 40 ST-11 18 Ciray CLAY and Silt with trace Sand 40 40 ST-11 18 Ciray CLAY and Silt with trace Sand 40 40 ST-11 18 Ciray CLAY and Silt with trace Sand 40 40 40 40 40	Elevation feet	Depth, feet	Type Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer	Water Content, %	Dry Unit Weight, pcf	Cohesion (kst	Liquid Limit, 9	Plastic Index,
-40 40 - 0.25 62 66 0.40 34 9 -40 40 - - - - 0.50 32 85 0.14 -40 40 - - - 0.50 32 85 0.14 -40 40 - - - 0.50 32 85 0.14 -40 - - - - 0.50 32 85 0.14 - - - - - - - 0.50 32 85 0.14 - - - - - - - 0.50 32 85 0.14 - - - - - - - 0.50 32 85 0.14 - <td< td=""><td>30</td><td>- - 30 - -</td><td>ST-9</td><td>22</td><td></td><td></td><td>Very Soft, Gray CLAY with Silt pockets becoming Gray Silt with Clay (CH)*</td><td>-</td><td>0.75</td><td>60</td><td>64</td><td>0.09</td><td></td><td></td></td<>	30	- - 30 - -	ST-9	22			Very Soft, Gray CLAY with Silt pockets becoming Gray Silt with Clay (CH)*	-	0.75	60	64	0.09		
	35	- 35 - -	ST-10) 18			Loose, Gray SILT with Clay (CL-ML)*	-	0.25	62	66	0.40	34	9
-45 45- 45 45- 	40	- 40 -	ST-11	18			Intermixed Gray CLAY and SILT with trace Sand and Organics (CL-ML)*	-	0.50	32	85	0.14		
	45	- - 45 - -					End of hole @ 40 feet below MUDLINE * - Look at Table: Boring B - 8 for additional Laboratory Results	-						
	50	- 50 - -						-						
	55	- 55 -	-					-						

Log of Boring B-9

Date(s Drilled	⁾ 2/1	9/09 - 2/ [.]	19/09				Logged By	A. E	Bukkapatnam		Check By	^{ed} I.	Harrou	ich		
Drilling Method		ary Was	sh				Drill Bit Size/Type	Bot	tom Discharge 4(5/8)"		Total Drilled	Depth (feet)	62.8			
Drill Ri Type	^g Ma	rsh Bug	gy				Drilling Contractor	SES	81		Sampl Type(s		Piston Tube	Sampl	er/ Sh	elby
Ground and Da	dwater I ate Mea	Level 0. sured 0.	2' 2/1	9/2009			Hammer Data	140	LBS Safety		Approx Surfac	kimate e Eleva	ation ().2'		
Locatio	on N4 (9821.95	51 E36	95191.9	11						Boreho Backfi		ement	Grout		
		SA	MPL	ES							tsf)					
 Elevation feet 	D epth, feet	Type Number	Recovery, in.	a,	Graphic Log		MATERI	AL	DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
	-	_				- WATEF MUDLII	R NE El2.63	3'		-						
5	- 5	ST-1	20"			PEAT(PT)			-		894	6			
5	-	ST-2	12"			Very So	oft, PEAT wi	ith Cla	ay and Organics (PT)*	-		255	20	0.06	257	173
	-	ST-3	18"			Very So	oft, Gray CL/	AY wi	th Organics (CH)*	-	0.25	135	36	0.11		
10	10-	ST-4	20"			PEAT v	with Clay poo	ckets	and Silt pockets (PT)*	_	0.25	334	17	0.17	573	427
	-	ST-5	18"			Very So	oft, SILTY C	LAY v	vith Organics (CL)*	-	0.25	205	22	0.05		
	- 15	ST-6	18"			Very So pock	oft, Gray CL/ kets (CH)*	AY wi	th trace Silt and Organic		0.50	60	62	0.08	65	39
−-15	-	ST-7	20"			Very So (CH)		AY wi	th trace Organic pockets		0.25	59	72	0.15		
	-	ST-8	18"			Very So (CH)		AY wi	th Silt and trace Organic	-	0.25	49	81	0.13	54	26
20	20-	ST-9	20"			Loose, – Fine	Gray SILT w Sand (ML)	with cl	ay pockets and trace	_	0.75	34	87	0.53		
	=	ST-10	22"			Firm, G (ML)		th trac	ce Fine Sand and Clay	-	0.25	25	95	2.94	NP	NP
	-	ST-1	1 18"			Very So	oft, Gray CL/	AY wi	th Silt lenses (CH)	-	0.25	98	51	0.10		
25	25									1						

Log of Boring B-9

Sheet 2 of 3

		SA	MPL	ES				(tsf)				_	%
Elevation feet	Depth, feet	⊢ Z	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index,
		ST-12	18"			Soft, Gray CLAY with Silt pockets (CH)*		0.25	51	67		66	39
	-	ST-13	18"			- Very Soft, Gray CLAY with Silt (CH)* -		0.25	80	58	0.11		
30	- 30—	ST-14	22"			Soft, Gray CLAY with Silt pockets (CH)		0.25	64	62			
	-	ST-15	16"			- Very Soft, Gray CLAY with trace Silt and trace Organics (CH)*		0.50	71	60	0.14	72	45
	-	ST-16	20"			Loose, Gray SANDY SILT with Clay pockets (ML)		0.50	30	94			
35	35— -	ST-17	16"			Soft, Intermixed CLAY and SANDY SILT (CL-ML)		0.75	39	82	0.48	38	7
	-	ST-18	20"			Soft, Gray SILT with CLAY pockets (ML)*		0.25	43	78			
40	- 40	ST-19	16"			Soft, Gray SILT with CLAY pockets (ML)		0.25	55	66	0.31	86	52
	-	ST-20	16"			Soft, Gray SILT with CLAY pockets and layers (ML)		0.50	53	68			
	-	ST-21	16"			Very Soft, Gray CLAY with trace Silt (CH)		0.50	63	64	0.15		
45	45— -	ST-22	18"			Very Soft, Gray CLAY with Silt pockets (CH)		0.25	54			60	34
	-	ST-23	18"			Soft, Gray CLAY with Sandy Silt pockets (CH)*		0.25	58	65			
50	50-	ST-24	22"			Very Soft, Gray CLAY with Silt pockets (CH)		0.25	57	67	0.19	52	31
	_	ST-25	12"			Sandy Clayey SILT (ML)*		0.25	34				
	- 55	ST-26	22"			Medium, Gray CLAY with Silt pockets (CH)		0.50	43	76	0.46	56	30
55		ST-27	22"			Very Soft, Gray CLAY with trace Silt and Organics (CH)		0.75					

Log of Boring B-9

Sheet 3 of 3

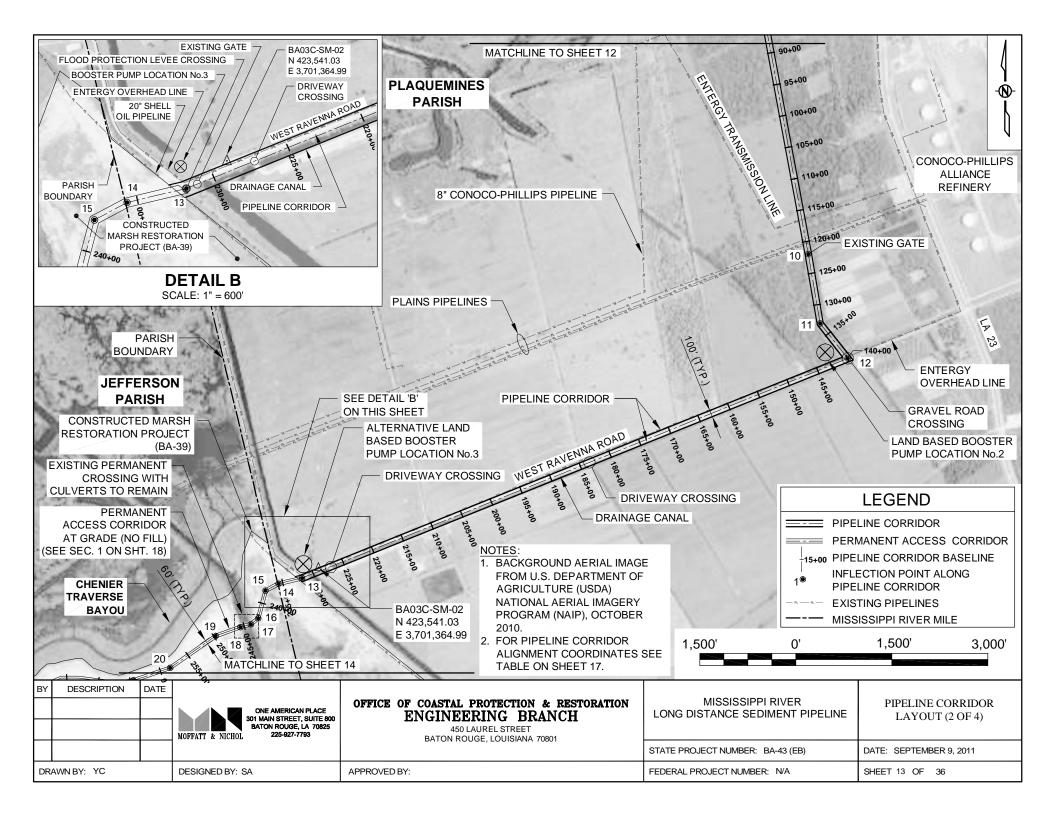
60 60 ST-28 22" Soft, Gray CLAY with Silt (CH)* 0.50 59 67 0.36 76 Soft to Medium, Gray CLAY (CH) 0.50 58 0.			SA	MPL					(tsf)			(%	%
60 60 ST-28 22" Soft, Gray CLAY with Slit (CH)" 0.50 59 67 0.36 70 Soft to Medium, Gray CLAY (CH) 0.50 58 0.50 58 0.50 58 0.50 57 66 0.15 60 ST-30 18" Very Soft, CLAY with trace Slit (CH)" 0.50 57 66 0.15 61 65 65	Elevation feet	Depth, feet	Type Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer	Water Content, %	Dry Unit Weight, pcf	Cohesion (kst	Liquid Limit, %	Plastic Index, %
60 60 151-29 20" ST-30 18" Very Soft, CLAY with trace Silt (CH)* - 0.50 57 66 0.15 65 - 0.50 58 - 0.50 57 66 0.15 65 - 0.50		-	ST-28	3 22"			Soft, Gray CLAY with Silt (CH)*					0.36	76	49
65 65 70 70 75 75 75 75 757575 75 75 757575 757575 757575 757575 757575 757575 757575 757575 75757575 75757575 7575757575 7575757575757575	60	60—	ST-29	20"			Soft to Medium, Gray CLAY (CH)		0.50	58				
65 65- 		-	ST-30) 18"			-		0.50	57	66	0.15	69	43
		-					Bottom of the hole @ 60 feet below mudline * - Look at Table: Boring B - 9 for additional Laboratory Results							
	65	65-												
		-				-	·							
	70	- 70												
		-				-	· · ·							
		-				-	· · ·							
	75	75 -				-								
		-				-	· · ·							
	80	- 80—					 							
		-					· · ·							
		-					· -							
85 85- 	85	85 -												
Template: 19228956_BAYOUDUPONT Proj ID: 19228956.00001.GPJ				<u>I</u>	I	<u> </u>		ļ	ļ	<u> </u>	I	<u> </u>	I	I

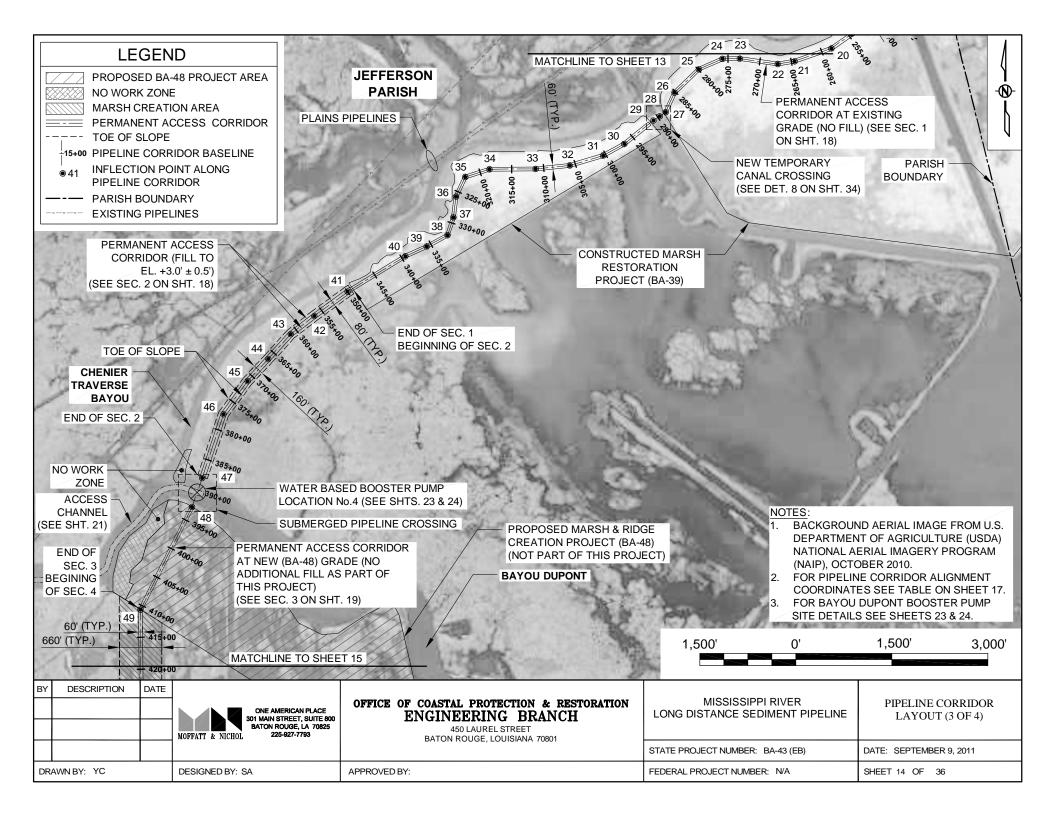


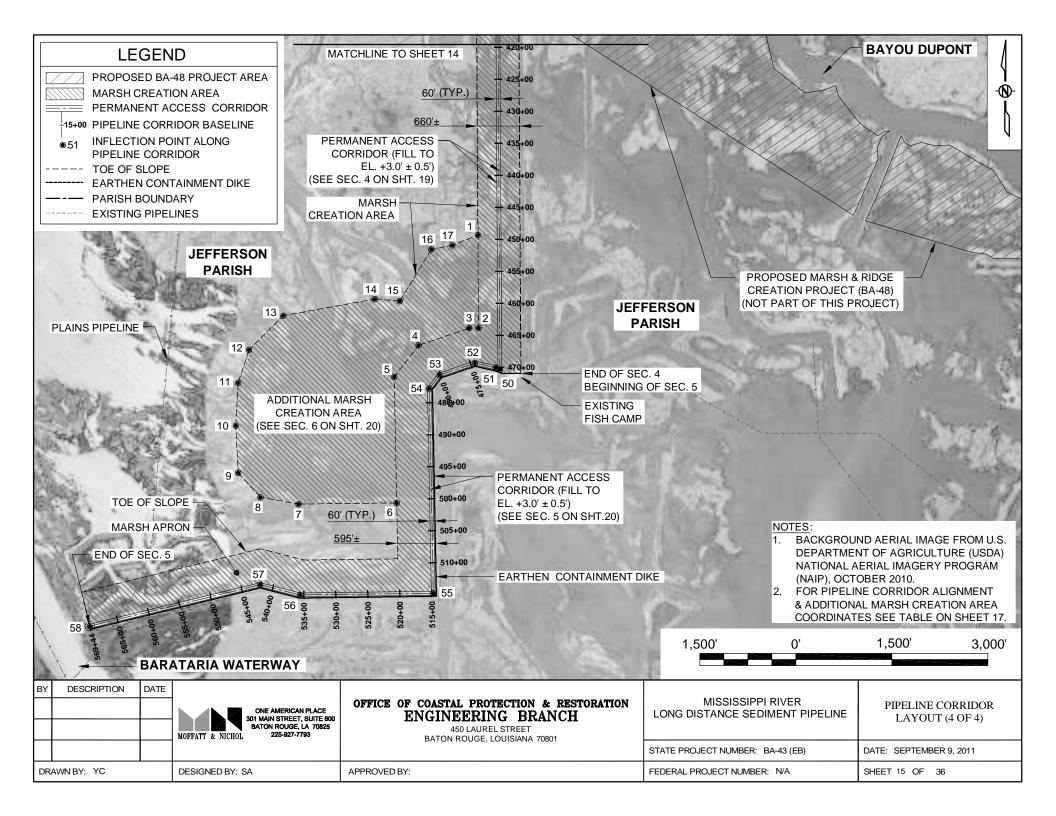
APPENDIX E

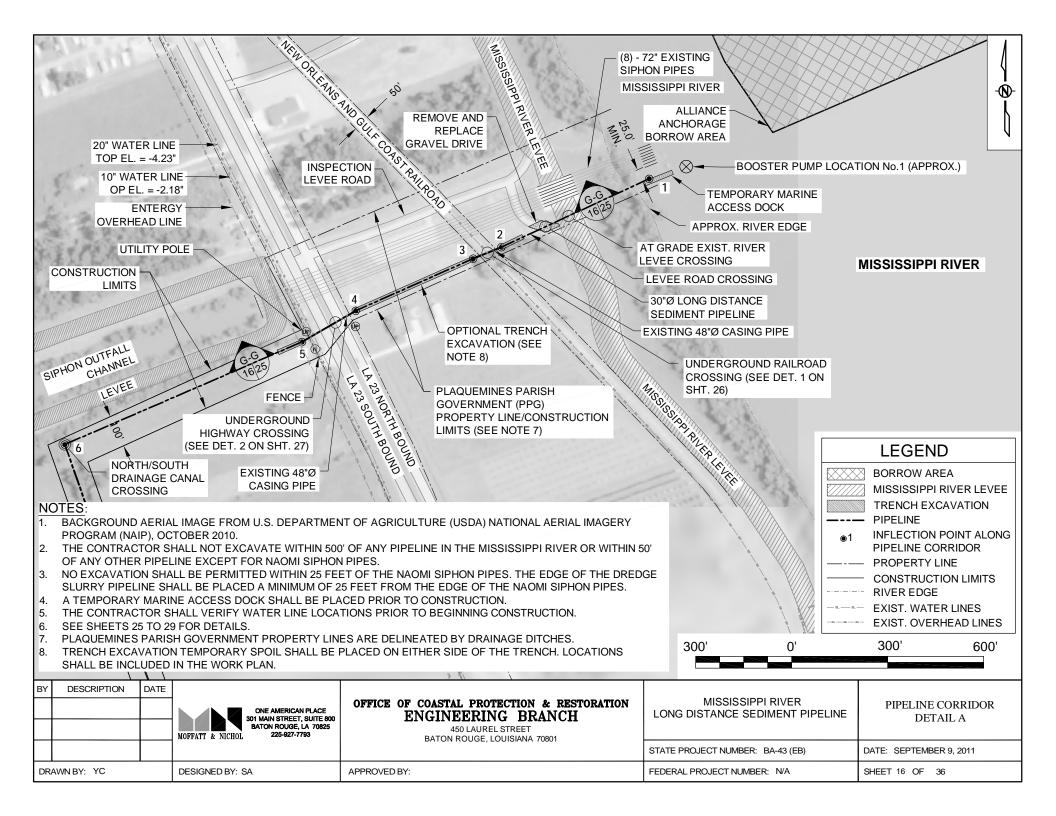
TYPICAL CROSS-SECTIONS PROVIDED BY MOFFATT AND NICHOL











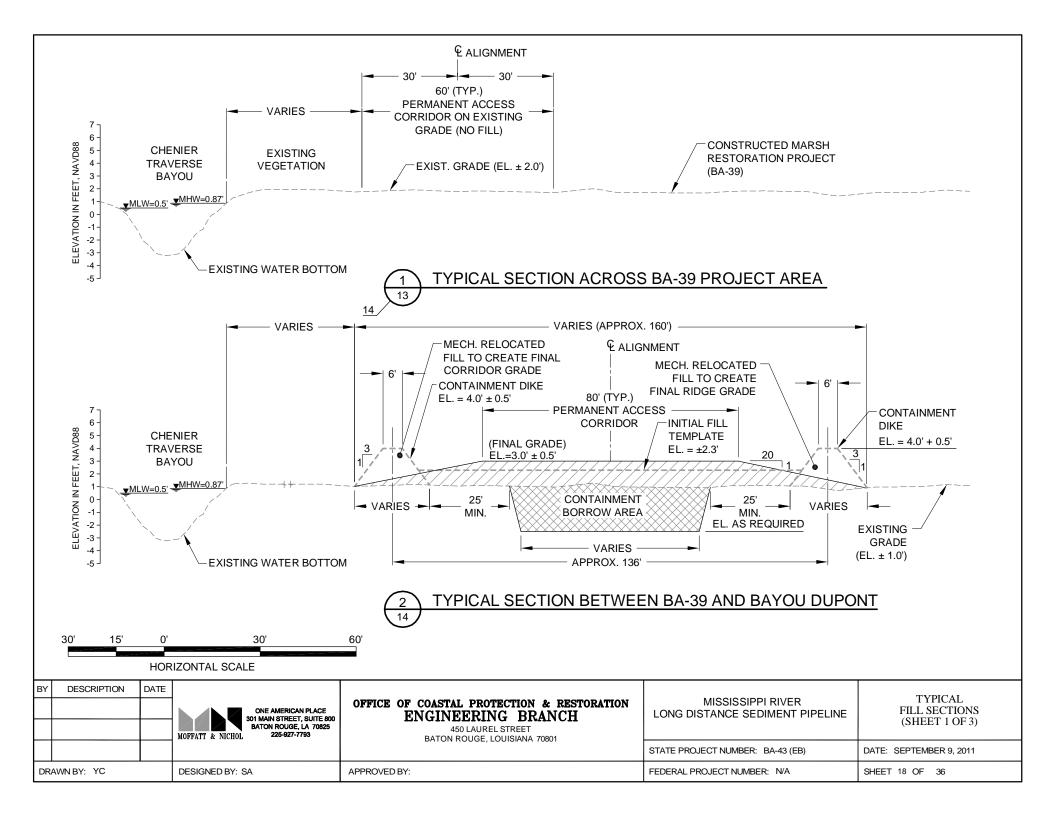
PIPELINE CORRIDOR ALIGNMENT

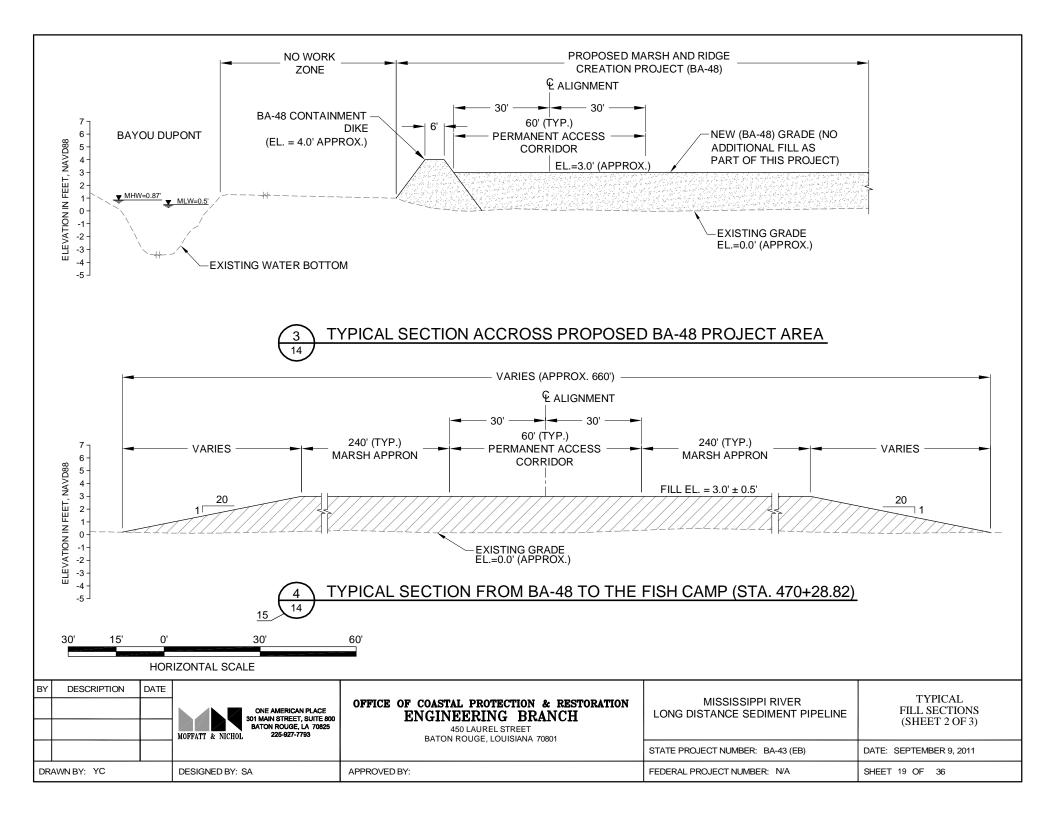
PT.	EASTING	NOTRHING	PT.	EASTING	NOTRHING		PT.	EASTING
1	3709295.15	439287.46	46	3689546.48	416264.89		1	3674046.3
2	3708833.00	439073.60	47	3689213.40	415268.22		2	3674443.8
3	3708745.00	439037.80	48	3689054.74	414815.39		3	3674549.1
4	3708378.00	438874.90	49	3688249.91	413214.21		4	3674605.3
5	3708210.00	438777.60	50	3688282.83	407251.28		5	3674768.3
6	3707468.37	438457.08	51	3688214.75	407277.40		6	3674891.1
7	3708010.71	436924.44	52	3687891.71	407348.42		7	3675173.9
8	3708151.13	433271.33	53	3687340.48	407159.87		8	3675374.3
9	3708274.87	432470.08	54	3687180.94	406952.63		9	3675899.4
10	3709020.90	428442.06	55	3687243.43	403753.80		10	3676242.80
11	3709207.34	427358.82	56	3685161.39	403726.37		11	3676428.65
12	3709640.03	426810.80	57	3684537.11	403885.76		12	3676548.44
13	3701112.29	423381.44	58	3681873.45	403237.73		13	3676739.59
14	3700741.69	423294.08					14	3677375.53
15	3700538.00	423185.19		DITIONAL MA			15	3677870.90
16	3700424.62	422753.89	AD		ARON AREA		16	3678337.82
17	3700308.53	422659.59	PT.	EASTING	NOTRHING		17	3678811.83
18	3700145.88	422615.52					18	3679772.32
19	3699761.50	422478.14	1	3687941.24	409350.34		19	3679930.74
20	3699047.76	421979.44	2	3687949.27	407895.61	:	20	3680221.2
21	3698472.93	421778.59	3	3687802.63	407895.61		21	3680593.8
22	3698209.03	421735.03	4	3687011.95	407626.56		22	3680718.2
23	3697614.62	421819.58	5	3686632.31	407133.37		23	3680950.8
24	3697345.59	421817.02	6	3686670.77	405164.44		24	3681378.5
25	3696976.65	421653.04	7	3685135.17	405145.15		25	3681635.2
26	3696595.44	421288.58	8	3684540.07	405252.97		26	3681977.30
27	3696457.72	420983.63	9	3684192.66	405633.55		27	3682205.5
28	3696365.29	420919.59	10	3684154.49	406370.04		28	3682250.83
29	3696265.66	420853.30	11	3684191.67	407042.44		29	3682397.09
30	3695810.63	420487.43	12	3684363.02	407557.46	;	30	3683138.30
31	3695480.80	420305.26	13	3684898.65	408089.54		31	3683474.3
32	3694958.57	420150.54	14	3686328.06	408348.46		32	3683792.94
33	3694425.06	420098.06	15	3686719.48	408317.68		33	3684035.9
34	3693702.83	420090.22	16	3687210.41	409124.00		34	3684285.5
35	3693324.98	419970.64	17	3687540.48	409189.26		35	3684542.7
36	3693181.49	419664.54				'	36	3684764.8
37	3693138.44	419339.30					37	3685015.3
38	3693047.57	419061.89		PROBA			38	3685168.42
39	3692722.33	418884.92	BOO	STER PUMP	LOCATIONS		39	3685281.60
40	3692387.88	418732.22		FAOTING	NOTDUINO		40	3685359.4
41	3691538.38	418212.51	No.	EASTING	NOTRHING		41	3685450.5
42	3690965.90	417799.60	1	3709411.03	439325.16		42	3685898.0
43	3690596.95	417515.21	2	3709430.00	426505.97		43	3686447.2
44	3690245.94	417128.33	3	3701075.84	423518.50		44	3686740.1
45	3689923.11	416782.44	4	3689132.52	415040.26		45	3687188.6

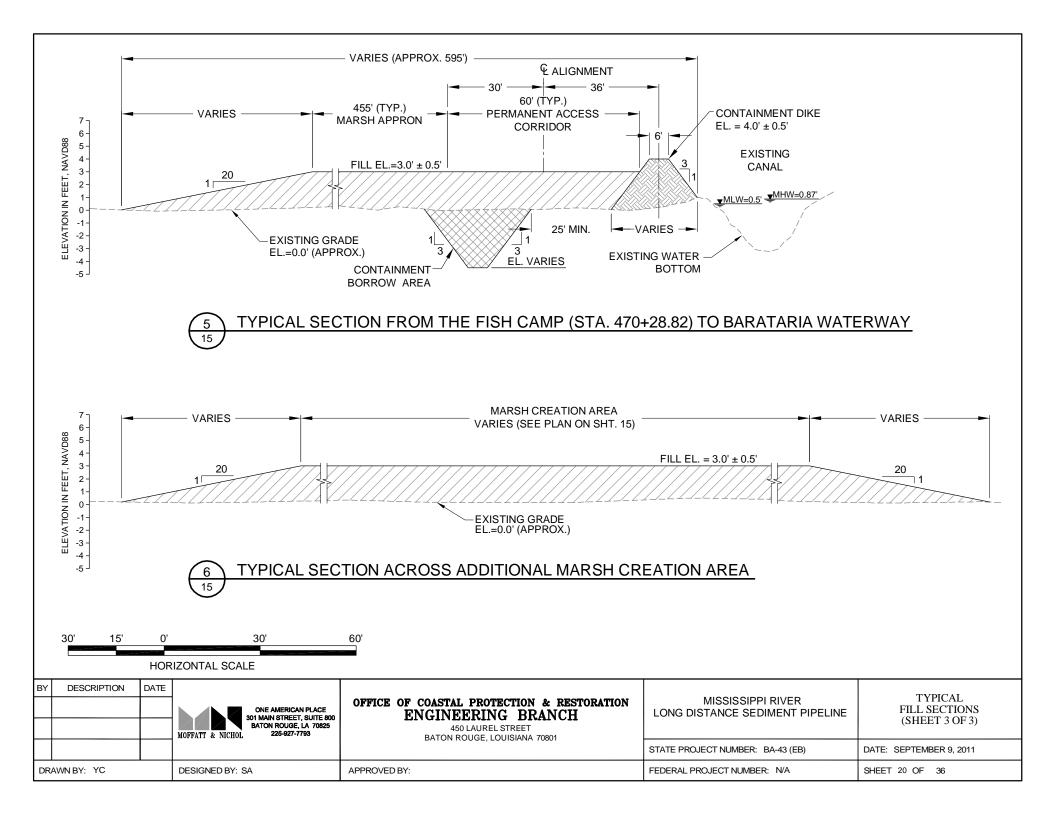
ACCESS CHANNEL ALIGNMENT

		AC				1	
PT.	EAST	ING	NOTRHING	PT.	EASTIN	G	NOTRHING
1	36740	46.30	417690.06	46	3687438.	03	413721.65
2	36744	43.87	417928.38	47	3687616.	06	413782.04
3	36745	49.10	417843.37	48	3687710.	79	413852.06
4	36746	05.34	417650.30	49	3687766.	22	414034.24
5	36747	68.33	417626.30	50	3687811.	91	414175.11
6	36748	91.14	417524.89	51	3687930.	02	414339.53
7	36751	73.97	417404.50	52	3688053.	13	414460.19
8	36753	74.37	417400.08	53	3688138.	44	414524.38
9	36758	99.41	417192.18	54	3688306.	59	414717.17
10	367624	42.80	417171.66	55	3688397.	69	414842.33
11	367642	28.65	417358.88	56	3688450.	73	414937.10
12	367654	48.44	417686.20	57	3688547.	73	415047.00
13	367673	39.59	417811.17	58	3688627.	47	415092.91
14	36773	75.53	417869.55	59	3688728.	60	415115.08
15	36778		417830.11	60	3688878.		415127.36
16	36783	37.82	417708.89	61	3689243.	43	415004.47
17	36788		417514.80				
18	36797	72.32	416805.21				
19	367993	30.74	416596.04				
20	36802	21.29	416069.93				
21	36805	93.81	415970.76				
22	36807	18.25	415816.36				
23	36809	50.88	415619.43				
24	36813	78.51	415564.60				
25	36816	35.27	415496.11				
26	36819	77.36	415432.46				
27	36822	05.59	415229.13				
28	36822	50.83	415129.57				
29	36823	97.09	414968.27				
30	36831	38.30	414802.76				
31	36834	74.36	414513.64				
32	36837	92.94	414308.27				
33	36840	35.91	414239.78				
34	36842	85.57	414253.96				
35	36845	42.75	414352.05				
36	36847	64.87	414409.57				
37	36850	15.36	414387.73				
38	36851	68.42	414252.81				
39	36852	81.66	414088.33				
40	36853	59.42	414002.16				
41	36854	50.50	413949.56				
42	36858	98.07	413778.66				
43	36864	47.21	413686.62				
44	36867	40.16	413671.24				
45	36871	88.62	413691.73				
	TION		MISSISSIPPI				PROJECT
IUKA	LIUN	1	INIGOIOOIFFI				

BY	DESCRIPTION	DATE				PROJECT
			ONE AMERICAN PLACE 301 MAIN STREET, SUITE 800	OFFICE OF COASTAL PROTECTION & RESTORATION ENGINEERING BRANCH	MISSISSIPPI RIVER LONG DISTANCE SEDIMENT PIPELINE	ALIGNMENT
			BATON ROUGE, LA 70825 MOFFATT & NICHOL 225-927-7793	450 LAUREL STREET BATON ROUGE. LOUISIANA 70801		TABLES
					STATE PROJECT NUMBER: BA-43 (EB)	DATE: SEPTEMBER 9, 2011
DR	AWN BY: YC		DESIGNED BY: SA	APPROVED BY:	FEDERAL PROJECT NUMBER: N/A	SHEET 17 OF 36







MISSISSIPPI RIVER BORROW AREA BORING LOGS

Following pages contain the boring logs corresponding to F-1, F-3, F-4, and F-5 on Sheets 7 and 8 of 81 of the Plans.

		1			LOCATION: See Plate 1			CL	ASSIF	ICAT	ION	1		SHE	AR S	TREN	GTH	
DEPTH , FT	WATER LEVEI	SYMBOL	SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 44' 29.7" W 90° 00' 13.3" SURFACE EL.: -38.9' NAVD88	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetron rvane eld Var		Ur Miniat		xial 🔴
	MA		S	В	STRATUM DESCRIPTION	- N E	UNIT	PAS 200	S COS		<u>п</u>	IN PLA		к	IPS PE	R SQ F	Т	
		<u> </u>	·.M		POORLY GRADED SAND WITH SILT (SP-SM),		<u> </u>	7	30				0	.5 1	.0 1	.5 2.	0 2	.5
			.fl		brown and gray, with layers of organics	2.0	-	<i>'</i>	50			-						
– .					SILTY SAND (SM), brown and gray	2.0	_					-						
							-					-						
- 5 -							F					-						
							-					-	-					
							-	32				-						
-10					- with clay layers below 10'		╞					-						
							_					-						
							-					-	-					
- 			X	N=10	POORLY GRADED SAND WITH SILT (SP-SM), medium-dense, brown and gray	14.0	_	9	33			_						
				N=14			-					-						
- ·							-					-						
	1		÷Й	N=11			-	9	27			-						
			<u>:</u> [N=12			-	11	27			-						
			A	N=4	LEAN CLAY (CL), soft, gray, with sand pockets	+ 22.0 + 24.0	-	91	47	46	22	24 _	-					
-25-			M	N=29	SILTY SAND (SM), medium-dense, gray	24.0	-	25	19			_						
				N=42	- dense from 26' to 27.5'		-					-	-					
			X	N=19	- with clay pockets at 28'		-	22	26			-	-					
- 30 - -			X	N=18			-					-						
			X	N=18			-	17	28			-						
-35-	+						╞					-						
	1						F					-						
	+			N=1.1			ŀ	_	000			-	-					
			Ĥ	N=14	- with a clay layer at 38.5'		-	7	29			-						
<u>NOT</u>												ion d. Pth:		April	13, 2	2012		
				-	ols defined on Plates 8a and 8b. below water surface = 44 ft at time of drilling.					CAVI	ED DE	EPTH:	Not A					
	'	_										ER: No ARY: (le			
												Cem			nite G	rout		
										LOG	GER:	L. Me	yer					
	-			20	LDSP River Borings					L	_OG	OF	BO	RIN	IGI	NO.	F-'	1
Fugr	o C	ons	ultar	nts, Inc.	Plaquemines, Louisiana				Pro	ject N 04		240	14		PI	_ATI	= 2)a
L										÷ '			• •			-/ \	_ 4	

				~	LOCATION: See Plate 1			CL/	ASSIF	ICAT	ION			SHE	AR S	TRENG	ЭTН	
DEPTH , FT	WATER LEVEI	SYMBOL SAMPLES		BLOWS PER FOOT	COORDINATES: N 29° 44' 29.7" W 90° 00' 13.3" SURFACE EL.: -38.9' NAVD88	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	netron vane Id Var		Uno Miniatu	confine Triaxi re Var	ial 🔶
ä	WA	000		H H		N B		PASS 200 S	CON			PLA		к	PS PE	R SQ F	Г	
	+	/ जनक			STRATUM DESCRIPTION SILTY SAND (SM), medium-dense, gray								0.	5 1	.0 1	.5 2.0	2.	5
 			۱	√=26			- - - -	13	29			- - - - - -						
 			۹ <u>۲</u>	V=13			-											
 	-		× 1	V=23			-	8	29			_						
 	-		X	N=7	FAT CLAY (CH), firm, light gray and tan, with silt seams	- 56.0	-		37	56	23	- - 33 _						
 	-		X	N=6			- - -	95	35									
 	-			N=4	POORLY GRADED SAND WITH SILT (SP-SM),	- 71.0	- - -		46	64	24	- 40 _ _						
 75 -	-		۱	√=46	dense, gray and tan		- - -	11	23			- - - -						
	-		۲ ۱	\= 50			-	5	21			-	-					
	1. T	Terms			ols defined on Plates 8a and 8b. below water surface = 44 ft at time of drilling.			·		TOTA CAVE DRY WET BACA	al de Ed de Auge Rot/ Kfill:	ION D. PTH: EPTH: ER: No ARY: (Cem L. Me	84.5' Not A ot App 0' to 8 ent-B	opplic blicab 4.5'	able le			
	ī	lG		0	LDSP River Borings					L	.OG	OF	BO	RIN	IGN	10.	F-1	
Fugr	o Co	onsult	tants	s, Inc.	Plaquemines, Louisiana				Pro	ject N 04		240	14		PL	_ATE	E 2	b

	_				LOCATION: See Plate 1			CL	ASSIF	ICAT	ION			SHE	AR S	TREN	IGT⊦	ł
H, FT	WATER LEVEL	30L	LES	BLOWS PER FOOT	COORDINATES: N 29° 44' 29.7"	STRATUM DEPTH, FT	Ň,	0%	%		0	È≘		enetror orvane	neter	U	nconfi	ned ▼ axial ●
ОЕРТН, F1	TER	SYMBOL	SAMPLES	FOO	W 90° 00' 13.3" SURFACE EL.: -38.9' NAVD88	EPTH	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIMIT	PLASTIC LIMIT	PLASTICITY INDEX (PI)		eld Va	ne	Minia		ane 🔺
	MA		$\left \right $	BL	STRATUM DESCRIPTION		LINU	PAS 200	S S		E	<u>I</u>				ERSQ		
_					POORLY GRADED SAND WITH SILT (SP-SM),	80.0							. 0	0.5 1	.0 ,	1.5 2	.0 2	2.5
-	-				gray and tan		-					-	-					
-			\cdot				_					-						
-85	-					- 84.5	F	1	1							+		+
_							-					-	-					
-							_					-	-					
-90	-						╞					-	-					
-							-					-	-					
-	-						-					-						
- 							F					_						
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- 1 10 ⁻							-					-						
-												-						
-	-						-					-	-					
115							-					-						
	-						-					-	-					
							-					-						
		I			I					COM	I IPLET	ION D	L ATE:	Apri	13, 2	2012		<u> </u>
			ms a	nd symb	ools defined on Plates 8a and 8b.					TOTA	AL DE	PTH:	84.5'					
	2. [Dep	oth to	mudline	e below water surface = 44 ft at time of drilling.							EPTH: ER: No						
												ARY: (: Cem			vito C	rout		
501 L												L. Me		ento	iile C	iout		
047100																		
	ī			20	LDSP River Borings					L	.OG	OF	BO	RIN	IG	NO.	F-	1
			3															
	ro C	ore		te Inc					Pro	ject N	lo.							
rug	00	OUS	unar	nts, Inc.	Plaquemines, Louisiana					04	.551	240	14		Ρ	LAT	E	2c

FCBR_LOG (FINAL) 04:55124014.GPJ FUGRO DATA TEMPLATE 042610.GDT 06/08/12

	<u>.</u>	i		~	LOCATION: See Plate 1			CL	ASSIF	ICAT	ION			SHE	AR S	TREN	GTH	
DEPTH , FT			SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 44' 13.3" W 89° 59' 55.3"	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	STIC	PLASTICITY INDEX (PI)	♦To	netron rvane eld Var		Ur Miniat		xial 鱼
DE	VATI		SA	BLO	SURFACE EL.: -45.2' NAVD88	RIST	D LIN	PASSI 200 SI	CONT	25	PLA	PLAS		к	IPS PE	ER SQ F		
		>			STRATUM DESCRIPTION								0			1.5 2.		.5
	-			N=22	POORLY GRADED SAND (SP), medium-dense, brown		-	3	25			-						
		. .	.:: x	N=12								-						
				N=2	- very loose from 4' to 8'		-	2	31			-						
			:	N=2			_	4	28			-						
				N=8	- loose below 8'		-	2	28			-						
10				N=10			-					-						
		Ŀ		N=9	POORLY GRADED SAND WITH SILT (SP-SM),	13.0	-	5	27									
- ·				N=18	medium-dense, gray - brown at 14'		F					-						
 	_			N=13	- brown and gray from 15' to 25'		-	11	25			-						
E .			: . F	N=4			_	7	33			-						
- <u>20</u> -	_						- - -					-						
- 25 - 	-			N=3	- brown from 25' to 38'		-	13	38									
 	_			N=34	- medium-dense below 91'		- - -	8	29									
	_			11-20			- - -					- - -						
			∷Ì⊼	N=17	- brown and gray below 38'		F					-						
	1.	Te			bols defined on Plates 8a and 8b. e below water surface = 52 ft at time of drilling.		<u> </u>			TOTA CAVE DRY WET BACE	al de Ed de Auge Rot/ Kfill:	ION D. PTH: PTH: ER: No ARY: (Cem L. Me	74.5' Not A ot App 0' to 7 ent-B	Applic blicab 74.5	able le			
	F	J	ਜ _/	20	LDSP River Borings					L	OG	OF	BO	RIN	IG	NO.	F-:	3
Fugr	ro C	Con	sulta	ints, Inc.	Plaquemines, Louisiana				Pro	oject N 04		240	14		P	LATI	Ξ.3	Ba

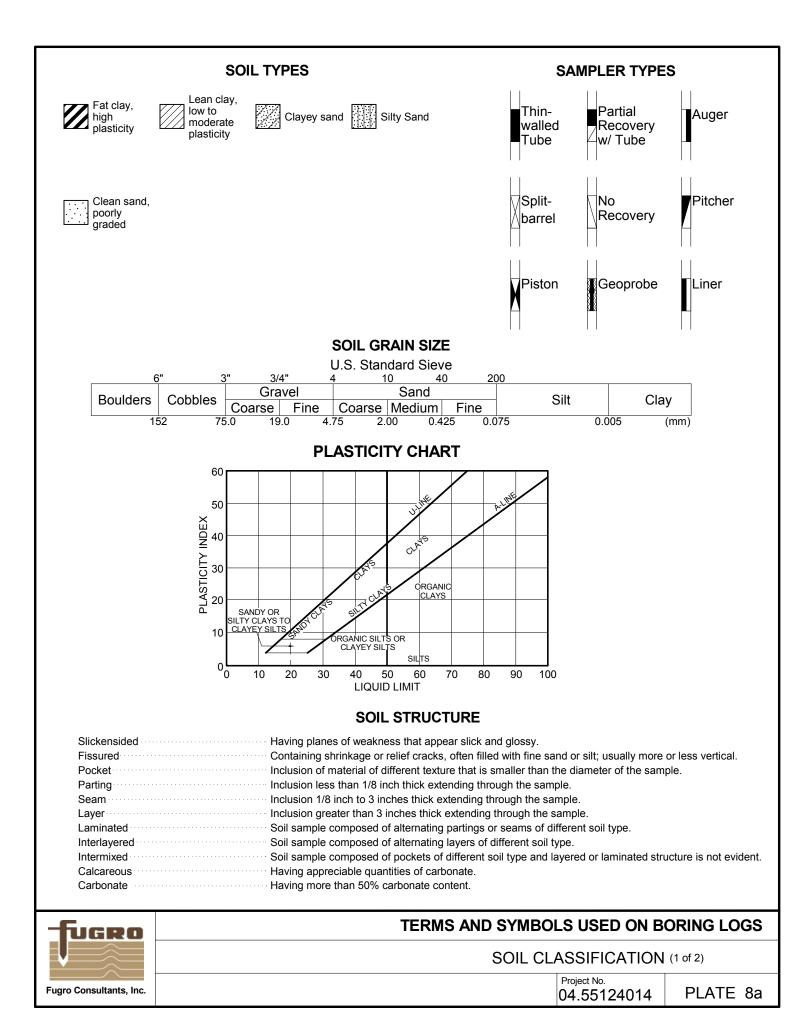
		i		~	LOCATION: See Plate 1			CL	ASSIF	ICAT	ION			SHE	AR S	TREN	GTH	
H, FT	WATER I EVE		JLES	BLOWS PER FOOT	COORDINATES: N 29° 44' 13.3"	STRATUM DEPTH, FT	WT,		, %		U	۲۲ (ات		netron	neter	Ur	iconfin Triax	ied ▼ kial ●
DEPTH, FT	TER	SVMBOI	SAMPLES	PO0-	W 89° 59' 55.3" SURFACE EL.: -45.2' NAVD88	STRA	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, 9	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)		eld Var	ie	Miniat		
	M			BI	STRATUM DESCRIPTION		INN	PAS 200	100			PL	0			ER SQ F		5
					SILTY SAND (SM), medium-dense, gray	40.0	-					-			-		-	
												-						
			X	N=15			-	12	32			-						
45							-					_						
					with the larger below (0)		-					-						
			X	N=19	- with clay layers below 48'		-	14	29			_						
							F					-						
					POORLY GRADED SAND WITH SILT (SP-SM), medium-dense, gray	- 52.0	-					_						
		 .	Ă	N=15			L	5	29			-						
- 55							-					-						
				NI 40	- with layers of organics at 57' - with a clay layer at 58'		_					-						
			∴Å	N=13			L					-						
							_					-						
			: .: .:	N=30			-	11	29			-						
				11-30	FAT CLAY (CH), very stiff, gray	65.0			23									
							-					-						
				N=19		69.0	-		54	77	25	52						
-70-	+				SILTY SAND (SM), medium-dense, gray, with organic lenses	09.0	╞					_						
							_					-						
				N=11			_	18	28			-						
75						- 74.5	F	+										
							_					_						
							-					-						
	L ES						I			COM	L PLET	ION D	L ATE:	April	6, 20)12		
	1.	Ter			pols defined on Plates 8a and 8b.							PTH: PTH:		Applic	able			
	2.	De	pth to	o mudlin	e below water surface = 52 ft at time of drilling.					DRY	AUGE	ER: No	ot App	olicab				
										BACI	KFILL	ARY: (: Cem	ent-B		ite G	rout		
										LOG	GER:	L. Me	yer					
.t.																		
	-		2	20	LDSP River Borings				I	L	.OG	OF	BO	RIN	IG I	NO.	F-:	3
			£						Pro	ject N	0.							
Fugr	0 0	Con	sulta	nts, Inc.	Plaquemines, Louisiana							240	14		Ρl	_AT	E 3	ßb

	<u></u>			~	LOCATION: See Plate 1			CL	ASSIF	ICAT	ION			SHE	AR S	TREN	GTH	
H, FT	WATER LEVE	30L	LES	BLOWS PER FOOT	COORDINATES: N 29° 43' 06.1"	STRATUM DEPTH, FT	ΨT,		; %		0	<u>ک</u>		netrom	neter	Un	confined Triaxial	
DEРТН, FT	TER	SYMBOL	SAMPLES	FOO	W 89° 59' 21.6" SURFACE EL.: -50.1' NAVD88	STRA	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, 9	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)		eld Van	ie	Miniat	ire Vane	
	MA		$\langle \rangle$	В	STRATUM DESCRIPTION		INN	PAS 200	20		L.] ₹	n			ER SQ F		
			· .		POORLY GRADED SAND (SP), brown - with shell fragments from 0' to 8'		-					-		- 1				
					- with wood fragments and organics to 10'			3	29			-						
	$\left \right $		÷				-					-						
- 5 -							_	4	20			-						
							-					-						
	$\left \right $.X	N=13	- medium-dense from 8' to 14'		-	6	36			-						
10			Ξ	N=16			-					-						
			\mathbb{R}	N=12	- gray and brown from 12' to 57'		-	4	23			-						
- 15 -				N=6	- loose from 14' to 16'		-					-						
			÷Ĥ	N=22	- medium-dense from 16' to 22'		F	5	24			-						
			:11 	N=21			-					-						
- 20-					- with clay pockets at 20'		-					-						
			Ĭ	N=26			-	9	25			-						
	$\left \right $		÷Д	N=34	- dense from 22' to 24'		-					-						
-25-		· · · ·	8	N=27	- medium-dense from 24' to 32'		-	7	28			-						
			:M	N=20			-					-						
							-					-						
-30-	$\left \right $						-					-						
					- dense from 32' to 40'		_					-						
			<u>.</u> М.:	N=34			-	3	23			-						
[™] -35 -							_					-						
	+		M	N=33			-					-						
				N=55			-					-						
	<u> </u>	<u></u>	<u>· </u>			1	1	1				ion d		April	3, 20	012	<u> </u>	┨
	1. 1	Tern		•	ols defined on Plates 8a and 8b. bolow water surface $= 57$ ft at time of drilling							PTH: PTH:		Applic	able			
	∠. L	Jeh	נט	muuline	below water surface = 57 ft at time of drilling.					DRY	AUGE	ER: No ARY: (ot App	olicab				
										BACI	KFILL	: Cem	ent-B		ite G	irout		
- 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6										LOG	ger:	L. Me	yer					
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2																		
				20	LDSP River Borings					L	.OG	OF	во	RIN	IG I	NO.	F-4	
			~															
	~ ~	000-							Pro	ject N								_
Fugi	TO C	onsi	utar	nts, Inc.	Plaquemines, Louisiana					04	.551	240	14		Pl	_ATE	E 4a	

		i				LOCATION: See Plate 1			CL	ASSIF	ICAT	ION			SHE	AR S	TREN	GTH	
H, FT	WATER I EVE		LES	BLOWS PER	ь	COORDINATES: N 29° 43' 06.1"	TUM 4, FT	, M		%		0	≿≘		netron rvane	neter	Ur	confin	ied ▼ kial ●
DEPTH , FT	TER		SAMPLES	SMO	БО ГО	W 89° 59' 21.6" SURFACE EL.: -50.1' NAVD88	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, 9	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)		rvane eld Var	ie	Miniat		
	MA			BL		STRATUM DESCRIPTION		INN	PAS 200			۲. ۲] ₹	0			ER SQ F		.5
						POORLY GRADED SAND (SP), very dense, brown	40.0	-					-					<u> </u>	
E :				N=(67	- with shell fragments at 42'		E	5	22			-						
								-					-						
45								-					-						
-			X	N=:	37	- medium-dense to dense below 47'		-					-						
								-					-						
50			:					-					-						
-			∷k	N=:	25			E	7	23			-						
								F					-						
55						- with a clay layer from 56' to 57'		-					-						
		. [.] . .				- gray below 57'		-	3	17			-						
								-					-						
60								-					-						
			$\frac{1}{2}$	N=:	29			-					-						
								-					-						
65			: :					-					-						
_ ·			÷Ϊ	N=	31	- with clay pockets at 67'			4	22			-						
							68.5		+					·			+ - +		
70								-					-						
								-					-						
								-					-						
75								-					-						
								-					-						
42610.								-					-						
	ES	<u>:</u>											ion d. Pth:		April	3, 20)12		
EMP						ols defined on Plates 8a and 8b. below water surface = 57 ft at time of drilling.					CAV	ED DE	EPTH:	Not A					
													ER: No ARY: (le			
-06KC											BAC	KFILL	: Cem	ent-B		ite G	rout		
- CHJ -											log	GER:	L. Me	yer					
124014																			
	-			20		LDSP River Borings					L	_OG	OF	во	RIN	IG I	NO.	F-4	4
			Ŀ	\ge						Pro	ject N	lo.							
Fugi	·o C	Con	sulta	nts, lı	nc.	Plaquemines, Louisiana							240	14		Ρl	_ATI	Ξ 4	ŀb

		i		~	LOCATION: See Plate 1			CL	ASSIF	ICAT	ION			SHE	AR S	TREN	GTH	
DEPTH , FT		SVMROI	SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 42' 39.7" W 89° 59' 09.9" SURFACE EL.: -49.8' NAVD88	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetror rvane eld Va		Ur Miniat		xial 🔶
Ö	- MA		No.	BLo		N B	UNIT	PAS 200	SON			PLA		к	IPS PI	ER SQ F	т	
					STRATUM DESCRIPTION SILTY SAND (SM), brown, with gravel								0	.5 1	1.0 ·	1.5 2.	0 2	.5
	-		ľľ		SILTI SAND (SM), DOWN, WILL GRAVE		-	27	48			-						
					POORLY GRADED SAND (SP), brown	- 2.0	_					_						
 							-	2	25			-						
							-					-						
- ·							-	2	23			-						
				N=13	- medium-dense from 11' to 13'		-	1	22			-						
·	-		. [N=8	 loose from 13' to 21' with shell fragments at 13' 		╞	3	22			-						
15				N=7	- with wood fragments at 15'		-	2	25			-						
				N=7			-					_						
				N=9	- with organic layer at 18.5' - with wood fragments at 19'		-	3	33									
				N=21	- gray and brown from 21' to 27' - medium-dense from 21' to 32'		-					-						
	_		÷β	N=16			-	2	22			-						
- 25				N=18			-	3	22			-						
				N=19	- gray below 27'		-	4	26			-						
				N=27			-					-						
	_		· k	N=9	POORLY GRADED SAND WITH SILT (SP-SM),	- 32.0		9	28									
					loose to medium-dense, gray		_					-						
35							-					-						
				N=21			-	5	25			-						
		<u> ::</u>									 PI FT	ION D		Anri		012		
	1.	Ter		-	ols defined on Plates 8a and 8b. e below water surface = 48.5 ft at time of drilling.					TOT/ CAVI DRY WET	al de Ed de Auge Rot/	EPTH: EPTH: ER: No ARY: (Cem	73.5' Not A ot App 0' to 7	Applic blicat '3.5'	able le			
												L. Me						
	1	J	н	RO	LDSP River Borings					L	.0G	OF	BO	RIN	IG	NO.	F-	5
Fugr	ro C	Con	sulta	ints, Inc.	Plaquemines, Louisiana				Pro	ject N 04		240	14		P	LATI	= #	วิล
L					I • •													

Line Discrete Constrained Constrained <thconstrained< th=""> Constrained <thco< th=""><th></th><th>_</th><th>Ŀ</th><th></th><th>~</th><th>LOCATION: See Plate 1</th><th></th><th></th><th>CL</th><th>ASSIF</th><th>ICAT</th><th>ION</th><th></th><th></th><th>SHE</th><th>AR S</th><th>TREN</th><th>IGTH</th><th>I</th></thco<></thconstrained<>		_	Ŀ		~	LOCATION: See Plate 1			CL	ASSIF	ICAT	ION			SHE	AR S	TREN	IGTH	I
The image: stratuly DESCRIPTION 1	ОЕРТН, FT	ATER I EVE	SYMBOI	SAMPLES	LOWS PER FOOT	W 89° 59' 09.9"	STRATUM DEPTH, FT	IT DRY WT, PCF	SSING NO. 0 SIEVE, %	WATER DNTENT, %	LIQUID	PLASTIC LIMIT	LASTICITY NDEX (PI)	♦To	rvane eld Var	ne	Minia	Tria ture V	xial 🕈
45 POORLY GRADED SAND WITH SILT (SP-SM). dense, brown, with gravel - with wood fragments at 42' 40.0 40.0 45 CLAYEY SAND (SC), loose, gray, with shell fragments and wood 45.0 - 32 36 38 15 23 50 N=6 LEAN CLAY (CL), very stiff, gray and tan, with sill seams 52.0 - 22 44 14 30 55 - - with silly sand layers at 57' - 94 28 36 16 20 60 - FAT CLAY (CH), stiff to very stiff, gray and tan 62.0 86 33 58 21 37 60 - SILTY SAND (SM), tan and gray 72.0 - - - - -		3	Š	$\langle $	ш	STRATUM DESCRIPTION		S	20 20	ŭ			_ <u> </u>	0					2.5
N=33 - with wood fragments at 42' 45 CLAYEY SAND (SC), loose, gray, with shell 45 32 36 38 15 23 50 N=5 - - 32 36 38 15 23 50 N=16 LEAN CLAY (CL), very stiff, gray and tan, with sit seams 52.0 - 22 44 14 30 60 - - with silty sand layers at 57' - - 28 36 16 20 94 28 36 16 20 - - - - 60 - FAT CLAY (CH), stiff to very stiff, gray and tan 62.0 86 33 58 21 37 - - - 70 - SILTY SAND (SM), tan and gray 72.0 - <td></td> <td></td> <td></td> <td>•••</td> <td></td> <td>POORLY GRADED SAND WITH SILT (SP-SM), dense brown with gravel</td> <td>40.0</td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td></td> <td></td> <td>.0</td> <td></td> <td></td> <td></td>				•••		POORLY GRADED SAND WITH SILT (SP-SM), dense brown with gravel	40.0	-					-			.0			
N=5 N=5 S0 N=16 LEAN CLAY (CL), very stiff, gray and tan, with silt seams 52.0 - with silty sand layers at 57' - with silty sand layers at 57' - FAT CLAY (CH), stiff to very stiff, gray and tan 60 - FAT CLAY (CH), stiff to very stiff, gray and tan 62.0 - S1LTY SAND (SM), tan and gray 70 70 70 71 - SILTY SAND (SM), tan and gray 72 75					N=33	-		-					-	-					
N=5 N=5 S0 N=16 LEAN CLAY (CL), very stiff, gray and tan, with silt seams 52.0							45.0						-						
50 N=16 LEAN CLAY (CL), very stiff, gray and tan, with silt seams 52 22 44 14 30 60 - with silty sand layers at 57 - with silty sand layers at 57	- 45						40.0	-					-	-					
N=16 LEAN CLAY (CL), very stiff, gray and tan, with silt seams 52.0 22 44 14 30 - - with silty sand layers at 57' 94 28 36 16 20 60 - - with silty sand layers at 57' 94 28 36 16 20 64 - - - - - - - - 65 - - - - - - - - 66 - - - - - - - - 66 - - - - - - - - 70 - - - - - - - - 70 - - - - - - - - 70 - - - - - - - - 70 - - - - - - - - - 70 <t< td=""><td></td><td></td><td></td><td></td><td>N=5</td><td></td><td></td><td>-</td><td>32</td><td>36</td><td>38</td><td>15</td><td>23 _</td><td></td><td></td><td></td><td></td><td></td><td></td></t<>					N=5			-	32	36	38	15	23 _						
N=16 LEAN CLAY (CL), very stiff, gray and tan, with silt seams 22 44 14 30 - with silty sand layers at 57' - with silty sand layers at 57' 94 28 16 20 60 - with silty sand layers at 57' 94 28 16 20 94 28 35 58 21 37 65 - - - - - 70 - SILTY SAND (SM), tan and gray 72.0 - - - 75 - - - - - - -	50 -		/					_					-						
- with silty sand layers at 57" - with silty sand layers at 57" - 60	-				N=16		- 52.0			22	44	14	30						
- with silty sand layers at 57' - with silty sand layers at 57' 60 - with silty sand layers at 57' 60						silt seams		E					-						
60 FAT CLAY (CH), stiff to very stiff, gray and tan 62.0 94 28 1	- 55							-					-						
FAT CLAY (CH), stiff to very stiff, gray and tan 62.0 65 62.0 66 35 58 21 37 65 65 65 70 86 33 69 24 45 65 65 70 70 72.0 72.0 72.0 72.0 72.0 72.0 72.0 72.0 73.5 72.0 73.5						- with silty sand layers at 57'		94			36	16	20						
AT CLAY (CH), sum to very sum, gray and tan 35 58 21 37 65 33 86 33 86 33 9 70 88 37 69 24 45 6 70 82 37 69 24 45 6 70 72.0 72.0 72.0 73.5	- 60 -							-					_						
65 39 69 24 45 70 82 37 69 24 45 82 37 69 24 45 82 37 69 24 45 70 72.0 72.0 72.0 72.0 75 73.5 22 25 1						FAT CLAY (CH), stiff to very stiff, gray and tan	62.0	-		35	58	21	37						
70 SILTY SAND (SM), tan and gray 72.0 75 75								86		33			-					•	
70 82 37 SILTY SAND (SM), tan and gray 72.0 75 73.5	- 65							-					-						
70 70 SILTY SAND (SM), tan and gray 72.0 75 73.5								82			69	24	45				•		
No SILTY SAND (SM), tan and gray 77.5 - 77.5 - 1 <td< td=""><td>- 70-</td><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td></td<>	- 70-							-					-						
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	75-							-					-						
NOTES: 1. Terms and symbols defined on Plates 8a and 8b. COMPLETION DATE: April 1, 2012 TOTAL DEPTH: 73.5' CAVED DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 73.5' BACKFILL: Cement-Bentonite Grout LOGGER: L. Meyer Image: Complex in the image: Complex in the image: Complex interval of th								-					-	-					
NOTES: 1. Terms and symbols defined on Plates 8a and 8b. 2. Depth to mudline below water surface = 48.5 ft at time of drilling. COMPLETION DATE: April 1, 2012 TOTAL DEPTH: 73.5' CAVED DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 73.5' BACKFILL: Cement-Bentonite Grout LOGGER: L. Meyer LDSP River Borings LOG OF BORING NO. F-								-					-						
1. Terms and symbols defined on Plates da and 80. 2. Depth to mudline below water surface = 48.5 ft at time of drilling. CAVED DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 73.5' BACKFILL: Cement-Bentonite Grout LOGGER: L. Meyer LDSP River Borings LOG OF BORING NO. F-	NOT					hale defined on Diates 25 and 25									April	1, 20	U12		
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BACKFILL: Cement-Bentonite Grout LOGGER: L. Meyer											WET	ROT	ARY: (0' to 7	73.5'				
LDSP River Borings LOG OF BORING NO. F-	5														entor	nite G	Fout		
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		5	Ir	e -	20	LDSP River Borings					L	.OG	OF	во	RIN	IG	NO.	F-	5
Fugro Consultants, Inc. Plaquemines, Louisiana 04.55124014 PLATE	Fugr	o C	Con	sultar	nts, Inc.	Plaquemines, Louisiana				Pro			240	14		P	LAT	Έ	5b



STANDARD PENETRATION TEST (SPT)

A 2-in.-OD, 1-3/8-ID split spoon sampler is driven 1.5 ft into undisturbed soil with a 140-pound hammer free falling 30 in. After the sampler is seated 6 in. into undisturbed soil, the number of blows required to drive the sampler the last 12 in. is the Standard Penetration Resistance or "N" value, which is recorded as blows per foot as described below.

SPLIT-BARREL SAMPLER DRIVING RECORD

Blows Per Foot	Description
25	25 blows drove sampler 12 inches, after initial 6 inches of seating.
50/7"	50 blows drove sampler 7 inches, after initial 6 inches of seating.
Ref/3" ·····	50 blows drove sampler 3 inches during initial 6-inch seating interval.

NOTE: To avoid damage to sampling tools, driving is limited to 50 blows during or after seating interval.

DENSITY OF GRANULAR SOILS

Descriptive Term	*Relative Density, %	**Blows Per Foot (SPT)	Term	Undrained Shear Strength, ksf	Blows Per Foot (SPT) (approximate)
Very Loose	< 15	0 to 4	Very Soft	< 0.25	0 to 2
Loose	15 to 35	5 to 10	Soft	0.25 to 0.50	·····2 to 4
Medium Dense	35 to 65	11 to 30	Firm	0.50 to 1.00	4 to 8
Dense	65 to 85		Stiff	1.00 to 2.00	
Very Dense	> 85	> 50	Very Stiff	2.00 to 4.00	16 to 32
*Estimated from some landwising upper			Hard	> 4.00	> 32

*Estimated from sampler driving record.

**Requires correction for depth, groundwater level, and grain size.

STRENGTH OF COHESIVE SOILS

Term	Undrained Shear Strength, ksf	Blows Per Foot (SPT) (approximate)
Very Soft	< 0.25	0 to 2
Soft	0.25 to 0.50	·····2 to 4
Firm	0.50 to 1.00	·····4 to 8
Stiff	1.00 to 2.00	·····8 to 16
Very Stiff	2.00 to 4.00	16 to 32
Hard	> 4.00	> 32

SHEAR STRENGTH TEST METHOD

U = Unconfined Q = Unconsolidated - Undrained Triaxial

P = Pocket Penetrometer T = Torvane V = Miniature Vane F = Field Vane

HAND PENETROMETER CORRECTION

Our experience has shown that the hand penetrometer generally overestimates the in-situ undrained shear strength of over consolidated Pleistocene Gulf Coast clays. These strengths are partially controlled by the presence of macroscopic soil defects such as slickensides, which generally do not influence smaller scale tests like the hand penetrometer. Based on our experience, we have adjusted these field estimates of the undrained shear strength of natural, overconsolidated Pleistocene Gulf Coast soils by multiplying the measured penetrometer reading by a factor of 0.6. These adjusted strength estimates are recorded in the "Shear Strength" column on the boring logs. Except as described in the text, we have not adjusted estimates of the undrained shear strength for projects located outside of the Pleistocene Gulf Coast formations.

Information on each boring log is a compilation of subsurface conditions and soil or rock classifications obtained from the field as well as from laboratory testing of samples. Strata have been interpreted by commonly accepted procedures. The stratum lines on the logs may be transitional and approximate in nature. Water level measurements refer only to those observed at the time and places indicated, and can vary with time, geologic condition, or construction activity.



TERMS AND SYMBOLS USED ON BORING LOGS

SOIL CLASSIFICATION (2 of 2)

Proiect No. 04.55124014